# UNIVERSITY OF NATURAL RESOURCES AND LIFE SCIENCES, VIENNA DEPARTMENT OF FOREST AND SOIL SCIENCE

Master Thesis

# CO<sub>2</sub>-Exchange and Enzyme Activities of Climate Change Simulation Treatment Plots in Subarctic Tundra Heath

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## Abstract

Arctic ecosystems are exposed to stronger warming than the rest of the world and shrub vegetation is expanding in the tundra, which may alter soil organic matter (SOM) decomposition, while increasing litter input to the soil. These changes raise the question about possible climate change feedbacks: E.g. Will enhanced plant growth increase the carbon sink capacity, or will faster SOM turnover increase the CO2 emissions from the large belowground carbon stocks? The study site, located in a subarctic tundra heath in northern Sweden, has been manipulated for 6 years with warming (W) or addition of following substrates: Leaf litter from local Betula (B) or Salix (S) species or fungal fruitbodies (F), with a C:N ratio of 45, 22 and 11 respectively. Carbon fluxes on ecosystem level, respiration (ER), photosynthesis (GEP) and net exchange (NEE) and Net Differential Vegetation Index (NDVI) were measured 14 times during the snow free period. All fluxes and NDVI were enhanced by B, S and F treatment in correlation with the nitrogen content of the substrate. Warming increased fluxes and NDVI stronger than litter addition but less than the fungi treatment. We conclude that increasing litter input will enhance activity and growth in dependence of its quality, but warming is the main control agent for change in tundra ecosystems. Impact of W and F treatments were statistically significant ( $\alpha$ =0.05), except for NEE. Still, NEE changed with the same treatment pattern as ER, GEP and NDVI and strengthens our implications about the carbon sink function of the ecosystem. Abiotic soil properties and extracellular enzyme activities from soils collected during mid-summer were not affected after 6 years of treatment. Activity of carbon and nitrogen cycling enzymes were higher in 5-10 cm depth than in surface soil, in contrast to phosphatase. This suggests different nutrient demands of tundra soil at different depths and potential higher decomposition of SOM below the top 5cm of soil.

CO2-flux, Enzyme activity, subarctic tundra, climate warming, litter addition

## **Abstract in German**

Arktische Ökosysteme erwärmen sich stärker als der Rest der Welt und in der Tundra ist bereits Verstrauchung zu erkennen, was den Streueintrag erhöht und den Abbau organischer Bodensubstanz (OBS) verändern kann. Das könnte Rückkopplungs-Effekte auf den Klimawandel verursachen, z.B. begünstigte Kohlenstoff-Speicherung durch erhöhtes Pflanzenwachstum oder aber erhöhte CO2-Emissionen durch den verstärkten Abbau im Boden gespeicherter OBS. Untersuchungsflächen, in einer subarktischen Tundra in Nordschweden, wurden 6 Jahre lang mit Erwärmung (W) oder Zugabe folgender Substrate behandelt: Laub lokaler Birken (B. pubescens ssp tortuosa, B) und Weiden (S. myrsinifolia, S) sowie Pilz-Fruchtkörpern (F) mit einem jeweiligen C:N Verhältnis von 45, 22 bzw. 11. Die CO2-Flüsse, Atmung (ER), Photosynthese (GEP) und Nettoaustausch (NEE), und der Normierte Differenzierte Vegetationsindex (NDVI) wurden 14-mal während der schneefreien Periode gemessen. Alle CO2-Flüsse, sowie der NDVI wurden durch B-, S- und F-Behandlungen in Korrelation mit dem Stickstoffgehalt des Substrats erhöht. Erwärmung erhöhte CO2-Austausch und NDVI stärker als Laubaber weniger als Pilz-Zugabe. Daraus schließen wir, dass der zunehmende Streueintrag die Aktivität in Abhängigkeit von der Streuqualität steigern wird, wobei Erwärmung der kontrollierende Faktor für Tundra-Ökosysteme bleibt. Der Einfluss von W- und F-Manipulation war für alle Messgrößen statistisch signifikant ( $\alpha = 0,05$ ), außer für NEE. Jedoch wies NEE ähnliche Trends auf wie ER, GEP und NDVI und zeigte erhöhte CO2 Aufnahme des Ökosystems. Bodenparameter und extrazelluläre Enzymaktivitäten aus einer Probenentnahme im Sommer waren nach 6 Jahren Manipulation nicht verändert. Die Aktivität aller hydrolytischer Enzyme, mit Ausnahme der Phosphatase, waren in 5-10 cm Tiefe höher als in 0-5 cm. Dies deutet auf andere Nährstoffumsätze in verschiedenen Bodentiefen der Tundra und potentiell stärkerem Abbau von OBS unterhalb von 5 cm Bodentiefe hin.

CO2-Austausch, Enzymaktivität, subarktische Tundra, Klimaerwärmung, Streu-Zugabe

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## 1 Introduction

Climate change causes temperatures to rise and will alter ecosystems globally but will be especially pronounced in northern high latitudes (IPCC 2014). Arctic regions north of 67.5°N are estimated to face a more than 2 times stronger warming on a yearly average than global mean (IPCC 2013). Although strongly amplified warming can be accounted mainly to increased warming in winter, most climate simulations also result in above average temperature changes during summer in Scandinavia (Kjellström et al. 2018).

Arctic ecosystems belong to the least productive on the globe, but large amounts of carbon have accumulated in its soils, as respiration in the past was more inhibited than primary production (Shaver and Jonasson 2001). The combination of both large carbon stocks in arctic ecosystems and extraordinary exposure to warming and its resulting direct and indirect effects on ecosystems induces high concern about a possible positive climate change feedback and net carbon release to the atmosphere. However, enhanced carbon uptake through enhanced primary production due to climate change has been reported for the past as well (McGuire et al. 2009). Apart from faster respiration and photosynthesis through higher temperatures itself, carbon flux dynamics can be influenced by several changes in the ecosystem, such as prolonged growing season, vegetation shifts and subsequent changes in substrate inputs to ecosystems, altered biogeochemical cycles in soils, changes in precipitation patterns or herbivory pressure (Larsen et al. 2014).

## 1.1 Carbon fluxes in changing ecosystems

It is widely recognised, that respiration reacts more sensitive to warming than photosynthesis (Davidson and Janssens 2006), and this can be confirmed by experimental warming in field studies in the tundra (Biasi et al. 2008; Welker et al. 1999). Consequently, potential stronger carbon loss with higher temperatures than increasing carbon uptake through primary production may be expected. This however is maybe only true for labile fractions of SOM, and falls short regarding other environmental chemical constraints to decomposition, which could be further affected by climate change (Davidson and Janssens 2006). Also, primary production from ecosystems can be enhanced by increased temperatures at least for some plants or ecotypes and thus increase living plant biomass and counteract potential carbon losses from respiration of soils (Campioli et al. 2013; Welker et al. 2004).

Vegetation changes in arctic ecosystems have been reported over earlier warming periods (Larsen et al. 2014). Perennial shrub vegetation is expanding as result of climate change in tundra ecosystems (Hallinger and Wilmking 2011; Tape et al. 2006), such as on our study site close to Abisko in Sweden. Plant biomass is therefore likely to increase, and assimilated carbon will remain longer in the system with woody shrub vegetation, compared to graminoid or moss dominated tundra types (Campioli et al. 2009a).

Higher temperatures will further likely prolong the growing season as summarized by Linderholm (2006), again allowing plants to gain more biomass. However, changes in growing season length should be observed with caution, because local climate variabilities and other factors, such as changes in snow depths, could result in shortened growth seasons as well. Declining snow depths and shorter duration of ice cover on Lake Torneträsk (Callaghan et al. 2010) would also suggest lengthening of growing season at our research site in subarctic Sweden close to Abisko.

Apart from to the harsh climate, nitrogen is supposed to be the main limiting factor in tundra for both SOM decomposition (Mack et al. 2004) and plant growth (Jonasson et al. 1999). Thus available nitrogen can possibly amplify carbon release or uptake from the ecosystem (Weintraub and Schimel 2005a). In principle the main input of nitrogen to the ecosystem is through fixation by moss associated cyano-bacteria and is likely increasing with warming (Rousk and Michelsen 2017). But shrub expansion will also increase litter input and is a possible source of nutrients to the top layer of the soil and affect both respiration and photosynthetic production of the ecosystem.

Additional plant litter input also holds the potential for building up carbon stocks in soils. Cornelissen et al (2007) point out, that expanding deciduous shrubs could have a positive or negative feedback dependent on whether easier decomposed higher quality litter of forbs and graminoids, or more recalcitrant mosses will be replaced. The quality of the litter therefore seems to be of importance for carbon fluxes. Increased plant growth due to warming could possibly reduce nitrogen content of plant biomass, because of a dilution effect, thus also of the litter, although this is very species dependent and likely to be offset by increased nitrogen availability due to release from decomposed SOM in the long term (Turunen et al. 2009).

Decomposition of SOM could be also enhanced by additional labile carbon input, an effect named as priming, as litter input and root exudates could be increased, as result of higher plant productivity (Kuzyakov 2002). This would be confirmed by Hartley et al (2012) who observed bigger carbon stocks in soils of low productive tundra compared to the more productive mountain birch forests in the same region. In contrast a direct priming effect after labile carbon addition in tundra soils could not be observed by Lynch et al (2018) but microbial communities of shrub vegetation could reduce respiration of fresh carbon inputs compared to graminoid dominated soils. Rousk et al (2016)

reported rather selective mining for nutrients in SOM, but reduced overall decomposition of SOM in response to carbon input, giving potential of carbon accumulation in soils as result of shrub growth.

Considering the seasonal development of the ecosystem during growth season, it is not an easy task to make general conclusions of responses to climate change. Leaf Area Index (LAI) can be correlated to Normalized Difference Vegetation Index (NDVI) and changes along the short growing season of tundra ecosystems also differ for dominant species (Juutinen et al. 2017). LAI increases early after snow melt, especially for deciduous shrubs (Campioli et al. 2009b), while secondary growth and also leaf productivity of evergreen plants remains high through the whole growing season (Campioli et al. 2009a). Variation in nitrogen content of produced plant tissue at different times could change nitrogen demand during the season. Input of fresh nutrient rich litter occurs mainly in autumn, at a point of low nitrogen demand by plants. Nutrients, however, appear to be solubilized and accumulated during autumn and winter and are most available for assimilation into biomass by microbes and plants during snow melt, while depletion and hence competition is highest in mid-summer (Weintraub and Schimel 2005b). Temperature conditions, soil moisture and solar radiation are changing permanently according to actual weather conditions throughout the growing season and can readily affect the carbon flux dynamics at any point of time.

#### 1.2 Changes of potential enzymatic activities

Soil microorganisms play a crucial role in the decomposition of complex organic molecules for the purpose of cycling and provision of nutrients for assimilation into new biomass. To a large extent this is conducted by extracellular enzymes, mainly released by microorganisms, which decompose specific substrates in a kinetic cascade, controlled by environmental factors such as substrate, enzyme and product concentration, sorption and diffusion processes in soil, water potential, pH or temperature (Sinsabaugh and Follstad Shah 2012). Because of the comparably easy and reliable assessment methods of potential enzyme activities and their importance in organic matter metabolism, enzymes can be used as a valuable indicator for biological activity and biochemical processes in ecosystems (Nanniperi 2002). The resource allocation theory that enzymes are expressed as a response to nutrient limitation and resource demands for microbial growth (Sinsabaugh and Moorhead 1994) and can be confirmed by a recent comprehensive meta-analysis of 132 studies on natural ecosystems undergoing N or P addition treatments, among others (Xiao et al. 2018). According to Sinsabaugh and Follstad Shah (2012) this is most apparent for phosphorus cycling enzymes, though in principle also reported for enzymes associated with catabolism of nitrogen rich compounds, which are often simultaneously also a relevant source of carbon. Anyway, to draw clear

conclusions on the effect of the complicated interactions of C and N limitation on SOM decomposition in tundra is difficult. Low N availability is expected to limit decomposition of SOM, and N addition showed amplification of decomposition and associated extracellular enzymes (Koyama et al. 2013; Sistla et al. 2012). But theoretically, enhanced catabolization of organic carbon could also occur under nitrogen limitation and be reduced by N addition (Schimel and Weintraub 2003). This could also explain the observation of Melle et al. (2015), where nitrogen addition in arctic tundra soils did not increase carbon mineralization or growth of microbial biomass, although Melle et al. rather concluded carbon limitation in his study.

Temperature affects the in-situ degradation through enzymes in many ways. Increasing temperature generally fastens up the turnover rate of any biological process, as well as makes substrates and enzymes more soluble in soil water and enhance turnover in that way (Wallenstein et al. 2011). But also the production rate of exoenzymes is likely to increase with temperatures, and shift resources allocation of microbes towards enzyme production, thus increasing potential enzyme activity (Wallenstein et al. 2011). The meta analysis by Brzostek et al (2012) observed a global trend for increased proteolytic enzyme activities after experimental warming, especially in organic soils and in soils of higher northern latitudes. In the study of Sistla and Schimel (2013), increased enzyme activity was observed strongly in winter, but very weakly during the warmest month and if present only in mineral horizons. For Jing et al (2014) an increase of potential enzyme activity in response to warming treatment was not detectable. These results depict clearly that still uncertainties exist in which way extracellular enzyme expression is affected by enhanced temperatures.

As resource availabilities and demands moisture and temperature conditions change through the season it is of no surprise, that enzyme activities change permanently in dependence of environmental conditions and dominant vegetation. In tussock tundra potential enzyme activities peaked right before and shortly after snowmelt, while remained generally low with a slight increase along the growth period for shrub dominated tundra (Wallenstein et al. 2009). Similar peaks of hydrolytic enzymes during spring thaw were observed by Sistla and Schimel (2013) and could be explained by high nutrient availability after winter and increased nutrient demand during mid-summer for all tundra types, but also increased competition through the whole season by tundra typical shrub vegetation (*Betula nana*) which is very efficient in N uptake (Weintraub and Schimel 2005b).

#### 1.3 Aim of the Study

It is evident, that climate change will alter ecosystems globally, but especially in higher northern latitudes. If the large carbon stocks are affected by those changes, a feedback on CO<sub>2</sub> concentrations in the atmosphere and thus on global warming is likely. Although the scientific community is aware of that threat, the mechanisms causing either an increase or loss of biomass are only partly understood and possibly also unequal among different ecosystem types in the northern regions. It is further also difficult to extrapolate from single ecosystem processes to overall changes in the ecosystem. Therefore, analysis of carbon fluxes for different biomes on ecosystem level could help assessing possible feedback mechanisms.

The subarctic region around Abisko is undergoing typical changes of climate change, with rising temperatures, prolonged growth season and expansion of shrub vegetation in tundra areas. The experiment located in a mesic tundra heath close to the treeline of birch forest is exposed to 4 different treatments to resemble possible effects on the changing ecosystem.

Input of litter material and its quality appears to be of importance to decomposition processes in soil and nutrient availability to plants. Two treatments should reveal the effect of additional litter input of expanding shrubs (Birch and Willow) with two contrasting qualities, with Birch litter having a twice as high C:N ratio than Willow litter. A third treatment with substrate addition (fungal fruitbodies) was not considered to resemble increased fungal growth in tundra, rather than offering another but high-quality substrate with easily available nitrogen for an additional comparison to more recalcitrant shrub litter.

The warming treatment should give insights on changes in the carbon balance under elevated temperature conditions, probably the most obvious and direct effect of climate change.

Environmental parameters are changing either along with the growth season or from day to day dependent on actual weather conditions. Measurement of CO<sub>2</sub> fluxes therefore have been conducted from beginning of the growing season after snow melt until the end when first frost occurred and plants shed their leaves. A total number of 14 measurement rounds could disclose whether possible treatment effects on carbon flux dynamics are different at different time points in the season, under special environmental conditions or over all throughout the growth period after several years of treatment application.

Enzymes are an easy measurable indicator for resource demand and soil microbial activities in manipulated ecosystems and play a crucial role in decomposition of SOM. As a huge proportion of the measurable carbon exchange between the environment and the atmosphere are controlled by photosynthesis and respiration of plants and therefore possibly mask treatment effects on soil

respiration, an assessment of potential enzymatic activity should indicate whether treatments have also impact on organic matter decomposition in the soil. Although enzymatic activities change along with the season and environmental conditions as well, only one soil sampling for enzymatic activity assessment was conducted to reduce impact on treatment plots to a minimum extent and to allow relatively unaffected future research on these manipulation plots. The sampling was scheduled towards the end of the most active growth season in mid-summer, when nutrients are probably limited. Direct effects of fresh additional carbon inputs through litter are therefore unlikely and extracellular enzymes will hopefully give a clearer picture on enzyme activity in general due to alterations of the ecosystem after 6 years of manipulation.

## 1.4 Hypotheses

Based on above reported knowledge of past experiments and theories, I hypothesise that:

- Substrate addition will have a positive impact on Gross Ecosystem Production as well as Ecosystem Respiration. Effects will be relatively stronger with increasing N content of the substrate: Fungi > Salix > Betula.
- Warming will enhance Ecosystem Respiration to a stronger degree than photosynthesis, reducing Net Primary Production and thereby ecosystem uptake of carbon during the growing season.
- Additional available substrate enhances enzymatic activity in the top layers of soils. Relative to substrate quality, potential activity will be higher for nitrogen cycling enzymes for lower quality litter addition (*Betula*) and higher for phosphorus and carbon cycling enzymes for addition of N rich substrates (*Salix* and fungi fruitbody).
- Warmed plots will slightly enhance the potential activity of carbon cycling enzymes.

## 2 Methods

## 2.1 Site description

The experiment is located about 200 kilometers north of the Arctic Circle close to the scientific research station in Abisko, Sweden, which also records long term weather data. The annual precipitation is around 300mm and mean temperatures about 0.5 °C. The experiment is adjacent to the Birch forest tree line but contains solely tundra vegetation, mainly dwarf shrubs and mosses with some graminoids and forbs. Common ericoid dwarf shrubs are, *Vaccinium uliginosum, Empetrum hermaphroditum, Rhododendron lapponicum* and *Andromeda polifolia*, common non erocoid dwarf shrubs are *Betula nana, Salix myrsinites*, and *Dryas octopetala*. Typical moss vegetation contains *Dicranum* spp., *Tomentyphnum nitens* and *Hylocomium splende*ns (Rousk et al. 2016; Rousk and Michelsen 2017). The organic soil layer is 8-15cm deep with a pH of 6.7 ±0.03 (Rousk et al. 2016), and the bedrock material is a base-rich schist. There is no permafrost in the field site.



Figure 1: Field site in subarctic tundra adjacent to mountain birch forest treeline in autumn. (Photo: Balduin Landl)

### 2.2 Experiment setup

To simulate effects of global warming, 5 treatments have been established. The treatments are control (referred to as "C"), litter addition of birch leaves (*Betula pubescens* ssp. *tortuosa*; referred to as "Betula" or "B"), litter addition of willow leaves (*Salix myrsinifolia*; referred to as "Salix" or "S"), fungal fruitbody addition (mainly *Leccinum scabrum* referred to as "Fungi" or "F") and warming treatment (referred to as "W" conducted by open top chambers.

The treatments where applied to 1x1m plots on the tundra vegetation in a randomized block design with 6 replicates. First Betula, Salix and Fungi applications have been conducted annually in autumn with 90g dw m<sup>-2</sup> yr<sup>-1</sup> of litter and 90g dw m-2 yr<sup>-1</sup> fresh weight of fungi since 2011. The C:N ratio of the added substrate was  $45 \pm 4.1$  for Betula,  $22 \pm 1.3$  for Salix (mean  $\pm$  se, n = 3) and for the Fungi 11.25. Fungi is expected to reduce nitrogen limitation in the ecosystem. Treatment application in 2017 was conducted on 30th of August.

The warming is established with open top chambers (OTC) which side walls are assembled as a hexagonal frustum of 35cm height and a diameter of 150cm at bottom and 85cm at top with 3mm thick transparent acrylic glass. The OTCs are in place throughout the whole year since May 2012 and led to an annual temperature increase of the soil surface of 0.7°C and 1.8°C during the snow free period. All measurements and samplings in 2017 have been conducted in the 6th year of treatment.

At each plot a 33 x 33 cm squared metal frame is permanently installed to allow closure of the manipulated ecosystem for gas flux measurements. The metal frame can be filled with water to seal the gap between CO<sub>2</sub> flux chamber and frame and prohibit gas exchange.



Figure 2: Warming treatment plot with OTC and 33 x 33 cm metal frame for CO<sub>2</sub> flux measurements. (Photo: Anne Schäfer)

## 2.3 CO<sub>2</sub> flux measurements

CO2 fluxes of each climate change manipulation plot have been measured 14 times during the snow free period between 24<sup>th</sup> of May and 19<sup>th</sup> of September. The average measurement interval was 9 days but not fully consistent due to weather limitations. One whole set of measurements (all 30 manipulation plots) required 2 consecutive working days of similar environmental conditions which was tried to be assured at its best. All 5 different treatment plots per block were measured in one series to achieve best comparability of the treatments. The measurements of the blocks were conducted in ascending order for the first three measurements (24 May, 2 Jun, 16 Jun) and since then randomized for the following 11 measurements (28 Jun - 19 Sep). The net ecosystem CO<sub>2</sub> exchange (NEE) was measured by placing a cubic transparent acrylic glass chamber of 33cm side length on the installed metal frames and sealed with water for minimum 3 and maximum 7 minutes depending on environmental conditions. The change in CO2 concentration in the closed system was recorded by an infra-red gas analyser EGM 4 (PP Systems, Amesbury, USA) connected to the chamber every 1.6 seconds. Additionally, temperature, relative humidity, atmospheric pressure and

photosynthetically active radiation (PAR) were recorded by the EGM-4 probe in the chamber. Soil moisture (3 places), soil temperature at 2cm and 5cm were measured manually in the manipulation plots, but outside the chamber frame to avoid disturbance of the plot area used for carbon flux measurements. Normalized Differential Vegetation Index was measured disturbance free with a hand-held device of the area within the chamber frame (3 replicates).

After a NEE measurement of each plot a subsequent ecosystem respiration (ER) measurement was conducted by shortly removing and replacing the chamber but covered with a cardboard box and a black cloth, to prohibit photosynthesis.

The CO2 concentration changes were used to calculate the CO2-flux ( $\mu$ mol CO<sub>2</sub> h<sup>-1</sup> m<sup>-2</sup>) of NEE and ER under given conditions with MS Excel using following formula,

$$CO_2 flux = \frac{slope * volume * pressure}{area * temp * R} * 360$$

with slope ( $\mu$ mol mol<sup>-1</sup> s<sup>-1</sup>) as the concentration change in the chamber, volume (m<sup>3</sup>) as the volume of the chamber, pressure (Pa) as the pressure in the chamber, area (m<sup>2</sup>) as the ground area of the measured plot, Temp (K) the temperature in the chamber and the universal gas constant R (8.31446 kg m<sup>2</sup> s<sup>-2</sup> K<sup>-1</sup> mol<sup>-1</sup>).

Gross ecosystem production (GEP) was calculated from NEE-flux and ER-flux with following formula

$$ER - GEP = NEE$$



Figure 3: Transparent gas flux measurement chamber for NEE measurement on metal frame connected to EGM-4 and laptop in early spring (Foto: Anders Michelsen)

## 2.4 Soil sampling

Soil samples were collected once on August the 3<sup>rd</sup> in 2017. Two cores per plot were taken with a 37mm diameter auger and divided in 5cm sections. In the research station lab in Abisko, soils were weighted for estimation of bulk density. Soil cores of same depth and plot have

been homogenized and roots picked out manually. Sieving the samples was not possible due to the high organic matter content and high water content at time of sampling. Root biomass of fine roots <1mm and coarse roots >1mm were determined separately. 5g fresh soil per sample were used for determining gravimetric water content, by weighing after 48h drying in oven at 60°C. 3g subsamples were frozen and transported to Vienna for later potential enzyme activity analysis. The rest of the soil samples were transported to Copenhagen for analysis of carbon and nitrogen content.

#### 2.5 Enzyme activity assessment

Potential enzyme activity in 0-5cm and 5-10cm depth of each plot was assessed in the laboratory of the Institute of Soil Science at University of Natural Resources and Life Sciences Vienna (BOKU). Fluorometric assays were conducted following the standard protocol used by BOKU for extracellular enzyme activities assay after (German et al. 2011; Sinsabaugh et al. 1999) for following enzymes:  $\beta$ glucosidase (BG),  $\beta$ -Xylosidase (BX),  $\beta$ -N-Acetylglucosaminidase (NAG), Acid Phosphatase (AP),  $\beta$ -D-Cellubiosidase (CB) using Methylumbelliferyl (MUF) linked Substrates and for Leucine Aminopeptidase (LAP) using Leucine-Aminomethylcoumarin (AMC) as substrate.

1 gram of soil was suspended in 100ml sodium acetate buffer (50mM) at environmental pH 6,7 (Rousk and Michelsen 2017) and homogenised with ultrasonicator for 40 seconds. Stock solutions with the respective substrates for each enzyme where prepared to guarantee excess availability for extracellular enzymes. Substrates and soil suspension were pipetted together with 4 replicates for each sample on microtiter plates, together with a few representative quenched MUF and AMC standards and standards in pure buffer solution, as well as buffer control, substrate control. The microtiter plates were incubated for 120min at 20°C and fluorescence of the metabolized substrate measured on a fluorescence spectrophotometer (Perkin Elmer EnSpire Plate Reader) with an extinction wavelength 365nm and Emission wavelength 450nm and 30 flashes. Potential enzyme activity was calculated with slightly adapted formulas of German et al. (2011) as follows.

Activity (nmol  $g^{-1} h^{-1}$ )

= <u>Net fluorescence \* Buffer volume(mL)</u> = <u>Emission coefficient \* Homogenate volume [mL] \* Time[h] \* Soil mass[g]</u>

Net fluorescence =  $\left(\frac{Assay - Homogenate \ control}{Quench \ coefficient}\right)$  - Substrate control

 $Emission \ coefficient \ [fluorescence \ nmol^{-1}] = \frac{Standardcurve \ slope(buffer) \left[\frac{Fluorescence}{nmol \ mL^{-1}}\right]}{Assay \ volume[mL]}$ 

$$Quench \ coefficient \ = \ \frac{Standarccurve \ slope \ (homogenate)}{Standardcurve \ slope \ (buffer)}$$

Activity of oxidative enzymes, Phenoloxidase and Peroxidase were assessed by using L-3,4dihydroxyphenylalanin (DOPA). Soil suspension or sodium acetate buffer for blanks have been pipetted with DOPA in 2ml-Eppis, mixed for 20s on a Vortexer and centrifuged at 5000 rpm for 5 min. 3 replicates of each sample and blank where transferred on two transparent microtiter plates respectively, one with additional 10µL of 0.3% H2O2 to enable additional Peroxidase activity in reaction wells. Absorption was measured with the Perkin Elmer EnSpire Plate Reader, first right after pipetting and again after 20h incubation at 20°C at at 450 nm wavelength. Calculation of oxidative enzyme activity is based on (2011).

Activity( $\mu$ mol  $g^{-1}h^{-1}$ )

= <u>Net absorbance \* Buffervolume[mL]</u> <u>Extinctioncoefficient \* HomogenateVolume[mL] \* Time[h] \* Soilmass[g]</u>

Net absorbance = Assay  $t_{20}$  - Blank control  $t_{20}$  - Assay  $t_0$  - Blank control  $t_0$ 

*Extinctioncoefficient* = 0.445[absorbance/µmol]

Phenoloxidase activity could be assessed and calculated in this way, while Peroxidase activity could be assessed separately but together with Phenoloxidase in the same wells with added Hydrogen Peroxide. Hence, Peroxidase activity hat to be calculated by substraction of Phenoloxidase activity from activities of both oxidative enzymes together.

 $Activity_{Peroxidase} = Activity_{Phenolox.+Perox.} - Activity_{Phenoloxidase}$ 

### 2.6 Statistical analysis

Statistical analysis of treatment and additional measured variables impact on NEE, GEP, ER, enzyme activities and soil parameters was conducted with Rstudio statistic software.

Effect of treatment on CO<sub>2</sub> fluxes was modelled with generalized linear mixed effect models, for different seasons (spring: 24 May - 17 Jun, summer: 28 Jul - 27 Aug, autumn: 4 Sep - 20 Sep) and whole season where applicable. At least 2 measurements in autumn (4/5 Sep and 11/12 Sep) were influenced by application of litter and fungi treatments a few days earlier and therefore only warming and control plots were modelled for autumn season. The two influenced measurement

rounds starting 4 and 11 September were further excluded for the whole season models. Effect of block was included in the model if it expressed a likely impact on the flux (p < 0.2). Plot ID was included as random effect to account for repeated measures on the same plots throughout the whole season. Validity of models were assessed visually, with normal Q-Q plots and observed vs fitted residual plots. Log transformation of fluxes was conducted if necessary to meet model assumptions.

For soil parameters and enzymatic activities, 2- or 3-way ANOVAs have been conducted, with treatment, block (if p < 0.2) and if applicable depth as factors. Soil variables where tested for each depth layer in 5cm intervals down to 20 cm depth. Soil cores of only 8 plots reached a depth below 20 cm, therefore only summary statistics, but no statistical analysis was performed for soil depth 20-25 cm. Enzymatic activity assays were only conducted for top soil layers in 0-5cm and 5-10cm depth. MANOVA was conducted for functional grouped enzymes to assess treatment effects of several enzymes in combination. Multivariate normality was tested with Shapiro-Wilk-Test as well as visually with Q-Q plots. For grouped enzymes which appeared to show interesting results for MANOVA analysis Linear Discriminant Analysis (LDA) was conducted as follow up analysis, to assess graphically patterns of treatment influence on ecoenzyme expression.

## **3** Results

#### 3.1 Soil Characteristics

#### 3.1.1 Characteristics of the soil profile

The depth of the soil at the field site showed high variability for individual plots. Depths from the 60 soil cores taken beginning of August 2017 ranged from only 8cm to 25cm, depending upon presence of stones and the depth of the bedrock. There was no permafrost at the site. Soil depths were distributed randomly among the site, as a spatial influence of the soil depth could not be observed by ANOVA. The first 5 cm or 10cm of the profile contained a large amount of weakly decomposed organic material, as for example mosses. The upper layers were penetrated with fine roots (<1mm) and coarse roots ( $\geq$ 1mm) more than the soils in deeper layers which were still rich in organic matter but consisted more of dark, well decomposed organic material. Carbon content was almost 40% in top 5cm and declined with depth to slightly above 30% for the deeper layers. Nitrogen content is lowest in the top layer of the soil but remains steady at approximately 2% for the rest of the profile below 5cm. The C to N ratio therefore declines from 28 to 16 from top to 15cm depth but from that point remains steady further down in the profile. Also, gravimetric water content of sampled soil declined continuously with depth. Bulk soil densities of those high organic soil cores were generally low but increased with depth from 0.05 g cm<sup>-3</sup> at the top to 0.22 g cm<sup>-3</sup> at the bottom. Biomass of both fine roots (<1mm) and coarse roots (≥1mm) is highest in the top layers and declines continuously with depth. While coarse root biomass is bigger in the first 10cm, at depth 10-15cm coarse root biomass almost equals fine root biomass and is even lower in the deep soil layers. Twoway ANOVAs do not indicate any effect of treatment on any of the described soil parameters, 6 years after first application, in each 5cm layer of the soil. Statistical tests, integrating all soil layers within 0-10cm or 0-20cm with treatment, block and depth as factors result in significant influence of depth only, but no significant effect of treatment. An exception to this is soil nitrogen content if modelled over the whole profile depth of 0-20cm.

	0 - 5 cm	5 - 10 cm	10 - 15 cm	15 - 20 cm	20 - 25 cm
Bulk soil density (g cm <sup>-1</sup> )	0.05 (0.01)	0.10 (0.01)	0.14 (0.01)	0.20 (0.03)	0.22 (0.03)
Water content (g $H_2O$ g Soil <sup>-1</sup> )	386.1 (23.1)	370.6 (27.5)	341.1 (23.7)	283.7 (16.7)	264.9 (25.4)
Carbon content (%)	39.98 (0.22)	36.98 (0.65)	33.86 (0.78)	31.84 (0.95)	31.94 (1.69)
Nitrogen content (%)	1.46 (0.04)	1.97 (0.06)	2.11 (0.06)	1.99 (0.07)	2.0 (0.13)
C:N ratio	27.70 (0.72)	19.51 (0.60)	16.24 (0.43)	16.12 (0.41)	16.21 (0.76)
Fine root biomass (g dm <sup>-1</sup> )	4.74 (0.32)	2.93 (0.14)	1.47 (0.12)	0.90 (0.11)	0.90 (0.26)
Coarse root biomass (g dm-1)	7.65 (0.67)	4.52 (0.60)	1.75 (0.38)	0.32 (0.12)	0.10 (0.08)

Table 1: Soil characteristics in various depths, (mean  $\pm$  se; 0-5cm n=30, 5-10cm n=30, 10-15cm n= 29, 15-20cm n=23, 20-25cm n=8)

A general linear mixed effect model returns a tendency towards an effect of treatment on nitrogen content (p= 0.052), lower in control plots than in the B treatment ( $\alpha$ =0.05) and in the F treatment ( $\alpha$ =0.1). The higher nitrogen levels in plots with treatment are more pronounced in lower depths of 10-20cm (Figure 4).



Figure 4: Carbon content, Nitrogen content and C:N ratio of soil in various depths (mean  $\pm$  se,  $6 \ge n \ge 5$ , but  $n_{C.15-20} = 4$ ,  $n_{S.15-20} = 3$ )

#### 3.1.2 Soil temperature and moisture during flux measurements throughout the season

The soil water content in the top 6 cm changed throughout the growing season between  $19.9 \pm 1.5$  vol % (mean ± SE, n=30) on July 28 and  $97.5 \pm 3.1$  vol % (mean ± SE, n=30) on July 15 where the site was partly flooded after heavy rainfalls. Partly flooding of the site resulted to few erroneous

moisture measurements of more than 100% volumetric water content. A soil moisture gradient was present from East to West side of the site with a significant higher soil water content on the 3 blocks on the East side from spring until summer (25 May – 15 August, p<0.001) which changed in the comparable dry period later in the season (26 Aug – 19 Sep, p<0.001) where water content was higher in the West. Soil moisture showed a very weak response to treatment over the whole season if the moisture gradient was included as East/West factor variable in a linear model (p=0.072). Tukey pairwise comparison resulted in higher moisture content of *Salix* compared to *Betula* litter treatment only on  $\alpha$ =0.1 level.

Soil temperatures fluctuated over the whole growing season according to weather conditions. Based on soil temperature measurements during each flux measurement, no treatment effect was observed during the time periods spring, summer and autumn or at single measurement days, except on 11 September (p=0.016) with open top chambers (warming) being warmer than B and S treatment (1.4 and 1.1°C respectively). However, soil temperature was significantly enhanced by warming over the whole season, if PAR (measured in transparent chamber) and daytime, as a surrogate for change in ambient temperature, is included in the generalized linear mixed effect model. Temperature was enhanced by 1.1 °C in 2 cm depth (p=0.014) and by 0.9 °C in 5 cm depth (p=0.018).



Figure 5: Seasonal development of:  $CO_2$ -fluxes: Ecosystem Respiration = positive values, Gross Ecosystem Photosynthesis = negative values, Net Ecosystem Exchange (positive values =  $CO_2$  release, negative values =  $CO_2$  uptake by ecosystem), for different treatments (mean ± SE, n=6) and additional Variables: PAR in Chamber (transparent) during flux measurements (mean ± SE, n=30); Mean temperature in Chamber (dark), 2cm and 5cm soil depth during flux measurements (mean, n=30); Normalized Differential Vegetation Index for different treatments (mean ± SE, n=6), NDVI data for 24 May is missing, note that scale does not start with 0.



Figure 6: Seasonal development of: Soil temperature during flux measurements in 2cm and 5cm depth for different treatments (mean  $\pm$  SE, n=6); Soil moisture on flux measurement days for different treatments (mean  $\pm$  SE, n=6)

### 3.2 CO<sub>2</sub> fluxes

### 3.2.1 Ecosystem Respiration (ER)

Ecosystem respiration is significantly influenced by treatments throughout the whole growing season (Table 2, Figure 7). F and W treatment plots show higher activity compared to control plots similar in spring, summer and over the whole season. Measurements on 4 and 11 September were not included in the whole season model because of obvious strongly enhanced respiration due to fresh litter and fungal fruit body application on B, S and F treatment plots. Only W treatment was compared to control in autumn season and showed a significant enhancement of respiration.

Table 2: Treatment effects on Ecosystem Respiration compared to control: p-values for Dunnett's test for generalized mixed effect models estimated marginal means. For autumn, B, S and F treatment excluded from model and for whole season, measurements on 4 and 11 of September excluded, due to influence of treatment application. Significant treatment effects in bold, indicated by:  $^{+}p \le 0.1$ ,  $^{*}p \le 0.05$ ,  $^{**}p \le 0.01$ .

	В	S	F	W
Spring (24 May - 16 Jun)	0.668	0.248	0.001 **	0.002 **
Summer (28 Jun - 26 Aug)	0.397	0.307	0.002 **	0.004 **
Autumn (4 Sep - 19 Sep)	-	-	-	0.007 **
Whole Season (24 May - 19 Sep)	0.400	0.236	0.001 **	0.001 **



Figure 7: ER of different treatments at different seasons, mean  $\pm$  SE (mg CO<sub>2</sub> h<sup>-1</sup> m<sup>-2</sup>). Spring: 24 May, 2 and 16 Jun. Summer: 28 Jun - 26 Aug (8 measurement rounds). Autumn: 4, 11 and 19 Sep (B, S and F treatment excluded from model due to treatment application impact). Whole season: 24 May - 19 Sep, (12 measurements, 4 and 11 Sep excluded due to treatment application impact). Letters indicate significant differences between treatments after Tukey pairwise comparison of estimated marginal means ( $\alpha$ =0.05).

#### 3.2.2 Gross Ecosystem Photosynthesis (GEP)

Early in the season warmed plots showed increased activity compared to the control plots. Photosynthesis remained rather high over the whole season, but shows now significant difference to other treatments, but to the *Betula* addition treatment during autumn. Although photosynthesis activity of F treatment plots dropped slightly below the W treatment in spring, F and W are clearly most productive treatments during the whole season and the only treatments with a significant treatment effect compared to controls. Litter addition treatment plots B and S showed no significant treatment effect but the trend for intermediate productivity between the lower C and higher F and W plots is visible. (Table 3, Figure 8)

Table 3: Treatment effects on Gross Ecosystem Photosynthesis compared to control: p-values for Dunnett's
test for generalized mixed effect models estimated marginal means. Significant treatment effects indicated
by: ⁺p ≤ 0.1, * p ≤ 0.05, ** p ≤ 0.01

	В	S	F	W
Spring (24 May - 16 Jun)	0.985	0.721	0.206	0.018 *
Summer (28 Jun - 26 Aug)	0.902	0.769	0.016 *	0.067 +
Autumn (4 Sep - 19 Sep)	0.630	0.899	0.034 *	0.167
Whole Season (24 May - 19 Sep)	0.999	0.803	0.024 *	0.066 +



Figure 8: GEP of different treatments at different seasons, mean  $\pm$  SE (mg CO<sub>2</sub> h<sup>-1</sup> m<sup>-2</sup>). Spring: 24 May, 2 and 16 Jun. Summer: 28 Jun - 26 Aug (8 measurement rounds). Autumn: 4, 11 and 19 Sep. Whole season: 24 May - 19 Sep (14 measurements rounds). Letters indicate significant differences between treatments after Tukey pairwise comparison of estimated marginal means ( $\alpha$ =0.05).

#### 3.2.3 Net Ecosystem Exchange (NEE)

No significant treatment effect could be observed by the models, although enhanced carbon uptake from W and F plots can be observed visually over the whole season (Figure 9). Covariates as Photosynthesis Active Radiation, temperature in chamber during measurement and soil temperature improved the model fit but did not influence treatment response. Spatial effects from block was not included, except in the model for spring, as it showed no effect on NEE (p>0.2). During the first two measurement rounds (24 May and 2 June) NEE was very close to zero but slightly positive for warming (Figure 5), but strong CO<sub>2</sub> uptake un 16 June turned the ecosystem into a net carbon sink already in spring. Also, the autumn season remains a net carbon sink until the the last measurement day, although on the second last measurement round 11 September respiration equaled primary production for C, S and W treatment plots and was a source of carbon for B and F plots. It must be recognised, that NEE of B, S and F treatment plots is influenced by enhanced respiration at least on 4 and 11 September due to substrate application shortly before and were therefore not analysed in the model.

Table 4: Treatment effects on Net Ecosystem Exchange compared to control: p-values for Dunnett's test for generalized mixed effect models estimated marginal means. For autumn, B, S and F treatment excluded from model and for whole season, measurements on 4 and 11 of September excluded, due to influence of treatment application. Significant treatment effects in bold, indicated by:  $p \le 0.1$ ,  $p \le 0.05$ ,  $p \le 0.01$ .

	В	S	F	W
Spring (24 May - 16 Jun)	0.987	0.967	0.764	0.555
Summer (28 Jun - 26 Aug)	0.996	0.950	0.063+	0.288
Autumn (4 Sep - 19 Sep)	-	-	-	0.525
Whole Season (24 May - 19 Sep)	0.982	0.963	0.103	0.216



Figure 9: NEE of different treatments at different seasons, mean  $\pm$  SE (mg CO<sub>2</sub> h<sup>-1</sup> m<sup>-2</sup>). Spring: 24 May, 2 and 16 Jun. Summer: 28 Jun - 26 Aug (8 measurement rounds). Autumn: 4, 11 and 19 Sep (B, S and F treatment excluded from model due to treatment application impact). Whole season: 24 May - 19 Sep (12 measurements, 4 and 11 Sep excluded due to treatment application impact). Letters indicate significant differences between treatments after Tukey pairwise comparison of estimated marginal means ( $\alpha$ =0.05).

### 3.3 Normalized Differential Vegetation Index (NDVI)

In the early season the F treatment plots appear to have a higher NDVI with a significant difference to the generally low NDVI of the *Betula* treatment. During summer also the NDVI of the warming plots was significantly higher than the control. In the autumn when leaf senescence started, a difference in NDVI cannot be confirmed by the statistical models anymore on  $\alpha$ =0.05 level, although the patterns of higher and lower NDVIs did not change on visual impression.

Table 5: Treatment effects on Normalized Differential Vegetation Index compared to control: p-values for Dunnett's test for generalized mixed effect models estimated marginal means. For autumn, B, S and F treatment excluded from model and for whole season, measurements on 4 and 11 of September excluded, due to influence of treatment application. Significant treatment effects in bold, indicated by:  $*p \le 0.1$ ,  $*p \le 0.05$ ,  $**p \le 0.01$ .

	В	S	F	W
Spring	0.819	0.992	0.098	0.646
Summer	0.970	0.365	0.003	0.020
Autumn	0.977	0.844	0.093	0.195
Whole Season	0.999	0.474	0.003	0.027



Figure 10: NDVI of different treatments at different seasons, mean  $\pm$  SE (mg CO<sub>2</sub> h<sup>-1</sup> m<sup>-2</sup>). Spring: 2 and 16 Jun. Summer: 28 Jun - 26 Aug (8 measurement rounds). Autumn: 4, 11 and 19 Sep. Whole season: 24 May - 19 Sep (14 measurement rounds). Letters indicate significant differences between treatments after Tukey pairwise comparison of estimated marginal means ( $\alpha$ =0.05).

### 3.4 Potential Enzyme Activity

 $\beta$ -Xylosidase and  $\beta$ -C-Cellubiosidase activity is very low close to the limit of detection. But since they express a very similar pattern, which appears to be not random variation, results are still considered as trustworthy. Potential activity of  $\beta$ -Glucosidase  $\beta$ -N-Acetylglucosaminidase Acid Phosphatase and Leucine-Aminopeptidase were higher in general (Figure 12). The potential enzyme activity of all six enzymes changed significantly with depth. All measured enzymes activities were higher in 5-10 cm depth compared to the top 5 cm layer, except for Phosphatase which was more active close to the surface. The control plots appeared to be lower in activity compared to any other treatment for most of the enzymes in the top 5 cm of the soil. This pattern seemed not to be repeated in 5-10 cm depth where especially activity of warmed plots usually was equal to or below control plots. Treatments where substrate has been added (B, S and F) enzyme activities appeared to be still slightly higher also in 5-10 cm, with the exception of NAG in which the control plots showed the highest activity.



Figure 11: Potential activity of enzymes in 0-5cm depth. Note different scale for BX and CB (left) and BG, NAG, AP and LAP (right), (mean±SE, n=6)



Figure 12: Potential activity of enzymes in 5-10 cm depth. Note different scale for BX and CB (left) and BG, NAG, AP and LAP (right), (mean±SE, n=6)

Statistically testing the potential enzyme activity with two- and three-way ANOVAS revealed no significant effect of 6 years of treatment application on enzyme activity. NAG in 0-5cm depth is the only enzyme which showed a tendency towards an effect (Table 6). A pairwise comparison after Tukey could not reveal any differences between treatments.

	0 – 5 cm		5 - 10 cm		0 – 10 cm		
Enzyme	Treatment	Block	Treatment	Block	Treatment	Block	Depth
BX	0.596	-	0.605	0.147	0.277	-	<0.001 ***
СВ	0.396	-	0.300	-	0.221	-	<0.001 ***
BG	0.397	0.012 *	0.248	-	0.152	0.084 +	0.006 **
NAG	0.051 +	0.072 +	0.338	-	0.285	-	<0.001 ***
AP	0.447	0.020 *	0.274	-	0.168	0.022 *	<0.001 ***
LAP	0.256	-	0.741	0.190	0.842	-	<0.001 ***

Table 6: Two-way ANOVA results on potential enzyme activity effects of treatments and block in several depths of soil (0-5cm and 5-10cm), 3 way ANOVA results including depth as variable and error term for plot ID to account for measurements in two depths on same plot on top 10 cm of soil.

To analyse the effect of treatment on several enzymes in combination, several different statistical methods have been conducted. Enzymes where grouped as follows: All enzymes together, C-cycling enzymes (BX, CB, BG), N-cycling enzymes (NAG, LAP), Nutrient-cycling enzymes (NAG, AP, LAP), and enzymes with relatively high activity (BG, NAG, AP, LAP) compared to BX and CB. Summing up several enzymes activities per plot does not make any treatment effects visible for any of the grouped enzymes and two different depths. MANOVA analyses were conducted to investigate potential treatment effects over several enzymes together. Tendencies for treatment effect on nutrient cycling enzymes are visible. Enzyme activity data were log transformed for all enzymes, but for C-cycling enzymes at depth 5-10cm. The model assumption of multivariate normal distribution of dependent variables, observed with Shapiro-Wilk test and visually with normal QQ-plots, were still often not met. Block had impact on all MANOVA models and was therefore included in the models.
Table 7: p-values for MANOVA analysis for treatment effect on several grouped Enzymes; p-value for Shapiro-Wilk-Test (multivariate normality given if  $p \ge 0.05$ ); visual interpretation of Q-Q plot for multi variate normality.

	0 – 5 cm			5 - 10 cm				
Enzyme cluster	TreatmentShapiro-WilkVisual modeleffectTestcheck		Treatment effect	Shapiro-Wilk Test	Visual model check			
All Enzymes	0.219	0.0001	poor	0.167	0.001	poor		
C-cycling Enzymes (BX, CB, BG)	0.376	0.133	ОК	0.225	0.127	poor		
N-cycling Enzymes (NAG, LAP)	0.165	0.077	poor	0.141	0.005	poor		
N,P-cycling Enzymes (NAG, AP, LAP)	0.094 +	0.0001	ОК	0.087 +	0.011	ОК		
High activity Enzymes (BG, NAG, AP, LAP)	0.221	0.0001	poor	0.103	0.001	ОК		

Expressing the enzyme activities per g soil carbon, instead of soil, does not affect the results of the tests to a relevant degree, as soil carbon content is very similar among all plots. Variance of nitrogen content and C:N ratio is higher, hence test results change to some degree if activities are divided by the C:N ratio or calculated as activities per g Nitrogen. ANOVAs on transformed potential enzyme activities do not indicate treatment effects (data not shown). MANOVA results however indicate a treatment effect on potential activities relative to C:N ratio on some enzyme clusters. Examples therefore would be enzymes with higher activity BG, NAG, AP and LAP divided by C:N ratio in depth 5-10 cm (p=0.064) or nutrient cycling enzymes NAG, AP and LAP divided by C:N ratio in 5-10cm depth (p=0.042). In both cases the Shapiro-Wilk-test and visual interpretation of residual plots and Q-Q plots suggest multivariate normality.

A Linear Discriminant Analysis have been further conducted complementary to the MANOVA models, to check in which way the treatments possibly change the activity of grouped enzymes. On the new calculated linear discriminant axes on the biplot a clear grouping of the individual treatments is not visible, indicating that treatment effects are not visible after 6 years of treatment yet.



Figure 13: Biplot of Linear Discriminant Analysis for nitrogen and phosphor cycling enzymes (NAG, AP, LAP) at two different depths (0-5cm, 5-10cm). Each datapoint depicts one experimental plot with a specific treatment. Direction and length of vectors indicate influence of the potential activity of the respective enzyme on the position of each plot on the 2 plotted new calculated linear discriminant axes.



Figure 14: Biplot of Linear Discriminant Analysis for potential enzyme activity relative to C:N ratio. enzymes with high activity (BG, NAG, AP, LAP) in 5-10cm depth and nutrient cycling enzymes (NAG, AP, LAP) at 5-10cm depth. Each datapoint depicts one experimental plot with a specific treatment. Direction and length of vectors indicate influence of the potential activity divided by C:N ratio of the respective enzyme on the position of each plot on the 2 plotted new calculated linear discriminant axes.

#### 3.4.1 Oxidative Enzymes

Peroxidase activities were in the negative range in 0-5cm soil depth. Both, Peroxidase and Phenoloxidase expressed very high variations within each treatment. Results of the oxidative enzymes were therefore considered as untrustworthy, probably due to methodological problems, and henceforth not considered any further. See supplementary graphs in the Appendix (S.Figure 1)

### 4 Discussion

#### 4.1 Soil properties

#### 4.1.1 Soil samples

The decline in carbon content with depth is common due to higher mixing with mineral substrate from the bottom and can be seen also in another experiment nearby, in a more wet heath type (Phillips et al. 2018). Interestingly at this site the carbon stocks differed with treatment and significant losses of carbon pools were observed in warmed plots after 16 years of treatment, which was not the case after only 7 years of treatments (Rinnan et al. 2008) and is apparently also not detectable at our site after 6 years of treatments. As losses through enhanced respiration of organic carbon or through lateral waterflow of dissolved organic carbon (Pedersen et al. 2017; Phillips et al. 2018) is taking place over longer time spans, the possibility of changing carbon stocks according to treatments at our field site can of course be not excluded, although relevant carbon losses at our dryer site through lateral waterflow are less likely.

A relative lower total nitrogen content in the soil close to the surface relative to deeper layers was also observed in other studies close by (Phillips et al. 2018; Rinnan et al. 2008) and can be probably accounted to the enhanced decomposition and nutrient uptake in this more active layer with higher root density. The resulting high C:N ratio fits well to the selective mineralization of N rich compounds of SOM observed by Rousk et al. (2016) with higher availability of labile carbon, which should be the case in the upper soil due to root exudates and litter input.

Difficult to answer is the observed higher total nitrogen levels of all treatment plots compared to control plots (Figure 4). A possible source of nitrogen is of course the substrate added with treatments B, S and F, and in fact the nitrogen content of the top 5 cm of the soils apparently increases slightly, in accordance with the nitrogen content of the added substrate. Enhanced nitrogen content in the top soil of warming treatment plots could possibly be explained by enhanced N<sub>2</sub> fixation, observed in previous studies in this region (Lett and Michelsen 2014; Rousk and Michelsen 2017). Another possibility is of course, that enhanced plant growth in warming treatment relocated nitrogen to the top layer, by uptake from deeper soils and partially return of N in aboveground biomass again with litter fall. These changes in total N in the top layer of the soil do follow a treatment pattern, but are anyhow not statistically significant and the explanations are rather insufficient for the varying nitrogen contents between treatments in deeper plots, where

lower nitrogen of control plots is most obvious. In these deeper layers however, not only the nitrogen content but also carbon content of control plots appears to be much lower and both are subject to much higher variation than the treatment plots. As we sampled the soils all the way down to the mineral bedrock, it is possible that considerably high amounts of mineral soil substrate were mixed with the rather high organic soil samples at the bottom end of the soil cores, although we carefully removed the grey sandy and silty mineral material. The soil depths were between 10 and 25 cm, thus influenced single samples at different depths. Testing treatment effect on nitrogen content was only significant if modelled over the whole profile depth of 20 cm and further very sensitive to removal of single datapoints with remarkably low SOM content. Although we observed no significant differences between treatment plots for soil depth, I assume that by chance control plots were more mixed with mineral bedrock than treatment plots, for which treatments cannot be accountable. Therefore, the visibly lower nitrogen contents of control and its confirmation by statistical tests should not be overrated especially in deeper soil layers. Still, the nitrogen content, hence also C:N ratios of the top 5 cm fits very well within the treatment response pattern also of carbon fluxes and NDVI measurements (see discussion of CO<sub>2</sub> fluxes)

In contrast to our samples, the soil samples of the same plots 3 years earlier observed significant higher amounts of carbon and nitrogen in the organic horizon of the litter addition treatments (Rousk et al. 2016; fungi treatment plots not reported). Three possible explanations could have led to this discrepancy between visible treatment effects after 3 years, but not after 6 years of plot manipulations. In the earlier study, a higher number of 6 soil cores were sampled per plot and maybe achieve a higher representativeness of the soil properties in contrast to the 2 soil core sampling we conducted 3 years later, in order to reduce destructive impact on the experiment. Rousk et al. (2016) further reported the differences for samples of the whole organic horizon which was reported to be 8-15 cm in depth, and did not strictly dissect the soil cores into 5cm sections, regardless of the soil profile depth, as we did. A third explanation could be, that the additional carbon and nitrogen observed by Rousk was derived from the additional added litter itself, and to a lesser extent from increased litter fall of enhanced plant growth of the warmed plots, which showed a slightly and less significant increase in organic carbon and nitrogen stocks in the earlier study as well. However, it does still not sufficiently explain why this effect was not observable after 3 more years of treatment.

The biomass of fine and coarse root as well as the decline with depth is well in line with the results from the wetter subarctic tundra site of Rinnan et al. (2008) and Phillips et al. (2018). However, Rinnan et al. observed a significant enhancement of fine roots in the top 5 cm of warmed plots what is not the case in our study although warming has been applied in a similar time span.

#### 4.1.2 Soil properties throughout the growth season

Although we observed a soil water gradient from East to West it is unlikely it had a relevant impact on our experiment. Blocks at different positions contained all treatments, therefore each treatment should have been influenced in similar way by different moisture conditions. Still the two litter addition treatments slightly differed with higher moisture for *Salix* addition treatment plots to *Betula* addition treatment plots on a low significance level ( $\alpha = 0.1$ ). As other experiments often observed a negative impact of litter addition to soil moisture (Lett and Michelsen 2014; Pedersen et al. 2017) it is surprising that the only visible changes in soil moisture of our experiment occurred between two litter treatments and not in comparison to C, F and W treatments. This moisture difference is anyway not explainable by differences in litter properties and therefore considered as neglectable, especially as soil moisture apparently had no detectable effect on CO<sub>2</sub> fluxes.

The range of observed soil warming of about 1 °C was slightly lower than during the growing season in 2014, where soil temperatures were enhanced by 1.8 °C in W treatment plots (Rousk and Michelsen 2017). As the soil temperature is of course influenced by incoming solar radiation it is possible that enhanced plant growth in warmed plots caused relatively more shading compared to control and reduced in that way the warming effect on soil with continuing experiment duration. Warming with open top chambers, built in tent form, in the experiment nearby however resulted in similarly low temperature enhancement as in our field manipulations (Pedersen et al. 2017; Ravn et al. 2017).

#### 4.2 CO<sub>2</sub> exchange of ecosystem

#### 4.2.1 Effects of environmental parameters on CO<sub>2</sub> fluxes

Figure 5 reveals clearly, that CO2 fluxes in both ways, uptake and release from the ecosystem, are very dependent on environmental parameters, which appears to be not true for soil moisture in the upper soil layer. For example, neither ER nor GEP appeared to change in any relation to big variations in volumetric water content during the 4 measurements in July. Similarily, also Pedersen et al (2017) observed no correlation of water content to ER in a similar manipulation experiment close to Abisko as well. Other environmental parameters (PAR, temperature in soil and in measurement chamber and NDVI) correlate well with fluxes. Radiation from the sun is clearly the main driver for temperature in 2 cm and 5 cm soil depth as well as in the measurement chamber, indicated very well by the fact that those parameters change along the whole growing season very much in parallel,

except for the first two measurement rounds very early in spring and on the last measurement round in autumn. Likewise, ecosystem respiration obviously rises and falls along with temperature, which confirms the long known temperature sensitivity of respiration processes in ecosystems (Davidson and Janssens 2006) which was also the case in other local experiments (Larsen et al. 2007; Pedersen et al. 2017). In accordance with that, respiration rates were lowest at dates when also temperatures were lowest, in early spring, on 4 and 15 July and late September, but relatively independent from plant development stage.

NDVI shows a simple pattern of quick increase in spring, remained very stable over the summer season, and NDVI declined continuously in September. (2010) reported not very strong and also plant community dependent but significant relationships of manually assessed NDVI on plot scale in various subarctic tundra ecosystems to LAI and plant biomass and even GEP and NEE carbon fluxes. Community dependence of plant development through the season in subarctic tundra and possible continuous plant growth throughout the snow-free season was reported by Campioli et al (2009b) and indicates that plant growth in tundra can continue until autumn. However, since NDVI increased quickly to a stable level in spring, it can be assumed that plant foliage was developed to a large extent already at the beginning of summer.

#### 4.2.2 CO<sub>2</sub> fluxes during growth period

Photosynthesis takes place in green plant tissue, therefore it is little surprising, that GEP was high and relatively stable in contrast to ER during summer at high NDVI values, although showing relevant fluctuations along with temperature and PAR. Since PAR and temperature in chamber or soil correlate apparently well for most of the season, it is not possible to assess whether one of those or both factors are governing photosynthesis. Although opinions and experimental observations of ER and GEP sensitivity to temperature are not unambiguous, it is likely that temperature affects respiration to a larger extent than primary production, especially on the short term (Davidson and Janssens 2006; Luo 2007), as for example temperature fluctuation during season. In accordance with that stands our observation on changes of NEE at different time points. Carbon uptake of the ecosystem is of course highly dependent on proper developed green plant tissue, but additionally fluctuates with temperature as it impacts ER and GEP. Highest carbon uptake occurred on relatively cold days of low respiration but during summer season, when productive plant tissue was fully developed, specifically during first half of July. Furthermore, lowest carbon uptake in summer season occurred on the 2 hottest measurement days right after cold days in the second half of July, because of strongly enhanced respiration and despite the similar NDVI and higher GEP compared to the

beginning of July. On cold days in spring and autumn, at times of low NDVI values, photosynthesis was impeded and the ecosystem functioned only as a very weak or no carbon sink.

#### 4.2.3 Treatment effects on CO<sub>2</sub> fluxes and NDVI

Although not statistically significant for single measurement rounds, a reoccurring pattern of treatment effects appears to be present for most of the CO2 flux measurements as well as for NDVI, especially during summer, but also to a relevant degree in spring and autumn season. This is a general visible enhancement of plant growth (NDVI) and for activity of ecosystem (CO<sub>2</sub> fluxes), in relation to quality of additional substrate added on plots. Changes to NDVI and CO<sub>2</sub> fluxes by *Betula* litter addition compared to control are almost not recognisable and range from a slight decrease to increase of fluxes and NDVI. Thus, we assume that *Betula* litter, the substrate addition treatment with highest C:N ratio, has very little to no effect on the ecosystem. Fluxes and NDVI of *Salix* litter addition plots, a substrate of better quality, is slightly higher in most of the single measurements of carbon fluxes and NDVI. Fungal fruitbody addition, the substrate with lowest C:N ratio resulted in the biggest increase of CO<sub>2</sub> fluxes and NDVI in all measurements compared to the two other treatments with substrate input. However, these responses are significant only for the F treatment, but for F in many cases of the seasonal grouped measurements.

Also, NDVI and CO<sub>2</sub> fluxes of warmed plots are enhanced to a very similar degree but on average usually a bit lower than the F treatment plots, thus have also a relative fixed position in the response pattern somewhere between F and S treatment, with a significant enhancement compared to control for ER over the whole season, for GEP in spring and for NDVI in summer.

Statistically insignificant, but apparently the same pattern is also visible for the top 5cm of the soil total N content and C:N ratio (Figure 4). While it appears logic, that N content changes with quality of substrate added continuously, the reasons for potentially enhanced N content in topsoil of warming treatment plots remains more difficult to explain.

However, similar patterns have been also observed in similar manipulation experiments in close proximity and similar vegetation. In mesic tundra enhancement of GEP and ER through fertilization (comparable to fungi addition treatment) was stronger as for warming treatment after 10 and 11 years of warming (Illeris et al. 2004). Although, the same site after 23 years of treatment, warming enhanced ER slightly more than fertilization (Ravn et al. 2017). A close by wet tundra heath shows same pattern of weak enhancement for *Betula* litter addition and a stronger enhancement through warming for ecosystem and soil respiration (Ravn et al. 2017) and similarly for ER and in early season also for GEP in the study of Pedersen et al (2017). These results from the wet tundra field site could

be further linked to enhanced losses of soil carbon and nitrogen stocks, more by warming than litter addition (Phillips et al. 2018) and significantly increased NDVI for the litter and warming treatment, although on the same magnitude (Rinnan et al. 2008). An incubation experiment with soil samples of the region showed same pattern for increased respiration rates by litter addition and stronger increase through 2° warming (Jonasson et al. 2004). Zamin and Grogan (2012) reported increased plant growth of *Betula glandulosa* in a similar response pattern to warming, low and high nitrogen fertilization, although phosphorus fertilization showed an even stronger response in their study. However, it should be noted, that this patterns in other studies were visible only for some assessed response variables, maybe even only for parts of the season, and only sometimes statistically significant and in other studies at subarctic tundra field sites around Abisko those patterns were not observable (Christensen et al. 1997). Net carbon exchange fluxes of the ecosystems anyway showed various responses, to warming, fertilization or litter addition, with increasing or decreasing uptake or even release of carbon from ecosystem and further, effects of combined treatments were not coherent (Christensen et al. 1997; Illeris et al. 2004; Pedersen et al. 2017; Tiiva et al. 2008; Zamin and Grogan 2012). Therefore, general conclusions of same effects of climate warming and increasing litter input over global tundra ecosystems should be taken carefully.

The reoccurring pattern of effect magnitude for all 3 different substrates, gives clear indication of the importance of litter quality on the activity effect on ecosystems. If we assume nitrogen limitation, as it is common in tundra (Jonasson et al. 1999; Mack et al. 2004; Sistla et al. 2012), this pattern is further easily explainable by the different nitrogen inputs of the respective substrates. *Betula* litter with a C:N ratio of 45 is even lower in quality than the soil with C:N ratio of 28 in top 5 cm, which further declines with depth, hence probably not improving nitrogen availability at all. The litter of *Salix* has a C:N ratio of 22, thus is of slightly higher quality than top soil. The very high nitrogen content of fungi with a C:N ratio of 11 obviously functions as a boost for plant growth and respiration. Not only the total amount of nitrogen inputs which differ by a magnitude of 4, also the C:N ratio of litter input is an important factor for N turnover rates in the soil and in this way higher quality litter can feedback to a higher nutrient availability and plant growth and carbon loss from soil on the long term (Buckeridge et al. 2010). Therefore, development of the species composition in a warming tundra, for example which shrub species will profit most with shrub expansion, can be of relevance to carbon and nitrogen cycling and hence the risk to carbon losses to atmosphere.

The warming treatment of course interacts in a different way with the ecosystem than the substrate addition treatments, but still shows a similar response. Remarkably the effect of warming on CO<sub>2</sub> fluxes is observable already earlier in the season compared to substrate addition plots, being the only treatment, which is a carbon sink in May already. Thus, a lengthening of the growing season due to

warmer temperatures could result in more carbon accumulation in new plant biomass to a small extent, even though enhanced NEE carbon uptake is not significant.

At least during summer period, NDVI of warmed plots is significantly higher than in control. Photosynthetic capacity is correlated with nitrogen content of plant leaves (Chapin et al. 2011), hence nitrogen uptake by plants is of importance for production green plant tissue which impacts NDVI and potentially enhances carbon fluxes. For this reason, chlorophyll and Nitrogen content of plants have been related to enhanced plant growth and been of interest in previous tundra ecosystem field studies. Semenchuk et al. (2015) reported enhanced growth and nitrogen accumulation in *Salix polaris* leaves, due to higher nitrogen availability of winter warmed soils and at a similar subarctic tundra heath as our site, enhanced nitrogen content and biomass was observed after few years of summer warming at least for dominant evergreen shrub (*Cassiope tetragona*) (Michelsen et al. 1996). I therefore conclude that plants in warmed plots were able to accumulate more nitrogen and invest in leaf production, resulting in higher NDVI for this treatment, even stronger as for litter treatments. Several explanations for the enhanced N uptake by plants and increase in NDVI are possible.

Nitrogen fixation by cyano bacteria associated with tundra mosses is considered as an important pathway of N input to arctic ecosystems. At the same field site of our study, N-fixation was enhanced by warming (Rousk and Michelsen 2017) as well as in a close by wet tundra heath (Lett and Michelsen 2014). However, the amount of enhanced N fixation during growth season under warmed conditions was modelled to be only 60 mg N m<sup>-2</sup> (Rousk and Michelsen 2017), thus only of a few percent of N input by either substrate addition and unlikely to exceed N availability at litter treatment plots.

Enhanced NDVI could be further explained by an increase of biomass or a change in plant community composition in favour of species allocating more nutrients. A shift towards deciduous shrubs and graminoids and increased biomass production thereof on the cost of lichens and mosses after warming, similarly as for fertilization, has been reported in previous studies (Chapin et al. 1995; Walker et al. 2006). Nitrogen uptake by deciduous shrubs was observed to be much more efficient compared to evergreen shrubs under high nitrogen availability in the soil and vice versa at sites with low availability (Vankoughnett and Grogan 2014). At our field site, Rousk and Michelsen (2017) observed twice as much plant cover of the dominant sedge *Carex vaginata*, and increased litter compared to control plots after 4 years of treatment already. If nutrient availability increased with warming, we would expect the vegetation to shift towards deciduous shrubs and graminoids and increased plant growth, thus resulting in higher NDVI values. Higher mineralization rates of SOM and associated nutrient release due to warming has been reported in numerous studies as summarized

by Hobbie et al (2002) although other environmental factors than temperature are also of importance for nutrient mineralization and availability. Results from subarctic tundra soil incubated together with grass seedlings and Betula litter addition and warming as treatment suggest that mobilization of nitrogen and uptake by plants is facilitated by warming, though not by Betula litter addition (Jonasson et al. 2004) which could explain the stronger response in NDVI and carbon fluxes due to reduced N limitation in warmed plots also in our study.

In summary it can be claimed, that effect of additional leaf litter input of expanding shrub vegetation has less consequences for the ecosystem than warming, despite the fact, that the ecosystem is obviously nutrient limited. Litter quality and nutrient availability is of importance for the activity and magnitude of carbon fluxes, but warming apparently offsets limitation of changing substrate quality to a bigger extent. Strong fertilization by enhanced fungi fruitbody appearance in future is not a realistic future scenario. The tundra experiences a vegetation change at the moment which alters litter composition which we were simulating by the two litter addition treatments. However, additional organic matter thus nutrient input will not be derived from external sources but recycled nutrients from its own soil beneath, returned through plant litter. Considering that and comparing the carbon fluxes and NDVI responses of the litter treatments to temperature enhancement, it is clear that temperature as accelerator for plant growth and organic matter turnover rates is of higher relevance on short terms than additional litter input.

The increase of ER is statistically significant for F and W treatment for every different subdivision of the season, spring, summer and autumn. Effects of F and W treatment on GEP are significant only partly for the seasonal subdivisions and only for F treatment over the whole season. This can probably be accounted to the observation that more environmental parameters than temperature have a main influence on photosynthesis. However, the magnitude to which treatment effects on GEP is bigger than for ER, which results in a higher net carbon uptake of the ecosystem compared to control plots. NEE is controlled by GEP and ER and therefore affected in complicated ways by several environmental parameters. This results in higher variation between plots for NEE and consequently, changes in NEE lack statistical evidence. But apparently the same treatment effect pattern occurs for NEE than it does for the other fluxes. Looking at subdivisions of the seasons the treatment effect pattern of NEE appears to be more or less identical to GEP. I therefore conclude that despite the lack of significant statistical evidence, the visual observation of enhanced carbon uptake in treatment plots is not random, but high nutrient input or warming strengthens the carbon sink function of tundra ecosystems during summer season and daytime in this experiment. This is maybe in contrast to observations in close by ecosystems (Christensen et al. 1997; Pedersen et al. 2017) where warming usually decreased net carbon uptake. Results from litter addition showed little effect on

carbon uptake rates (Pedersen et al. 2017) and fertilization enhanced carbon uptake (Christensen et al. 1997). Although, at the same manipulation experiment as in Christensen et al. (1997) no changes of NEE by treatments were observed a couple of years later by Illeris et al. (2004). This reflects maybe again the difficulty to assess the net carbon exchange. Anyway, there is a potential that although respiration and therefore potential carbon losses are the most evident effects of climate change, changes in plant community and increasing ecosystem production is able to offset those losses. Furthermore, it has to be noted, we measured CO<sub>2</sub> fluxes only during the day and under absence of rain, for the protection of instruments. Changing environmental conditions, such as light influx and temperature, change carbon flux dynamics on a diurnal circle and even vary between different years (Tenhunen et al. 1995) and temperature sensitivity of carbon fluxes changes strongly during the day and night cycle, making it not possible properly estimate carbon balances over seasons without diurnal measurements (Fouché et al. 2017). Illeris et al. (2004) observed that carbon uptake during day can be easily lost again at night, regardless of treatment. Diurnal CO<sub>2</sub> flux measurements, would therefore be necessary to estimate how much of the increased carbon uptake during day remains in the system on the long term.

#### 4.3 Enzymes

Because of the strong indication of the importance of nutrient inputs on the ecosystem and hence also for carbon fluxes, it is very surprising that the treatment response pattern of fluxes is not visibly related to any patterns of potential enzyme activities in the soil. Statistical evidence for treatment effects hardly exists. This in fact fits the observation of no or low effects of treatments on soil properties, such as carbon and nitrogen content or root biomass. The weak response to treatments make it further very difficult to assess whether methodological problems led to high variation within treatments, or whether treatment effects on soil conditions and enzyme production was very low just at sampling time in the middle of the active summer season.

#### 4.3.1 Activities at different depths

Surprisingly potential extracellular enzyme activity was higher in 5-10 cm depth than in the top layer of the soil. In general it is assumed, that hydrolytic enzymes decline with depth as organic material becomes less present as reported for forest ecosystems (Baldrian and Štursová 2011), but also observed in tundra ecosystems (Jing et al. 2014; Koyama et al. 2013). Also the potential enzyme activities in similar vegetation (Phillips et al. 2018) either remained similar or slightly declined with

depth. Although enzymes are produced to make more nutrients available, production thereof is nutrient intensive itself (Allison and Vitousek 2005). It might be possible, that the depleted nitrogen content of the first 5 cm in the soil and possible nutrient limitation are the reason for low enzyme production. This appears rather unlikely, since if nitrogen limitation was the reason for lower activity in our experiment, we could expect an increase in most hydrolytic enzymes with enhanced nitrogen availability (Sistla et al. 2012). An effect of treatments which have higher nitrogen inputs should be visible, thus for *Salix* litter addition plots and especially in the fungi addition treatment plots. This was not the case, at least at time of sampling. In addition, phosphatase activity behaves contrary to all other hydrolytic enzymes and exhibits a much higher activity in the top 5 cm of the soil than in the soil layer underneath, and for that reason production is probably not nitrogen limited.

According to the resource allocation theory (Sinsabaugh and Moorhead 1994) we should assume, that demand for phosphorus is relatively higher than for nitrogen and carbon in the top 5 cm compared to soil in 5-10 cm depth. As the total nitrogen concentration increases with depth, it appears rather confusing that nitrogen cycling enzymes have relative higher and phosphorus relative lower potential activity in deeper soils. The results in this way suggests, that phosphorus is even more limiting in the topsoil, while more available in 5-10 cm. This can be explained only with making simplifications and assumptions over parameters we did not assess. Possibly total nitrogen content or the C:N ratio is an unsuitable approximation of nitrogen availability. For example, ammonium concentrations and N mineralization rates in soils at our field site assessed by Rousk et al. (2016) appear to be unrelated to total nitrogen content. Another explanation could be that microbial community, hence also the microbial nutrient demand and associated extracellular enzyme production change significantly within these first 10 cm of the soil profile. For example the Fungi:Bacteria ratio, as well as microbial community response to treatment apparently differed between 0-5 cm and 5-10cm at a similar experiment site (Rinnan et al. 2007). The opposite depth response of phosphatase activity could maybe also be enhanced in top 5 cm by phosphatase release from plant roots. Plants can for example influence their phosphorus ability with release of high amounts of phosphatases to the environment (Wu et al. 2013). For instance, the tussock tundra plant Eriophorum vaginatum (not present at our site) was reported to increase phosphatase release late in the season, when litter input makes organic bound phosphorus relatively abundant, even though plant phosphorus demand is highest in spring (Moorhead et al. 1993). However, phosphate release from phosphatases associated with *Eriophorum vaginatum* root tips, doubled the plants demand but accounted for few percent of total phosphorus release in soil only. Weintraub and Schimel (2005b) observed peaks of available phosphates during mid-summer growth season in graminoid dominated tundra, as well as gradually increasing phosphate concentrations in shrub tundra in the second half of the growing season and set it in relation to increased phosphatases released from roots earlier in

season, as already than suggested by Moorhead. It is possible that also in our experiment, phosphatase release in middle of the growing season adds to the relatively high phosphatase activity in top 5 cm of soil, which is most densely rooted zone. Anyway, all those theories on opposite activity changes with depth effect for phosphatase compared to N and C cycling enzymes are highly speculative without additional information on total phosphorus, available forms of nitrogen and phosphorus or microbial biomass and community structure at different depths, which have unfortunately not been assessed by us or previous studies in at the site.

The general enhancement of all other enzyme activities than phosphatase in 5-10 cm indicates an enhanced turnover of organic matter underneath the top 5cm of the soil. This contradicts maybe the observations at the most similar field experiment very close to our location, where microbial biomass and all forms of soluble nutrients were decreased, as well as root biomass in 5-10 cm depth (Rinnan et al. 2007), which speaks against enhanced activity. In the study of Phillips et al. (2018) enzyme activities were not enhanced with depth in a similar way as in our experiment. However, carbon losses through warming were a result of C-stock depletion and enhanced soil respiration in 5-10 cm depth, while microbial biomass, nitrogen and phosphorus remained fairly similar in both depths. Although the strongest treatment effects would be expected on the top of the soils, this could maybe be an indication for the high relevance of deeper soils, and their impact on ecosystem functions and alteration of carbon stocks on the long term. At least in our ecosystem, possible climate change feedbacks, positive or negative, would probably be stronger from soils below 5cm depth.

#### 4.3.2 Effect of time during season on enzyme activities

The timepoint of soil sampling might have a very relevant effect on potential enzyme activities in the soil (Sistla and Schimel 2013; Wallenstein et al. 2009). Our samples were taken early in August in the middle of the main growing season. Nutrient availabilities in tundra soils can change rapidly within days and available nitrogen is very much depleted during summer and controlled by uptake activities rather than by source availabilities (Weintraub and Schimel 2005b). In that way, treatments which rather increase nutrient input, as we have in the substrate addition treatments of *Betula, Salix* and *Fungi* and indirectly also in the warming treatment, may not change the deficiency of nitrogen supply during summer, as additional nutrients are utilized immediately. Also Sistla and Schimel (2013) observed no difference of hydrolytic enzyme activities between control and warmed plots, in the organic soil horizon, after 22 years of treatment during summer season, when nutrient availabilities and microbial biomass were lowest, but treatment differences were significant during early winter and spring thaw. Additional substrate resources or warming allows for enhanced plant and microbial

growth, thus also carbon fluxes, but will not overcome nutrient limitation during the most active time of the year. Hence production of extracellular enzymes to encounter nutrient demand would be a necessary strategy of plants and microbes among all treatments, probably masking treatment effects at certain times of the season, probably explaining why treatment effects are clearly visible on a plant level but appear to not affect enzyme activities in soils at certain times of sampling, as in the beginning of August.

The only potential enzyme activity which showed statistical relevant difference by treatment compared to control is  $\beta$ -N-Acetylglucosaminidase in 0-5 cm soil depth (Table 6), an enzyme associated with nitrogen cycling. The enhanced activity of the *Betula* litter treatment was observed in the same way by Phillips et al. (2018). The same litter was used in this experiment and is low in its nitrogen content, but at the same time adds considerable high amounts of phosphorus (Michelsen, unpublished). Inorganic phosphorus was reported to increase at this wetter tundra site in the top 5 cm of soil (Rinnan et al. 2008), while this could not be observed by Phillips et al. (2018) several years later. If phosphorus is co-limiting the ecosystem, an increase in nitrogen cycling enzymes would fit well with the nutrient allocation theory (Sinsabaugh and Moorhead 1994) if phosphorus availability is enhanced by *Betula* litter addition. In any way, the enhancement of NAG remains the only indication for a treatment effect on potential enzyme activities, and our hypothesis of changing patterns of enzyme activities with changing quality of added substrates cannot be confirmed.

### 5 Conclusion

As I hypothesised, the results of this study clearly indicate that type of available substrate and nutrient input through litter plays an important role for the activity and carbon turnover of the tundra ecosystem. Plant growth responds to different substrate additions and in correlation to its nutrient content. However, if considered, that changing ecosystems will naturally not be subject to very high nutrient additions, as in the Fungi treatment, temperature remains the key driver for changing the ecosystem on intermediate terms. The activity and plant growth apparently responded with higher activity to warming. NDVI, as well as all carbon fluxes (ER, GEP and NEE) were increased to a larger extent than the two litter addition treatments, though usually to a lower extent than fungi addition treatment. In any way, if warming enhances plant growth, it will result in more litter input in future. The relatively low response of litter addition may not be underestimated on the long term (beside lacking statistical evidence), as the response pattern of different substrates was similar among all assessed fluxes and NDVI at any season. In that way, a cascading effect as suggested by Buckeridge et al. (2010) and Hartley et al. (2012) of enhanced activity, induced by warming, and amplified by accelerated nutrient cycling, plant uptake and return through litterfall, is likely to interactively change tundra ecosystems; here the C/N ratio of litter will play an important role and may control the pace at which this cascade is running. However, our experiment does not indicate increased carbon losses from ecosystem through climate change. All treatments increased carbon uptake to a stronger degree than carbon release through respiration. This contradicts our expectation for the warming treatment, as respiration is supposed to be more temperature sensitive than photosynthesis. Warming during past 6 years shifted the ecosystem to a state which supported plant growth and consequently increased its photosynthesis ability and CO<sub>2</sub> uptake during the day. Increasing plant growth of all treatment plots therefore suggests a potential carbon accumulation in the ecosystem. To estimate the magnitude of potential carbon accumulation, however, would require additional measurements during the whole diurnal circle, as photosynthesis and respiration may be differently affected by lower light conditions and temperatures at night. Furthermore, better estimates for actual plant biomass than NDVI would help to assess whether increased plant growth offsets possible carbon losses from soil.

After 6 years of treatment application, no significant effects on abiotic soil properties as well as potential enzymatic activities were detected. Abiotic soil conditions respond probably slower to treatments and climate change than plant growth and assessment of those is methodological more complicated than for in situ methods of carbon fluxes and NDVI measurements. Soil sampling for enzyme activity assessment was conducted during a time when nutrient availability was probably lowest, and deficiency might have affected all treatments in a similar way, masking possible

treatment effects. Additional potential enzyme activity assessments at different times of the growing season could reveal whether treatments do affect enzyme production at certain times of the season. Our hypotheses about enzyme activity response to treatments cannot be confirmed by our single time point assessment. Surprisingly, nutrient demands appear to change significantly with depth, and the top layer of the soil was lower in enzyme activities than 5 cm beneath, except for phosphatase. This would suggest, that phosphate is relatively more limiting in the top soil compared to the soil below. Higher carbon and nitrogen cycling enzyme activities in 5-10 cm depth suggest, that SOM decomposition and therefore potential carbon loss from soil through climate change effects is of bigger relevance below the top soil layer. This is similar as observed by Phillips et al. (2018) after 16 years of same treatments, despite the fact that the first centimetres of soil are generally considered as the most active layer. Also at our field site changes of carbon and nitrogen stocks in soil could become visible after additional years of continuing treatments, an should be subject to future research.

### 6 Library

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### 9 List of Acronyms

- C Control (no treatment)
- B Betula pubescens ssp. Tortuosa Litter addition treatment
- S Salix myrsinifolia litter addition treatment
- F Fungal fruitbody addition treatment
- W Warming treatment with open top chambers
- OTC Open top chambers for warming treatment
- ER Ecosystem Respiration
- GEP Gross Ecosystem Photosynthesis
- NEE Net Ecosystem Exchange
- NDVI Net Differential Vegetation Index
- BX β-Xylosidase
- CB β-D-Cellubiosidase
- BG β-glucosidase
- NAG β-N-Acetylglucosaminidase
- AP Acid Phosphatase
- LAP Leucine Aminopeptidase
- SOM Soil Organic Matter

# **10 Appendix**

#### 10.1 Oxidative Enzymes





### 10.2 Experimental plots

	Plot		Metal frame base area	Chamber + Base volume
Nr.	Treatment	Block	m²	M <sup>3</sup>
1	W	1	0.1190	0.0401
2	С	1	0.1190	0.0383
3	Р	1	0.1190	0.0413
4	F	1	0.0961	0.0427
5	В	1	0.1190	0.0395
6	W	2	0.1190	0.0425
7	Р	2	0.1190	0.0383
8	В	2	0.1190	0.0419
9	С	2	0.1190	0.0419
10	F	2	0.0961	0.0412
11	С	3	0.1190	0.0401
12	В	3	0.1190	0.0401
13	W	3	0.1190	0.0407
14	Р	3	0.1190	0.0359
15	F	3	0.0961	0.0436
16	В	4	0.1190	0.0449
17	С	4	0.1190	0.0425
18	F	4	0.0961	0.0403
19	Р	4	0.1190	0.0383
20	W	4	0.0961	0.0431
21	В	5	0.0961	0.0422
22	Р	5	0.0961	0.0422
23	W	5	0.0961	0.0412
24	F	5	0.0961	0.0427
25	С	5	0.0961	0.0431
26	W	6	0.0961	0.0436
27	В	6	0.0961	0.0427
28	Р	6	0.0961	0.0431
29	С	6	0.0961	0.0436
30	F	6	0.0961	0.0422

S.Table 1: Experimental design and plot attributes; Dimensions of metal frame bases and measurement chamber for flux measurements.

# 10.3 Data of soil properties

Plot	Soil layer	Depth core1	Depth core2	Water content	Dry weight	Bulk- soil	Coarse roots	Fine roots	Nitrogen content	Carbon content	C:N ratio
Nr.	cm	cm	cm	g H <sub>2</sub> O g soil <sup>-1</sup>	g	g cm <sup>-1</sup>	g dm-1	g dm <sup>-1</sup>	%	%	
1	0-5	13	13	385.4	3.63	0.0337	11.8	2.9	1.5	40.4	26.1
2	0-5	23	25	557.9	3.70	0.0344	9.0	1.7	1.2	40.5	33.2
3	0-5	20	22	594.4	4.22	0.0392	4.6	6.1	1.3	40.0	30.4
4	0-5	24	23	488.2	4.78	0.0445	3.0	4.4	1.4	39.8	29.4
5	0-5	17	22	293.7	5.64	0.0524	8.1	4.2	1.3	39.7	31.1
6	0-5	12	24	354.5	4.39	0.0408	7.3	4.5	1.4	39.2	27.8
7	0-5	23	24	338.6	3.23	0.0300	5.9	2.9	1.3	38.9	29.1
8	0-5	17	20	488.2	2.71	0.0252	9.6	5.0	1.5	39.4	25.8
9	0-5	10	10	254.6	8.04	0.0748	10.8	3.3	1.9	39.1	20.4
10	0-5	16	17	532.9	2.76	0.0257	20.1	3.1	1.5	39.3	26.8
11	0-5	17	19	693.7	4.53	0.0421	2.1	6.9	1.0	38.5	37.8
12	0-5	15	17	575.7	5.39	0.0501	8.7	4.1	1.3	39.0	29.6
13	0-5	15	20	455.6	4.33	0.0403	8.5	4.8	1.3	39.5	31.3
14	0-5	11	14	474.7	6.04	0.0562	8.0	5.8	1.7	39.2	22.9
15	0-5	17	18	338.6	3.73	0.0347			1.5	39.7	26.3
16	0-5	19	20	296.8	9.96	0.0926	5.8	5.7	1.6	38.9	25.1
17	0-5	12	15	313.2	4.90	0.0456	1.4	1.7	1.3	38.9	30.6
18	0-5	8	21	275.9	10.20	0.0949	10.3	4.2	1.8	37.7	20.9
19	0-5	10	13	237.8	7.25	0.0674	10.7	5.4	1.6	39.1	23.8
20	0-5	15	17	242.5	8.56	0.0796	8.3	5.3	1.6	38.8	24.2
21	0-5	14	14	380.8	5.04	0.0469	10.6	6.1	1.4	41.4	29.0
22	0-5	14	13	437.6	3.85	0.0358	6.3	6.9	1.2	39.3	32.3
23	0-5	14	17	509.8	3.84	0.0357	5.4	8.2	1.6	39.2	24.8
24	0-5	17	21	443.5	5.83	0.0542	7.1	3.8	1.3	40.2	29.9
25	0-5	18	20	267.6	6.53	0.0607	9.8	6.6	1.5	39.0	26.9
26	0-5	17	17	300.0	4.16	0.0387	5.8	2.8	1.2	39.9	32.0
27	0-5	17	19	278.8	5.45	0.0507	4.5	4.7	1.3	39.9	31.0
28	0-5	15	20	252.1	6.99	0.0650	3.8	4.1	1.6	39.8	24.3
29	0-5	15	16	222.6	6.94	0.0645	6.3	8.2	1.7	39.8	23.4
30	0-5	8	17	296.8	4.46	0.0415	8.1	4.1	1.8	45.0	24.7

S.Table 2: Soil properties for 0-5 cm.

Plot	Soil Iayer	Depth core1	Depth core2	Water content	Dry weight	Bulk- soil	Coarse roots	Fine roots	Nitrogen content	Carbon content	C:N ratio
Nr.	cm	cm	cm	g H <sub>2</sub> O g soil <sup>-1</sup>	g	g cm <sup>-1</sup>	g dm-1	g dm⁻¹	%	%	
1	5-10	13	13	380.8	10.04	0.0934	10.3	3.2	2.1	37.8	18.3
2	5-10	23	25	584.9	5.31	0.0493	6.6	2.8	1.3	38.4	28.5
3	5-10	20	22	541.0	5.11	0.0475	4.7	4.3	1.5	37.8	25.3
4	5-10	24	23	495.2	5.72	0.0532	8.1	3.6	1.6	38.1	23.8
5	5-10	17	22	323.7	7.57	0.0704	6.6	2.6	1.7	38.4	22.8
6	5-10	12	24	323.7	10.09	0.0939	0.8	2.2	2.0	38.8	19.6
7	5-10	23	24	624.6	4.81	0.0448	0.0	2.6	1.7	37.6	22.0
8	5-10	17	20	247.2	11.55	0.1074	8.3	3.3	2.3	37.6	16.6
9	5-10	10	10	145.1	42.52	0.3954	0.0	2.0	1.1	18.7	17.4
10	5-10	16	17	262.3	9.42	0.0876	10.0	2.6	2.0	37.4	18.5
11	5-10	17	19	861.5	5.19	0.0483	5.0		1.6	38.5	24.6
12	5-10	15	17	549.4	7.57	0.0704	4.2	2.2	1.8	37.7	20.8
13	5-10	15	20	443.5	5.73	0.0533	5.4	3.3	1.7	39.3	22.6
14	5-10	11	14	455.6	9.71	0.0903	3.8	2.6	2.5	37.0	15.0
15	5-10	17	18	281.7	8.09	0.0752			2.1	39.2	18.8
16	5-10	19	20	254.6	9.35	0.0869	1.2	0.8	2.1	36.4	17.1
17	5-10	12	15	287.6	11.32	0.1053	4.7	2.4	2.3	38.1	16.3
18	5-10	8	21	287.6	11.19	0.1301	5.3	3.6	2.2	37.4	17.2
19	5-10	10	13	267.6	18.30	0.1702	2.0	2.7	2.2	38.1	17.5
20	5-10	15	17	270.4	16.03	0.1491	1.1	3.7	2.0	37.3	18.4
21	5-10	14	14	385.4	10.67	0.0993	3.4	2.9	2.0	38.2	19.4
22	5-10	14	13	410.2	9.73	0.0905	2.4	4.6	2.1	38.0	18.2
23	5-10	14	17	437.6	10.64	0.0989	4.3	3.1	2.3	36.2	15.5
24	5-10	17	21	420.8	9.66	0.0899	0.0	3.8	1.9	37.6	19.6
25	5-10	18	20	303.2	9.93	0.0924	3.3	2.9	2.2	35.0	16.0
26	5-10	17	17	247.2	6.67	0.0621	6.3	2.7	1.6	37.8	23.3
27	5-10	17	19	267.6	6.81	0.0633	2.3	3.4	2.1	37.4	17.9
28	5-10	15	20	273.1	14.20	0.1320	3.4	2.2	2.2	36.1	16.2
29	5-10	15	16	247.2	11.22	0.1043	13.1	3.1	2.0	36.7	17.9
30	5-10	8	17	237.8	8.80	0.1023	4.3	3.0	1.8	37.0	20.1

S.Table 3: Soil properties for 5-10 cm.

Plot	Soil Iayer	Depth core1	Depth core2	Water content	Dry weight	Bulk- soil	Coarse roots	Fine roots	Nitrogen content	Carbon content	C:N ratio
Nr.	cm	cm	cm	g H <sub>2</sub> O g soil <sup>-1</sup>	g	g cm <sup>-1</sup>	g dm-1	g dm <sup>-1</sup>	%	%	
1	10-15	13	13	371.7	10.39	0.1611	0.2	0.9	2.4	34.6	14.4
2	10-15	23	25	461.8	7.01	0.0652	5.6	2.8	1.5	36.6	24.2
3	10-15	20	22	468.2	6.76	0.0629	4.9	2.9	1.8	37.2	20.5
4	10-15	24	23	733.3	6.37	0.0592	0.3	2.1	2.1	33.9	16.5
5	10-15	17	22	346.4	12.70	0.1181	3.0	1.2	2.2	35.8	16.5
6	10-15	12	24	293.7	9.74	0.1294	4.1	2.6	2.3	35.0	15.5
7	10-15	23	24	371.7	11.58	0.1077	0.6	1.9	1.8	37.2	20.7
8	10-15	17	20	316.7	16.06	0.1494	2.7	1.2	2.3	34.9	15.4
10	10-15	16	17	287.6	18.56	0.1726	1.2	0.7	2.1	35.0	16.8
11	10-15	17	19	706.5	7.69	0.0715	2.5	1.3	2.2	34.7	15.7
12	10-15	15	17	290.6	18.30	0.1702	0.3	1.0	2.1	30.6	14.6
13	10-15	15	20	400.0	10.46	0.0973		0.9	2.3	34.6	15.0
14	10-15	11	14	410.2	6.15	0.1144	0.3	1.4	2.2	35.9	16.4
15	10-15	17	18	313.2	14.83	0.1379	5.9	2.0	2.4	36.3	15.3
16	10-15	19	20	296.8	18.70	0.1739	0.3	1.1	2.3	36.2	15.5
17	10-15	12	15	184.1	18.72	0.2487	0.5	1.2	1.8	30.2	16.9
18	10-15	8	21	300.0	4.96	0.0923	2.3	2.2	2.1	35.4	17.1
19	10-15	10	13	309.8	5.07	0.1572	0.6	1.5	2.3	35.6	15.3
20	10-15	15	17	275.9	8.99	0.0836	0.2	0.7	2.1	35.7	17.0
21	10-15	14	14	346.4	13.86	0.1611	2.9	1.0	2.2	35.3	15.8
22	10-15	14	13	323.7	11.91	0.1582	1.0	1.1	2.2	33.8	15.2
23	10-15	14	17	148.8	32.98	0.3408	1.4	0.2	1.1	16.2	15.1
24	10-15	17	21	380.8	13.70	0.1274	0.5	1.6	2.5	34.4	13.7
25	10-15	18	20	197.6	23.89	0.2222	0.0	0.7	1.6	24.9	15.7
26	10-15	17	17	273.1	12.46	0.1159	6.7	2.2	2.4	35.8	14.7
27	10-15	17	19	284.6	17.45	0.1623	0.0	1.6	2.7	34.5	12.7
28	10-15	15	20	270.4	19.01	0.1768	0.8	1.4	2.3	32.8	14.3
29	10-15	15	16	262.3	18.39	0.1711	0.2	1.8	2.2	33.3	15.4
30	10-15	8	17	265.0	6.45	0.1200	0.0	1.4	1.9	35.2	18.9

S.Table 4: Soil properties for 10-15 cm.

Plot	Soil Iayer	Depth core1	Depth core2	Water content	Dry weight	Bulk- soil	Coarse roots	Fine roots	Nitrogen content	Carbon content	C:N ratio
Nr.	cm	cm	cm	g H₂O g soil⁻¹	g	g cm <sup>-1</sup>	g dm-1	g dm <sup>-1</sup>	%	%	
2	15-20	23	25	385.4	7.55	0.0702	1.0	1.8	1.7	35.2	20.6
3	15-20	20	22	415.5	9.93	0.0924	1.1	0.8	2.2	34.6	16.0
4	15-20	24	23	212.5	28.27	0.2629	0.0	1.0	1.9	27.2	14.0
5	15-20	17	22	303.2	11.54	0.1533	1.4	1.0	2.3	34.4	14.8
6	15-20	12	24	270.4	10.51	0.1956	0.4	1.9	2.2	32.8	14.7
7	15-20	23	24	293.7	15.28	0.1422	0.0	0.9	2.0	36.3	18.1
8	15-20	17	20	249.7	14.49	0.1925	0.0	0.2	2.0	30.8	15.1
10	15-20	16	17	214.5	8.61	0.2668	0.4	0.2	1.5	30.6	19.8
11	15-20	17	19	327.4	7.60	0.1178	0.0	0.7	2.1	34.0	16.4
12	15-20	15	17	358.7	2.17	0.1010	1.9	0.6	2.1	31.4	14.7
13	15-20	15	20	474.7	6.17	0.1148	0.0	0.9	2.0	26.2	13.2
15	15-20	17	18	287.6	10.72	0.1994	0.0	0.9	2.4	33.4	14.1
16	15-20	19	20	237.8	22.55	0.2330	1.0	0.7	1.9	33.8	18.0
18	15-20	8	21	303.2	8.04	0.1495	0.0	1.7	2.1	35.1	16.5
20	15-20	15	17	247.2	4.69	0.2183	0.0	0.0	1.8	33.6	18.4
23	15-20	14	17	208.6	6.88	0.3198	0.0	0.7	1.7	24.6	14.4
24	15-20	17	21	300.0	13.02	0.1730	0.1	0.5	2.3	34.2	15.1
25	15-20	18	20	71.8	60.03	0.6978	0.0	0.5	1.0	15.8	16.3
26	15-20	17	17	273.1	5.75	0.1337	0.0	0.7	2.4	34.1	13.9
27	15-20	17	19	281.7	13.64	0.2115	0.0	1.7	2.3	34.6	15.0
28	15-20	15	20	240.1	10.77	0.2002	0.0	0.9	1.9	32.6	17.2
29	15-20	15	16	297.7	1.72	0.1599	0.0	1.1	2.0	33.5	17.2
30	15-20	8	17	270.4	4.77	0.2219	0.0	1.3	2.0	33.7	17.3

S.Table 5: Soil properties for 15-20 cm.

Plot	Soil Iayer	Depth core1	Depth core2	Water content	Dry weight	Bulk- soil	Coarse roots	Fine roots	Nitrogen content	Carbon content	C:N ratio
Nr.	cm	cm	cm	g H <sub>2</sub> O g soil <sup>-1</sup>	g	g cm <sup>-1</sup>	g dm <sup>-1</sup>	g dm <sup>-1</sup>	%	%	
2	20-25	23	25	367.3	6.85	0.0797	0.0	0.4	2.2	34.8	15.5
3	20-25	20	22	327.4	3.52	0.1638	0.2	0.9	2.3	34.1	14.8
4	20-25	24	23	208.6	17.58	0.2336	0.0	0.6	2.1	28.9	13.8
5	20-25	17	22	287.6	3.62	0.1685	0.0	0.8	2.0	34.0	17.3
6	20-25	12	24	133.6	16.20	0.3767	0.0	0.6	1.2	21.3	17.5
7	20-25	23	24	267.6	14.52	0.1929	0.7	1.2	1.7	35.5	20.5
18	20-25	8	21	284.6	3.57	0.3324	0.0	2.5	2.3	34.8	15.3
24	20-25	17	21	242.5	2.58	0.2397	0.0	0.1	2.1	32.1	15.0

S.Table 6: Soil properties for 20-25 cm.
## 10.4 Data of $CO_2$ -flux measurement and environmental parameters

Plot	Measu Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope		CO₂ flu	x
											mg	CO <sub>2</sub> m	<sup>2</sup> h <sup>-1</sup>
	hour	min	NEE / ER	°C	vol %	°C	°C	mbar	ppm s <sup>-1</sup>	ppm s <sup>-1</sup>	NEE	ER	GEP
1	12	15	NEE	14.0	25.4	5.9	3.2	1227	943	-0.0822	-184		432
2	12	35	NEE	14.8	60.0	8.4	6.6	1084	943	-0.1025	-209		397
3	12	56	NEE	15.1	61.9	8.3	8.0	1020	943	-0.0248	-54		244
4	13	14 25	NEE	13.1	58.4	1.3	5.1	1296	943	-0.0099	-26		420
1	13	25	ER	14.8	25.4	5.9	3.2	0	943	0.1116	-08	249	2.37
2	12	44	ER	13.8	60.0	8.4	6.6	20	943	0.0916		188	
3	13	5	ER	12.1	61.9	8.3	8.0	3	943	0.0872		191	
4	13	24	ER	15.0	58.4	7.3	5.1	0	943	0.1510		394	
5	13	44	ER	16.4	58.8	6.6	3.1	27	944	0.0915		191	
6	14	2	NEE	15.1	59.5	8.8	7.6	537	944	-0.0438	-100		478
7	14	18	NEE	15.8	53.0	7.4	7.2	1152	944	-0.0275	-56		309
8	14	38	NEE	14.4	42.8	4.5	3.0	677	945	0.0098	22		123
9	14	57	NEE	12.5	44.6	6.0	3.9	774	945	-0.0072	-17		190
10	15	19	NEE ED	11.5	48.9	4.9	1./	908	945	0.0294	80	277	130
7	14	20	ED	14.0	52.0	7.4	7.0	0	045	0.1049		252	
8	14	47	FR	13.5	42.8	4.5	3.0	0	945	0.0647		145	
9	15	7	FR	10.7	44.6	6.0	3.9	0	945	0.0722		173	
10	15	30	ER	11.8	48.9	4.9	1.7	0	945	0.0773		209	
11	15	44	NEE	13.4	72.9	8.4	5.3	926	945	-0.0221	-48		249
12	16	6	NEE	14.5	62.8	9.4	6.2	926	945	0.0193	41		189
13	16	29	NEE	14.1	66.9	10.1	9.1	988	945	-0.0771	-163		450
14	16	52	NEE	13.8	59.3	9.7	7.9	389	946	-0.0341	-64		228
15	17	15	NEE	9.0	54.3	11.0	8.8	329	946	0.0274	75		200
11	15	55	ER	12.9	72.9	8.4	5.3	0	945	0.0920		201	
12	16	17	ER	14.1	62.8	9.4	6.2	0	945	0.1086		229	
13	16	41	ER	16.0	66.9	10.1	9.1	26	946	0.1369		287	
14	17	4	ER	10.6	59.3	9.7	7.9	0	946	0.0874		165	
15	17	26	ER	8.0	54.3	11.0	8.8	0	946	0.0999		275	
16	12	43	NEE	17.6	35.2	8.3	3.5	1335	947	0.0387	93		221
1/	13	2	NEE	18.5	67.1	4.5	1.8	904	946	0.0759	1/2		197
18	13	24	NEE	17.6	32.0	12.9	5.3	1246	946	0.0356	92		334
19	13	34	NEE	19.8	54.4 4E 4	13.8	4.5	0.05	946	0.0757	107		1/3
20	13	22	ED	16.4	45.0	0.9	2.5	020	940	0.0311	142	214	239
10	12	53	ED	10.0	67.1	4.5	1.0	10	947	0.1500		260	
18	12	15	ER	17.1	32.0	4.J	5.3	0	947	0.1627		126	
10	13	43	FR	19.6	54.4	12.7	4.5	1	946	0.1590		330	
20	14	11	FR	16.3	45.6	10.9	5.3	8	946	0.1433		401	
21	14	25	NFF	15.0	58.3	4.9	7.9	690	946	-0.0032	-9		331
22	14	44	NEE	13.0	50.8	9.6	5.0	555	946	0.0270	, 75		221
23	15	5	NEE	13.1	45.6	9.8	6.9	631	946	-0.1168	-316		629
24	15	31	NEE	12.7	46.4	8.1	5.1	509	946	-0.0819	-211		523
25	15	51	NEE	10.9	53.8	11.4	6.8	513	946	0.0385	110		164
21	14	35	ER	13.9	58.3	4.9	7.9	2	946	0.1168		322	
22	14	54	ER	12.2	50.8	9.6	5.0	17	946	0.1067		296	
23	15	19	ER	13.4	45.6	9.8	6.9	0	946	0.1162		314	
24	15	41	ER	11.4	46.4	8.1	5.1	0	946	0.1204		312	
25	16	0	ER	10.5	53.8	11.4	6.8	0	946	0.0957		273	
26	16	9	NEE	11.2	54.0	6.7	2.5	495	946	0.0199	57		229
27	16	29	NEE	14.9	45.3	8.4	4.5	1010	946	-0.0036	-10		268
28	16	49	NEE	13.7	54.4	6.7	3.9	458	946	0.0337	95		206
29	17	7	NEE	11.7	47.5	5.9	2.3	370	947	0.0155	43		162
30	1/	29	NEE	10.0	35.8	1.4	3.2	388	947	0.0760	208		130
26	16	19	ER	12.2	54.0	6.7	2.5	17	946	0.0998		286	
27	16	38	ER	15.9	45.3	8.4	4.5	1	946	0.0964		258	
28	16	59	ER	12.5	54.4	6./	3.9	0	947	0.1062		301	
29	17	41	ER	10.7 Q 1	47.5 35.8	5.9 7.4	2.3	0	947	0.0733		205	
50	17	71	1.15										

S.Table 7: CO<sub>2</sub>-flux measurements and environmental parameters on 24 and 25 May

Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope		CO₂ flu	x
											mg	CO2 m	<sup>2</sup> h <sup>-1</sup>
	hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
1	11	1	NEE	12.3	37.2	5.2	2.6	572	955	-0.0525	-119		324
2	11	16	NEE	11.1	25.9	4.5	1.9	533	955	-0.0456	-95		266
3	11	52 51	NEE	9.7	20.7	5.0	2.0	588	955	-0.0184	-41		201
4 5	12	8	NEE	9.6	26.7	3.1	2.0	665	955	-0.0380	- 104		273
1	11	9	ER	11.8	37.2	5.2	2.6	0	955	0.0896	,0	204	275
2	11	24	ER	10.0	25.9	4.5	1.9	0	955	0.0811		170	
3	11	41	ER	9.2	26.7	5.5	2.6	0	955	0.0717		160	
4	11	59	ER	9.1	35.8	5.1	2.0	0	955	0.0706		191	
5	12	17	ER	10.0	26.7	3.2	1.2	0	956	0.0818	150	177	120
0	12	27	NEE	10.6	31.1	8.1	3.2	713	955	-0.0651	-153		420
0	12	45	NEE	11.9	35.I 51.4	6.0	2.5	753	955	-0.0280	-59		334 251
9	13	2 19	NEE	11.7	21.0	5.8	2.4	546	956	0.0341	-32		180
10	13	37	NEE	9.3	35.9	6.6	1.8	494	956	0.0086	24		236
6	12	36	ER	11.2	31.1	8.1	3.2	18	955	0.1138	24	267	200
7	12	54	ER	11.6	35.1	6.0	2.5	0	956	0.1318		276	
8	13	11	ER	11.6	51.4	6.8	2.4	0	956	0.0962		220	
9	13	28	ER	9.9	21.0	5.8	2.7	0	956	0.1079		262	
10	13	46	ER	10.2	35.9	6.6	1.8	0	956	0.0940		259	05/
11	13	55	NEE	11.0	35.6	5.9	2.1	629	956	-0.0258	-57		256
12	14	12	NEE	13.1	30.0	0.1	2.4	690 E40	950	0.0014	3		198
13	14	30	NEE	13.3	20.7	72	4.0	526	956	-0.0182	-39		292
14	14	47	NEE	10.7	35.3	7.3 5.2	2.0	694	956	-0.0470	-73		201
11	14	3	FR	12.0	35.6	5.9	2.1	19	956	0.0895		199	021
12	14	20	FR	12.4	30.0	6.1	2.4	0	956	0.0936		201	
13	14	38	ER	12.3	20.7	11.1	4.5	7	956	0.1178		253	
14	14	56	ER	10.7	35.4	7.3	3.6	0	956	0.0987		188	
15	15	14	ER	10.5	35.3	5.2	2.2	0	956	0.0690		190	
16	15	23	NEE	9.8	27.2	5.9	2.7	430	956	0.0204	51		159
17	15	43	NEE	9.2	35.7	5.2	1.9	427	956	0.0175	41		166
18	16	4	NEE	9.8	31.0	5.3	2.2	677	956	-0.0205	-55		312
19	16	22	NEE	10.2	51.1	4.6	2.2	466	956	-0.0008	-2		319
20	16	42	NEE	12.0	39.6	10.5	4.2	890	956	0.0206	59		206
16	15	35	ER	9.7	27.2	5.9	2.7	0	956	0.0841		209	
17	15	54	ER	8.3	35.7	5.2	1.9	0	956	0.0875		208	
18	16	13	ER	9.9	31.0	5.3	2.2	17	956	0.0954		257	
19	16	32	ER	10.4	51.1	4.6	2.2	0	956	0.1464		317	
20	16	52	ER	13.2	39.6	10.5	4.2	0	956	0.0930		266	
21	12	43	NEE	25.5	34.2	11.0	2.9	1251	937	0.0037	10		213
22	13	2	NEE	20.1	50.7	7.1	3.1	860	937	-0.0445	-119		458
23	13	42	NEE	17.0	46.3	9.0	4.5	11/6	937	-0.0805	-220		030
24	14	42	NEE	20.4	40.3	7.7 12.4	4.1	1013	936	-0.0398	-147		730 170
23	12	53	FR	20.4	34.2	11.0	29	5	937	0.0839		223	170
22	13	12	FR	18.1	50.7	7.1	3.1	0	937	0.1260		339	
23	13	32	ER	18.1	63.4	9.0	4.5	0	937	0.2106		554	
24	13	53	ER	20.9	46.3	9.9	4.1	0	936	0.3145		780	
25	14	13	ER	19.0	43.3	12.4	4.7	0	936	0.0921		252	
26	14	23	NEE	20.1	36.9	10.3	5.1	1104	936	0.0609	168		487
27	14	43	NEE	23.6	28.0	9.7	3.6	1243	935	0.0560	144		402
28	15	0	NEE	22.9	30.9	11.6	3.4	739	935	0.0815	220		242
29	15	17	NEE	20.9	23.3	7.6	3.6	670	935	0.0217	58		427
30	15	36	NEE	20.3	28.2	11.1	5.6	1034	935	0.0643	168		334
26	14	34	ER	21.3	36.9	10.3	5.1	0	936	0.2382		655	
27	14	52	ER	23.1	28.0	9.7	3.6	0	935	0.2119		546	
28	15	10	ER	21.2	30.9	11.6	3.4	0	935	0.1701		462	
29	15	20	ER	19.9	23.3	7.0	5.6	0	930	0.1817		485	
211					10 1								

S.Table 8: CO<sub>2</sub>-flux measurements and environmental parameters on 2 and 5 Jun

Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	(	CO <sub>2</sub> flux	
											mg	CO2 m <sup>2</sup>	h⁻¹
	hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
1	11	49	NEE	17.5	30.8	13.6	3.2	517	945	-0.2512	-556		948
2	12	9	NEE	17.1	34.8	15.0	7.3	447	945	-0.1709	-347		706
3	12	28	NEE	16.0	57.4	13.2	5.8	442	945	-0.1246	-269		040
4	12	40	NEE	15.9	61.7	17.2	5.5	05/	945	-0.2190	-572		1198
5	13	5	FR	16.5	52.1 30.8	12.1	4.2	793 0	945	-0.2897	-607	393	1188
2	12	18	FR	16.3	34.8	15.0	7.3	0	945	0.1767		359	
3	12	37	ER	15.3	57.4	13.2	5.8	0	945	0.1738		376	
4	12	55	FR	15.7	61.7	17.2	5.5	0	945	0.2400		627	
5	13	15	ER	17.8	52.1	12.1	4.2	0	945	0.2784		581	
6	13	25	NEE	18.4	42.0	16.8	6.9	531	945	-0.1546	-350		953
7	13	43	NEE	19.3	34.8	13.6	4.5	621	945	-0.2217	-446		1100
8	14	10	NEE	19.6	29.9	14.1	4.4	481	945	-0.0628	-138		699
9	14	28	NEE	18.7	43.8	13.4	3.5	510	945	-0.0755	-176		565
10	14	48	NEE	16.7	36.3	16.9	4.3	524	945	-0.0845	-225		750
6	13	35	ER	18.4	42.0	16.8	6.9	0	945	0.2660		603	
/	14	2	ER	19.6	34.8	13.6	4.5	0	945	0.3251		654	
8	14	19	ER	19.0	29.9	14.1	4.4	0	945	0.2550		561	
9	14	39	ER	17.2	43.8	13.4	3.5	0	945	0.1665		389	
10	14	5/	ER NFF	16.7	36.3 71.4	16.9	4.3	0 469	945 945	-0.1050	-227	525	727
12	15	27	NFF	14.3	54.0	13.8	5.8	246	945	0.0352	74		403
13	15	46	NEE	12.7	46.8	13.0	5.3	246	945	-0.0098	-21		484
14	16	8	NEE	12.6	54.4	18.9	11.1	275	945	-0.0817	-153		625
15	16	27	NEE	12.7	40.2	17.8	8.5	243	945	0.0053	14		760
11	15	17	ER	15.1	71.4	12.5	5.4	0	945	0.2310		501	
12	15	37	ER	13.1	54.0	13.8	5.8	0	945	0.2250		477	
13	15	56	ER	12.4	46.8	13.0	5.3	0	945	0.2178		463	
14	16	17	ER	12.5	54.4	18.9	11.1	0	945	0.2520		472	
15	16	37	ER	12.4	40.2	17.8	8.5	0	945	0.2862		775	
16	12	2	NEE	29.3	21.0	17.5	8.4	1549	947	-0.2181	-504		1371
17	12	21	NEE	25.7	60.8	10.7	4.4	946	947	-0.1641	-364		1036
18	12	40	NEE	24.5	42.1	12.9	4.0	1113	947	-0.2626	-667		1572
19	12	58	NEE	23.3	41.9	12.8	3.5	1418	947	-0.1367	-280		936
20	13	16	NEE	23.4	27.9	15.7	4.9	905	947	-0.5306	-1450		2530
16	12	11	ER	27.8	21.0	17.5	8.4	0	947	0.3738		867	
17	12	31	ER	23.9	60.8	10.7	4.4	0	947	0.3014		672	
18	12	50	ER	22.7	42.1	12.9	4.0	0	947	0.3543		905	
19	13	7	ER	23.1	41.9	12.8	3.5	0	947	0.3193		655	
20	13	25	ER	24.4	27.9	15.7	4.9	0	947	0.3968		1080	
21	13	36	NEE	25.1	41.8	14.7	7.3	797	947	-0.0879	-233		949
22	13	54	NEE	24.4	42.0	14.5	5.5	1359	947	-0.1433	-382		1220
23	14	23	NEE	23.1	60.5	17.8	9.5	640	947	-0.3043	-795		1660
24	14	41	NEE	21.9	47.1	12.9	6.3	967	947	-0.4613	-1154		2139
25	14	58	NEE	20.3	50.5	15.3	6.3	448	947	-0.1279	-353		957
21	13	46	ER	23.5	41.8	14.7	7.3	0	947	0.2679		715	
22	14	15	ER	23.6	42.0	14.5	5.5	0	947	0.3142		839	
23	14	32	ER	22.0	60.5	17.8	9.5	0	947	0.3296		864	
24	14	50	ER	21.0	47.1	12.9	6.3	0	947	0.3928		985	
25	15	9	ER	19.1	50.5	15.3	6.3	0	947	0.2181	245	605	100/
26	15	18 21	NEE	18.5	08.0	10.0	5.9	483	947	-0.1229	-345		1006
27	15	30	NEE	1/.8	37.0	12.1	5.1	389	947	-0.0580	-154		193
28 20	15	54	NEE	10.4	48.8	15.0	5.3	380	947	-0.0868	-243		1079
29	10	1U 27	NEE	12.0	40.3 22 E	10.4	0.U	300	947	-0.0705	-210		077 501
30	10	21		10.1	22.0	10.1	4.0 E.O	524	747	0.0009	10	4/1	501
20	15	28	EK	17.0	08.0	10.0	5.9	0	947	0.2349		620	
27	15	40	EK	17.0	37.0	12.1	5.1	0	947	0.2393		039	
20	16	10	FD	15.7	46.0	16.4	6.0	0	0/7	0.2.702		680	
30	16	36	ER	14.6	22.5	15.1	4.8	0	947	0.2218		597	

S.Table 9:  $CO_2$ -flux measurements and environmental parameters on 16 and 17 Jun

Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	C	CO <sub>2</sub> flux	
											mg (	CO2 m <sup>2</sup>	h-1
	hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
1	15	40	NEE	15.0	41.1	10.2	7.0	449	947	-0.2553	-571		960
2	16	2	NEE	14.5	56.8	11.4	9.6	400	947	-0.2060	-422		854
3	10	22	NEE	18.6	47.0	12.7	8.9	774	947	-0.3233	-694		1245
4	16	39	NEE	20.8	51.8	8.9	6.5	/21	947	-0.1929	-496		1133
5	16	57	FR	20.6	41.2	11.6	8.6	1065	947	-0.4115	-852	389	1507
2	16	12	FR	16.4	56.8	11.4	9.6	0	947	0.2118		432	
3	16	31	FR	20.1	47.0	12.7	8.9	0	947	0.2579		551	
4	16	40	FR	20.1	51.8	8.9	6.5	0	947	0.2469		636	
5	17	6	FR	20.2	41.2	11.6	8.6	0	947	0.3180		655	
6	12	35	NEE	15.4	37.9	13.6	11.6	280	952	-0.0543	-125	000	703
7	12	51	NEE	15.6	34.3	13.3	12.4	631	952	-0.2494	-512		1078
8	13	8	NEE	16.5	28.5	12.1	10.8	333	952	-0.0604	-135		699
9	13	31	NEE	20.3	37.7	13.4	9.3	1317	952	-0.0906	-211		899
10	13	47	NEE	24.3	36.3	19.5	11.6	1362	952	-0.2305	-603		1144
6	12	43	ER	14.9	37.9	13.6	11.6	0	952	0.2501		578	
7	13	0	ER	16.3	34.3	13.3	12.4	0	952	0.2761		566	
8	13	15	ER	16.2	28.5	12.1	10.8	0	952	0.2520		564	
9	13	38	ER	22.3	37.7	13.4	9.3	0	952	0.2973		688	
10	13	56	ER	25.4	36.3	19.5	11.6	0	952	0.2075		541	40/5
11	14	5	NEE	25.0	58.3	19.0	12.2	1289	952	-0.2628	-555		1065
12	14	23	NEE	24.5	69.3	12.5	11.4	1337	952	-0.2783	-571		1271
13	14	43	NEE	26.7	40.2	18.7	13.8	1333	951	-0.2651	-540		1337
14	15	5	NEE	28.1	88.5	18.2	13.4	1157	951	-0.1965	-351		1232
15	15	23	NEE	27.5	54.8	16.8	11.2	1322	951	-0.4310	-1115		2442
11	14	15	ER	24.0	58.3	19.0	12.2	0	952	0.2411		511	
12	14	31	ER	25.9	69.3	12.5	11.4	0	951	0.3427		700	
13	14	55	ER	27.7	40.2	18.7	13.8	0	951	0.3927		/9/	
14	15	13	ER	27.0	88.5	18.2	13.4	0	951	0.4917		881	
15	15	32	ER	26.9	54.8	16.8	11.2	0	951	0.5122		1327	
16	15	44	NEE	26.9	35.4	16.5	13.4	966	952	-0.1537	-359		1019
1/	16	3	NEE	26.2	58.2	15.6	13.1	1164	951	-0.15/3	-349		992
18	16	22	NEE	25.1	38.3	16.9	10.4	1154	951	-0.2553	-650		1535
19	16	40	NEE	24.7	55.0	20.4	13.8	1136	951	-0.1507	-309		1035
20	10	57	NEE	24.1	66.5	20.0	11.9	886	952	-0.4320	-1184		2526
10	15	55	ER	26.0	35.4	10.5	13.4	0	952	0.2812		660	
17	10	12	ER	24.9	58.2	15.6	13.1	0	951	0.2877		642	
18	10	32	ER	24.8	38.3	10.9	10.4	0	952	0.3471		885	
19	10	48	ER	23.4	55.0	20.4	13.8	0	952	0.3524		1240	
20	17	0	ER	20.1	00.0	20.0	7.0	0	952	0.4932	507	1342	02/
21	11	5U 12	NEE	12.0	42.1	10.9	1.3	00/	947	-0.2119	-20/		930
22	12	13	NEE	13.4	63.2	12.5	8.1	525	947	-0.2115	-585		1024
23	12	49	NEE	15.9	79.5	11.8	9.7	534	947	-0.4121	-1104		1624
24	13	10	NEE	10.0	55.9	11.7	9.5	1303	947	-0.7115	-1812		2580
25	13	31	INEE	17.1	40.0	12.8	9.0	508	947	-0.2705	-/55	0.40	1075
21	12	2	ER	13.0	42.1	10.9	7.3	0	947	0.1259		348	
22	12	24	ER	13.0	03.2	12.5	8.1	0	947	0.1592		440	
23	13	0	EK	10.5	79.5	11.8	9.7	0	947	0.1947		520	
24	13	20	ER	18.7	55.9	11.7	9.5	0	947	0.3036		/68	
25 26	13	39	NEE	15.9	40.0	12.8	9.6	722	947	-0.2428	-691	320	1159
27	14	21	NFF	15.0	62.1	11.2	8.1	460	947	-0.2477	-665		1022
28	14	41	NFF	14.2	61.4	10.5	6.8	540	947	-0 2966	-836		1325
20	14	59	NFF	13.3	47.2	10.5	6.9	439	947	-0 2084	-576		981
30	15	18	NFF	14.5	63.6	95	6.1	560	947	-0.2397	-645		1135
26	14	11	FP	15.6	53.0	11.6	8.4	0	9/17	0.1650	0.0	468	
20	14	30	FR	14.5	62.1	11.0	8.1	0	947	0.1326		357	
28	14	49	FR	13.7	61.4	10.5	6.8	0	947	0.1730		489	
29	15	7	FR	13.3	47.2	10.0	6.9	0	947	0 1464		405	
30	15	27	ER	15.1	63.6	9.5	6.1	0	947	0.1825		490	

S.Table 10: CO<sub>2</sub>-flux measurements and environmental parameters on 28 and 29 Jun

Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	(	CO <sub>2</sub> flux	
											mg	CO2 m <sup>2</sup>	h⁻¹
	hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
1	12	31	NEE	11.1	51.8	9.3	6.8	504	949	-0.3852	-875		1218
2	12	49	NEE	11.2	48.0	10.7	6.5	486	949	-0.3381	-703		946
3	13	4	NEE	11.1	69.6	8.7	7.0	501	949	-0.4003	-884		1175
4	13	21	NEE	10.8	47.3	10.5	7.9	004	949	-0.3153	-841		11/4
5	13	40	ER	12.4	48.1 51.8	9.3	9.1 6.8	0	949	-0.5862	-1201	343	1247
2	12	56	ER	11.1	48.0	10.7	6.5	0	949	0.1171		243	
3	13	12	ER	10.7	69.6	8.7	7.6	0	949	0.1318		291	
4	13	29	ER	11.9	47.3	10.5	7.9	0	949	0.1253		333	
5	13	46	ER	13.1	48.1	11.1	9.1	0	949	0.1627		346	
6	11	4	NEE	9.5	23.5	11.4	7.6	421	949	-0.2864	-672		1102
7	11	23	NEE	10.2	32.5	9.3	7.0	442	949	-0.3045	-635		835
8	11	39	NEE	10.6	30.5	9.1	6.2	323	949	-0.1458	-332		581
9	11	55	NEE	10.5	71.3	9.1	6.2	471	949	-0.1452	-349		668
10	12	11	NEE	11.2	29.8	8.4	6.3	601	949	-0.3298	-900	420	1202
0	11	13	ER	10.0	23.5	0.2	7.0	0	949	0.1833		430	
,	11	17	ED	10.0	20.5	7.5	6.2	0	949	0.0750		250	
9	12	47	FR	10.4	50.5 71 3	9.1	6.2	0	949	0.1331		230	
10	12	10	FP	11.2	20.8	8.4	6.3	0	040	0.1107		302	
11	13	56	NEE	12.2	69.3	10.2	7.3	349	949	-0.2520	-554	502	848
12	14	13	NEE	12.6	76.9	12.6	7.9	589	949	-0.4675	-997		1286
13	14	31	NEE	12.2	83.8	14.9	9.8	451	949	-0.3363	-718		1062
14	14	52	NEE	11.9	97.0	11.6	9.1	369	949	-0.3763	-709		965
15	15	10	NEE	11.2	44.4	11.1	9.4	479	949	-0.5488	-1497		1940
11	14	5	ER	12.4	69.3	10.2	7.3	0	949	0.1339		294	
12	14	22	ER	12.9	76.9	12.6	7.9	0	949	0.1357		289	
13	14	41	ER	12.5	83.8	14.9	9.8	0	949	0.1614		344	
14	15	0	ER	11.4	97.0	11.6	9.1	0	949	0.1360		257	
15	15	22	ER	10.7	44.4	11.1	9.4	0	949	0.1622		443	
16	11	59	NEE	10.8	17.9	10.8	7.6	366	946	-0.1761	-432		942
17	12	21	NEE	11.6	24.3	8.4	7.6	531	946	-0.3380	-785		1200
18	12	42	NEE	12.0	24.0	11.0	7.2	357	946	-0.4185	-1108		1476
19	13	3	NEE	11.5	27.8	10.7	6.6	379	946	-0.2850	-608		881
20	13	20	NEE	11.2	16.7	9.7	7.9	385	946	-0.4816	-1371		1940
16	12	10	ER	10.9	17.9	10.8	7.6	0	946	0.2073		509	
17	12	32	ER	11.8	24.3	8.4	7.6	0	946	0.1787		415	
18	12	51	ER	11.7	24.0	11.0	7.2	0	946	0.1387		368	
19	13	11	ER	11.3	27.8	10.7	6.6	0	946	0.1278		273	
20	13	31	ER	12.1	16.7	9.7	7.9	0	946	0.2005		569	
21	15	14	NEE	13.2	68.1	12.6	10.4	302	946	-0.1531	-423		/62
22	15	54	NEE	10.9	/5.3	11.9	10.9	356	946	-0.2138	-596		822
23	10	10	NEE	10.5	95.2	12.5	10.9	317	946	-0.3215	-8/6		1234
24	10	28	NEE	11.0	73.2 20 E	12.1	0.5	388	947	-0.5033	-1403		1401
23	10	40	ED	11.7	27.3	13.5	7.5	/07	947	-0.3003	-1001	220	1401
21	15	23	FP	12.3	75.3	12.0	10.4	0	940	0.1223		226	
22	16	20	FP	10.7	95.2	12.5	10.9	0	9/6	0.1314		358	
23	16	37	FR	10.9	73.2	12.5	11.2	0	947	0 1908		496	
25	16	54	FR	12.0	29.5	13.5	9.5	0	947	0.1125		320	
26	13	45	NEE	14.8	20.9	10.2	9.1	927	946	-0.3580	-1018	020	1659
27	14	2	NEE	15.6	21.5	11.3	7.5	649	946	-0.2701	-723		938
28	14	18	NEE	13.8	35.7	11.7	7.7	422	946	-0.2063	-582		1014
29	14	36	NEE	12.0	34.4	11.0	8.2	514	946	-0.3062	-850		1053
30	14	55	NEE	13.2	26.6	13.1	8.4	578	946	-0.3666	-990		1680
26	13	54	ER	15.7	20.9	10.2	9.1	0	946	0.2264		641	
27	14	10	ER	14.5	21.5	11.3	7.5	0	946	0.0800		215	
28	14	27	ER	12.7	35.7	11.7	7.7	0	946	0.1528		433	
29	14	45	ER	12.5	34.4	11.0	8.2	0	946	0.0735		204	
30	15	3	ER	13.6	26.6	13.1	8.4	0	946	0.2558		690	

S.Table 11: CO<sub>2</sub>-flux measurements and environmental parameters on 4 and 5 Jul.

Norr         min         NEC / ER         'C         vol's         'C         C         min's         min's         ppm s <sup>-1</sup> NE         ER         GP           1         12         37         NEC         103         402         108         53         337         442         602382         4035         1113           4         13         24         NE         174         1172         112         86         448         442         602382         4037         1113           4         13         24         NE         174         1172         112         86         448         442         602384         437         86         448         442         602384         446         117         466         117         117         117         118         53         86         441         618         46         618         46         618         46         618         46         618         47         718         53         NE         113         445         116         44         47         738         744         747         747         748         748         74         747         748         748         748	Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	C	CO <sub>2</sub> flux	
												mg (	CO2 m <sup>2</sup>	h-1
1         12         37         MRE         18.3         92.2         11.8         57         887         442         4.222         4.49         1111           3         12         13         49         1112         114         1103         11.4         14.4         4.242         4.242         1103         1103           4         13         24         145         17.5         1103         11.4         4.4         4.4		hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
2         12         5.3         NEE         113         116         7.8         442         942         0.383         3.72         1101           4         113         24         NET         113         1101         5.4         444         492         0.313         6.0         7.7         7.7           5         13         24         MET         1174         1102         112         8.0         4.48         492         0.313         6.0         7.7         7.5           6         13         31         ER         17.3         1107         12.4         8.0         0         941         0.323         4.03           7         15         35         MEE         11.3         110.7         12.2         6.0         3.25         0.0         941         0.323         4.03         110           7         15         36         MEE         11.3         10.5         3.13         11.4         0.0         3.15         3.15         3.16         0.3         3.16         0.1         0.1         3.16         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1         0.1 <td>1</td> <td>12</td> <td>37</td> <td>NEE</td> <td>18.3</td> <td>92.2</td> <td>10.8</td> <td>5.7</td> <td>387</td> <td>942</td> <td>-0.2952</td> <td>-649</td> <td></td> <td>1114</td>	1	12	37	NEE	18.3	92.2	10.8	5.7	387	942	-0.2952	-649		1114
3         13         V         NEE         17.6         17.9         11.0         5.8         484         642         0.213         6.0         1232         6.0         1232         6.0         0.232         0.213         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.232         6.0         0.0	2	12	53	NEE	18.1	107.3	14.6	7.8	442	942	-0.3833	-772		1101
4         13         24         Not         11.4         10.9         13.3         80         448         942         0.0134         4.07           1         13         40         RR         17.7         10.73         14.8         7.8         0         941         0.0134         4.0         10.01           1         13         10         RR         17.7         10.73         14.8         7.8         0         941         0.0134         4.03           1         13         10         RR         17.3         10.72         12.2         6.0         9.91         0.0239         7.44         104           1         15         5         NEE         11.3         10.6         1.4         3.14         0.77         3.94         0.03         7.7         3.94         0.04         0.0239         7.44         10.04         10.04         10.05         10.04         5.0         3.25         0.77         3.94         0.75         3.90         7.8         3.48         16         0.2023         4.94         0.46         0.777         3.94         7.8         3.90         7.8         3.90         7.8         3.90         7.8         3.90	3	13	9	NEE	17.6	119.1	11.0	5.4	484	942	-0.4445	-952		1355
9         12         46         18         192         192         103         67         20         942         1043         403         403         403           1         13         16         FR         173         1191         110         54         0         942         0.1642         359           3         13         16         FR         173         1191         110         54         0         942         0.1642         359           4         15         36         KR         164         442         122         64         324         0.2788         424         1104           7         15         55         NEE         115         985         122         64         324         946         0.3797         394         756           9         16         29         NEE         104         106         101         53         311         947         0.143         348         10         946         0.2327         989         730         746           15         44         ER         123         1141         841         29         947         0.1440         346         36         <	4	13	24	NEE	17.4	107.2	13.2	8.0	448	942	-0.2193	-567		892
2         13         0         BR         17.7         103         14.6         13         0         941         0.122         0.23           4         13         31         18         RR         17.3         107.7         12.2         4.0         0         941         0.2578         4.03           5         13         34         BR         16.4         110.6         1.0         5.4         21.8         944         4.3298         -7.4         1048           6         15         50         NEE         11.5         94.5         102.2         6.4         21.4         4.4         0.00         10.1         5.3         21.4         -7.4         1048           7         16         42         NEE         10.4         10.4         5.4         0         944         0.2727         -899         13.0           10         16         45         NEE         10.4         5.4         0         944         0.2023         4.88         14.0           11         15         16         7.7         16.4         17.7         11.4         1.4         0.9023         4.89         1.0         1.0         1.0         1.0 <td>5</td> <td>13</td> <td>41</td> <td>FR</td> <td>17.0</td> <td>64.2 92.2</td> <td>12.3</td> <td>6.9 5.7</td> <td>322</td> <td>941</td> <td>-0.3234</td> <td>-6/3</td> <td>465</td> <td>1149</td>	5	13	41	FR	17.0	64.2 92.2	12.3	6.9 5.7	322	941	-0.3234	-6/3	465	1149
3         13         16         ER         17.3         17.9         17.10         8.4         0         942         0.1054         234           5         13         49         FR         56.6         64.7         17.3         49         0         941         0.1254         244           6         15         95         MLE         11.5         94.5         12.2         4.6         318         94.4         0.2278         -4.2         1110           7         15         95         MLE         11.5         94.5         12.2         4.6         32.5         94.4         0.4773         394         4.475           9         16         29         MFE         10.4         10.06         10.1         8.3         31.1         947         0.1273         394         4.475           9         16         20         MFE         10.4         10.6         10.4         20         0         944         0.1383         291         0.3         344         941         0.344         441           11         15         55         10.28         12.2         7.3         2.26         941         0.2074         444 <th< td=""><td>2</td><td>13</td><td>0</td><td>FR</td><td>17.7</td><td>107.3</td><td>14.6</td><td>7.8</td><td>0</td><td>941</td><td>0.1632</td><td></td><td>329</td><td></td></th<>	2	13	0	FR	17.7	107.3	14.6	7.8	0	941	0.1632		329	
4         13         33         18         17.3         107.2         12.3         40         941         92.34         92.4           6         15         36         NKE         11.43         11.09         10.4         5.4         31.8         94.6         0.2378         -6-12         11.0           7         15         35         NKE         10.9         84.5         10.5         5.0         22.5         947         -0.1373         -344         -0.04           8         16         12         NKE         10.4         10.4         11.4         5.3         31.1         94.0         -0.04         -0.02	3	13	16	FR	17.3	119.1	11.0	5.4	0	942	0.1883		403	
5         13         49         59         16         64/2         123         49         0         941         0.2789         -442         1110           7         15         55         MIE         115         965         122         4.6         318         944         -0.2789         -744         1048           8         16         12         MIE         10.4         10.05         10.1         5.3         311         947         -0.122         -390         754           9         16         29         MIE         10.4         10.05         10.1         5.3         311         947         0.3257         -390         734         675           6         15         44         FR         10.7         11.0         11.0         8.1         12.2         6.0         946         0.2237         -349         734           7         16         33         FR         10.3         10.0         10.1         10.1         8.0         0.0         947         0.1440         248         441           10         16         53         FR         10.2         11.4         8.4         257         941         0.2079 <td>4</td> <td>13</td> <td>31</td> <td>FR</td> <td>17.3</td> <td>107.2</td> <td>13.2</td> <td>8.0</td> <td>0</td> <td>941</td> <td>0.1254</td> <td></td> <td>324</td> <td></td>	4	13	31	FR	17.3	107.2	13.2	8.0	0	941	0.1254		324	
6       15       36       NIE       11.4       11.6       10.4       5.4       31.8       94.6       0.02788	5	13	49	ER	16.6	64.2	12.3	6.9	0	941	0.2279		475	
7       15       95       11.5       98.5       11.2       0.6       32.4       94.4       0.1393       7.44       1044         8       16       29       NEE       10.4       100.6       101.5       3       311       947       0.1393       7.394       675         9       16       29       NEE       10.4       100.6       10.1       5.3       311       947       0.3393       7.394       675         7       16       23       BR       11.1       94.5       10.2       66       0.0       947       0.142.7       44.8         8       16       20       RR       10.6       14.1       8.1       29       0.0       947       0.142.4       46.4         10       16       53       BR       12.4       11.4       8.1       29       0.0       947       0.164.4       471         11       16       53       BR       12.4       11.4       18       29       22.5       941       0.2034       441       941       0.2034       441       941       0.2034       441       941       0.2034       441       941       941       941       941	6	15	36	NEE	14.3	116.9	10.4	5.4	318	946	-0.2788	-642		1110
8         10         12         NEE         10.9         84.5         10.0         5.0         325         94.7         0.1737        394        677           10         45         NEE         10.6         11.41         8.1         2.9         055         94.7         0.1237        399         1340           6         15         44         ER         11.1         95.5         12.6         0.0         946         0.0237        399         1340           7         16         3         ER         10.4         84.5         10.5        6         0.0         946         0.0237        394        344           10         16         37         ER         10.3         100.6         10.1         5.3         0.0        447        446        447        446        446        447        446        447        446        44	7	15	55	NEE	11.5	98.5	12.2	6.6	324	946	-0.3593	-744		1048
9         6         29         NEE         10.4         100.6         10.1         5.3         311         947         0.3162         390         736           6         15         44         ER         127         116.9         10.4         5.4         0         946         0.3023         -468           7         16         20         ER         10.0         845         10.2         6.6         0         946         0.1228         6.8           9         16         20         ER         10.0         845         10.5         5.0         0         947         0.1028         222           10         15         58         ER         12.4         11.1         8.1         2.9         0.0         947         0.1024         446         801           12         16         27         NEE         15.5         10.28         12.2         7.3         22.6         941         0.0404         440         941         40.7         7.3           14         43         NEE         14.7         11.4         6.6         0.7         941         0.0404         941         0.1643         9139           14	8	16	12	NEE	10.9	84.5	10.5	5.0	325	947	-0.1737	-394		675
10       16       44       ER       12.7       11.6       3.6       2.9       505       947       0.23257       48.9       13.40         7       16       3       ER       11.1       98.5       12.2       6.6       0       946       0.2023       468         9       16       37       ER       10.0       648       100       947       0.1460       346         10       16       53       ER       12.4       11.4       8.1       2.9       0.947       0.1460       346         11       13       58       NEE       15.0       10.0       110.7       1.4       4.6       2.57       941       -0.2014       .444.6       801         12       14       12       NEE       15.0       100.5       10.7       5.2       226       941       -0.0140       .718       .718         14       14       14       14       118       12       2.258       941       -0.1466       .507       .737       .737       .737       .737       .737       .737       .737       .737       .737       .737       .737       .741       .741.2331       .741       .73333	9	16	29	NEE	10.4	100.6	10.1	5.3	311	947	-0.1627	-390		736
6         15         44         ER         11.1         98.2         12.4         5.4         0         94.6         0.1672         46.8           8         16         20         ER         10.6         84.5         105         5.0         94.7         0.164.7         30.4           9         16         37         ER         10.3         100.6         10.1         5.3         0         94.7         0.164.7         43.1           10         15         58         NEE         10.0         11.4         46         2.7         94.1         0.2074         44.6         80.1           11         13         58         NEE         15.0         102.8         12.2         7.3         226         941         -0.104.4         80.17         7.4           13         14         27         NEE         15.1         103.8         8.3         24.1         94.1         0.0308         -57.0         7.34           15         1         NEE         14.2         104.0         13.0         8.3         0         94.1         0.146.4         30.3         13.1         13.4         14         14         14.2         14.4         14.8 </td <td>10</td> <td>16</td> <td>45</td> <td>NEE</td> <td>10.6</td> <td>114.1</td> <td>8.1</td> <td>2.9</td> <td>505</td> <td>947</td> <td>-0.3257</td> <td>-889</td> <td></td> <td>1340</td>	10	16	45	NEE	10.6	114.1	8.1	2.9	505	947	-0.3257	-889		1340
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	6	15	44	ER	12.7	116.9	10.4	5.4	0	946	0.2023		468	
B         IO         LH         IOO         B4 5         IOO         IO         IO <thi< td=""><td>/</td><td>16</td><td>3</td><td>ER</td><td>11.1</td><td>98.5</td><td>12.2</td><td>6.6</td><td>0</td><td>946</td><td>0.1467</td><td></td><td>304</td><td></td></thi<>	/	16	3	ER	11.1	98.5	12.2	6.6	0	946	0.1467		304	
9         10         15         10         14         8.1         2.9         0         947         0.1644         451           11         13         58         NEE         16.0         110.7         11.4         6.6         257         941         0.2074         .446         801           12         14         12         NEE         15.5         10.2         12.2         7.3         226         941         0.2074         .446         801           13         14         27         NEE         15.6         10.7         5.9         225         941         0.2080         .570         734           15         1         NEE         14.2         104.0         13.0         8.3         241         941         0.2080         .570         734           13         14         45         ER         14.2         104.0         13.0         8.3         241         941         0.1541         323         .311           14         14         52         ER         14.4         14.8         10.9         5.3         755         945         .04132         .1001         14.3           17         14         18	8	16	20	ER	10.6	84.5	10.5	5.0	0	947	0.1238		281	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	9	10	37	ER	10.3	100.6	10.1	5.3	0	947	0.1440		340	
12         14         12         NEE         155         102.8         122         7.3         226         941         -0.2109         -4.42         744           13         14         27         NEE         15.1         103.5         10.7         5.9         225         941         -0.9109         -570         734           15         1         NEE         14.7         114.4         118         7.2         258         941         -0.2009         -618         1397           14         4         5         ER         15.6         110.7         11.4         6.6         0         941         0.1646         325           12         14         19         ER         15.2         102.8         12.2         7.3         0         941         0.1646         323           13         14         35         ER         14.4         114.8         7.2         0         941         0.0887         7.09         7.0         1431           15         5         9         ER         14.4         14.8         7.0         941         0.0887         -141         3.08         14.13         1199         1431         159	10	16	53 58	ER NFF	12.4	114.1	8.1	2.9	257	947	0.1664	-446	451	801
13         14         27         NEE         15.1         103.5         10.7         5.9         225         941         -0.1941         -407         718           14         14         43         NEE         14.7         114.4         118         7.2         256         941         -0.1941         -407         718           15         15         1         NEE         14.2         104.0         13.0         8.3         241         941         -0.209         -418         1397           11         14         5         ER         152         102.8         12.7         0         941         0.1646         323           13         14         26         ER         14.4         114.8         17.7         0         941         0.0887         -164           15         5         9         ER         14.4         114.0         118         12.2         0         941         0.0887         -101         14.11           14         18         NEE         12.9         91.1         10.9         6.3         484         945         -0.088         -945         1308           15         14         37 <td< td=""><td>12</td><td>14</td><td>12</td><td>NFF</td><td>15.5</td><td>102.8</td><td>12.2</td><td>7.3</td><td>226</td><td>941</td><td>-0.2109</td><td>-442</td><td></td><td>764</td></td<>	12	14	12	NFF	15.5	102.8	12.2	7.3	226	941	-0.2109	-442		764
14       14       14       14.7       114.4       11.8       7.2       258       941       -0.3080       -570       734         15       15       1       NEE       14.2       104.0       13.0       8.3       241       941       -0.2399       -618       1377         12       14       19       ER       15.2       102.8       12.2       7.3       0       941       0.164.6       355         13       14       36       ER       14.9       10.5       10.7       5.9       0       941       0.1683       311         14       14       52       ER       14.4       11.8       7.2       0       941       0.0887       164         15       7       ER       14.2       104.0       13.0       8.3       0       941       0.0208       777         16       13       51       NEE       14.4       44.8       10.9       5.3       76.5       945       0.4132       -1001       1431         17       14       54       NEE       11.4       44.8       10.9       5.3       0       945       0.1565       3.3.3         18       <	13	14	27	NFF	15.1	103.5	10.7	5.9	225	941	-0.1941	-407		718
15         15         1         NEE         142         1040         130         8.3         241         941         -0.2309         -6.18         1397           11         14         5         ER         15.6         110.7         11.4         6.6         0         941         0.1646         335           13         14         36         ER         14.9         103.5         10.7         5.9         0         941         0.1483         311           14         14         52         ER         14.4         114.4         118         7.2         0         941         0.0887         10.4           15         5         9         ER         14.4         114.4         11.8         7.2         0         941         0.0887         10.4           16         13         51         NEE         14.4         44.8         10.9         5.3         76.5         945         -0.408         945         10.0         11.3         1899           14         37         NEE         13.2         11.4.3         11.5         5.9         945         0.1772         430           14         27         ER         12.1<	14	14	43	NFF	14.7	114.4	11.8	7.2	258	941	-0.3080	-570		734
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	15	15	1	NEE	14.2	104.0	13.0	8.3	241	941	-0.2309	-618		1397
$        \begin{array}{ccccccccccccccccccccccccccccc$	11	14	5	ER	15.6	110.7	11.4	6.6	0	941	0.1646		355	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	12	14	19	FR	15.2	102.8	12.2	7.3	0	941	0.1541		323	
	13	14	36	ER	14.9	103.5	10.7	5.9	0	941	0.1483		311	
15159ER14.2104.013.08.309410.2908779161351NEE14.444.810.95.3765945-0.4132-100114.31171418NEE12.991.110.96.3484945-0.4088-9451308181437NEE13.2114.311.55.9895946-0.558-14.131899191454NEE14.696.810.74.3522946-0.7247-20462532161359ER14.44.810.95.309450.1765363161359ER14.44.810.96.309450.1665363171427ER12.191.110.96.309450.1665363181446ER15.7114.311.55.909460.1725486201521ER14.290.112.46.709460.1725486211518NEE13.7113.812.06.8202941-0.053-151433221534NEE13.7113.812.06.8202941-0.1674-50399524164NEE13.7113.812.0 <t< td=""><td>14</td><td>14</td><td>52</td><td>ER</td><td>14.4</td><td>114.4</td><td>11.8</td><td>7.2</td><td>0</td><td>941</td><td>0.0887</td><td></td><td>164</td><td></td></t<>	14	14	52	ER	14.4	114.4	11.8	7.2	0	941	0.0887		164	
16         13         51         NEE         14.4         44.8         10.9         5.3         765         945         -0.4132         -1001         1431           17         14         18         NEE         12.9         91.1         10.9         6.3         484         945         -0.4088         .945         1308           18         14         37         NEE         12.2         114.3         15         5.9         895         946         -0.4538         -1413         189           19         14         54         NEE         13.5         61.7         10.0         4.7         1020         946         -0.2247         -2046         2532           16         13         59         ER         14.4         44.8         10.9         5.3         0         945         0.1662         363           17         14         27         ER         13.1         96.8         10.7         4.3         0         945         0.1662         486           19         15         2         ER         13.1         96.8         10.7         4.3         0         945         0.1662         486           20         <	15	15	9	ER	14.2	104.0	13.0	8.3	0	941	0.2908		779	
17       14       18       NEE       12.9       91.1       10.9       6.3       484       945       -0.4088      945       1308         18       14       37       NEE       13.2       114.3       11.5       5.9       895       946       -0.5358       -1413       1899         19       14       54       NEE       13.5       61.7       10.0       4.7       1020       946       -0.7247       -2046       2532         16       13       59       ER       14.4       44.8       10.9       5.3       0       945       0.1772       430         17       14       27       ER       12.1       91.1       10.9       6.3       0       945       0.1662       486         19       15       2       ER       13.1       96.8       10.7       4.3       0       946       0.1058       224       20         21       15       34       NEE       14.2       60.1       12.4       6.7       222       941       -0.0533       -151       433         22       15       34       NEE       13.8       88.6       12.1       7.3       185	16	13	51	NEE	14.4	44.8	10.9	5.3	765	945	-0.4132	-1001		1431
18         14         37         NEE         13.2         114.3         11.5         5.9         895         946         -0.5358         -1413         1899           19         14         54         NEE         14.6         96.8         10.7         4.3         522         946         -0.4599         -971         1195           20         15         12         NEE         13.5         61.7         10.0         4.7         1020         946         -0.4599         -971         1195           16         13         59         FR         14.4         44.8         10.9         5.3         0         945         0.1727         430           17         14         27         FR         12.1         91.1         10.9         6.3         0         945         0.1565         363           18         14         46         FR         13.1         96.8         10.7         4.3         0         946         0.1565         363           19         15         21         FR         14.2         90.1         12.4         6.7         222         941         0.0553         -151         433           20 <t< td=""><td>17</td><td>14</td><td>18</td><td>NEE</td><td>12.9</td><td>91.1</td><td>10.9</td><td>6.3</td><td>484</td><td>945</td><td>-0.4088</td><td>-945</td><td></td><td>1308</td></t<>	17	14	18	NEE	12.9	91.1	10.9	6.3	484	945	-0.4088	-945		1308
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	18	14	37	NEE	13.2	114.3	11.5	5.9	895	946	-0.5358	-1413		1899
20         15         12         NEE         13.5         61.7         10.0         4.7         1020         946         -0.7247         -2.046         2532           16         13         59         ER         14.4         44.8         10.9         5.3         0         945         0.1772         430           17         14         27         ER         12.1         91.1         10.9         6.3         0         945         0.1665         363           18         14         46         ER         15.7         114.3         11.5         5.9         0         945         0.1662         466           19         15         2         ER         13.1         96.8         10.7         4.3         0         946         0.1058         224           20         15         21         ER         14.2         90.1         12.4         6.7         222         941         -0.053         -151         433           22         15         49         NEE         13.7         113.8         12.0         6.8         202         941         -0.0811         -3.2         956           23         15         56 <td>19</td> <td>14</td> <td>54</td> <td>NEE</td> <td>14.6</td> <td>96.8</td> <td>10.7</td> <td>4.3</td> <td>522</td> <td>946</td> <td>-0.4599</td> <td>-971</td> <td></td> <td>1195</td>	19	14	54	NEE	14.6	96.8	10.7	4.3	522	946	-0.4599	-971		1195
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	20	15	12	NEE	13.5	61.7	10.0	4.7	1020	946	-0.7247	-2046		2532
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	16	13	59	ER	14.4	44.8	10.9	5.3	0	945	0.1772		430	
181446ER15.7114.311.55.909450.186248619152ER13.196.810.74.309460.1058224201521ER14.261.710.04.709460.1725486211534NEE14.290.112.46.7222941-0.0553-151433221534NEE13.888.612.17.3185942-0.0831-228465231549NEE13.7113.812.06.8202941-0.1874-50399524164NEE13.7113.211.06.5190942-0.0691-194483211525ER14.090.112.46.709410.1025281221541ER13.6113.812.06.809410.1834492241612ER13.6113.812.06.809410.1834492231556ER13.6113.812.06.809410.1834492241612ER13.6113.812.06.809410.1834492241612ER13.6113.812.06.809410.	17	14	27	ER	12.1	91.1	10.9	6.3	0	945	0.1565		363	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	18	14	46	ER	15.7	114.3	11.5	5.9	0	945	0.1862		486	
201521ER14.261.710.04.709460.1725486211518NEE14.290.112.46.7222941-0.0553-151433221534NEE13.888.612.17.3185942-0.0831-228465231549NEE13.7113.812.06.8202941-0.1874-50399524164NEE13.7113.211.06.5190942-0.2062-528936251620NEE13.699.911.66.1167942-0.0691-194483211525ER14.090.112.46.709410.1025281221541ER13.688.612.17.309420.0862237231556ER13.6113.812.06.809410.1834492241612ER13.6113.211.06.509420.0862237231556ER13.6113.211.06.509420.1027289241612ER13.6113.211.06.109420.1027289261234NEE11.193.712.14.8330 <td>19</td> <td>15</td> <td>2</td> <td>ER</td> <td>13.1</td> <td>96.8</td> <td>10.7</td> <td>4.3</td> <td>0</td> <td>946</td> <td>0.1058</td> <td></td> <td>224</td> <td></td>	19	15	2	ER	13.1	96.8	10.7	4.3	0	946	0.1058		224	
21       15       18       NEE       14.2       90.1       12.4       6.7       222       941       -0.0553       -151       433         22       15       34       NEE       13.8       88.6       12.1       7.3       185       942       -0.0831       -228       465         23       15       49       NEE       13.7       113.8       12.0       6.8       202       941       -0.1874       -503       995         24       16       4       NEE       13.7       113.2       11.0       6.5       190       942       -0.2062       -528       936         25       16       20       NEE       13.6       99.9       11.6       6.1       167       942       -0.0691       -194       483         21       15       25       ER       14.0       90.1       12.4       6.7       0       941       0.1025       281         22       15       41       ER       13.6       113.8       12.0       6.8       0       941       0.1834       492         23       15       56       ER       13.6       113.2       11.0       6.5       0	20	15	21	ER	14.2	61.7	10.0	4.7	0	946	0.1725		486	
22       15       34       NEE       13.8       88.6       12.1       7.3       185       942       -0.0831       -228       465         23       15       49       NEE       13.7       113.8       12.0       6.8       202       941       -0.1874       -503       995         24       16       4       NEE       13.7       113.2       11.0       6.5       190       942       -0.262       -528       936         25       16       20       NEE       13.6       99.9       11.6       6.1       167       942       -0.0691       -194       483         21       15       25       ER       13.6       99.9       11.6       6.1       167       942       0.0691       -194       483         22       15       41       ER       13.6       88.6       12.1       7.3       0       941       0.1834       492       -         23       15       56       ER       13.6       113.2       11.0       6.5       0       941       0.1834       492         24       16       12       ER       13.3       99.9       11.6       6.1 <td< td=""><td>21</td><td>15</td><td>18</td><td>NEE</td><td>14.2</td><td>90.1</td><td>12.4</td><td>6.7</td><td>222</td><td>941</td><td>-0.0553</td><td>-151</td><td></td><td>433</td></td<>	21	15	18	NEE	14.2	90.1	12.4	6.7	222	941	-0.0553	-151		433
23       15       49       NEE       13.7       113.8       12.0       6.8       202       941       -0.1874       -503       995         24       16       4       NEE       13.7       113.2       11.0       6.5       190       942       -0.2062       -528       936         25       16       20       NEE       13.6       99.9       11.6       6.1       167       942       -0.0691       -194       483         21       15       25       ER       14.0       90.1       12.4       6.7       0       941       0.1025       281         22       15       41       ER       13.6       88.6       12.1       7.3       0       942       0.0862       237         23       15       56       ER       13.6       113.8       12.0       6.8       0       941       0.1834       492       24         24       16       12       ER       13.6       113.2       11.0       6.5       0       942       0.1027       289         26       12       34       NEE       11.1       93.7       12.1       4.8       330       945       -0.	22	15	34	NEE	13.8	88.6	12.1	7.3	185	942	-0.0831	-228		465
24       16       4       NEE       13.7       113.2       11.0       6.5       190       942       -0.2062       -528       936         25       16       20       NEE       13.6       99.9       11.6       6.1       167       942       -0.0691       -194       483         21       15       25       ER       14.0       90.1       12.4       6.7       0       941       0.1025       281         22       15       41       ER       13.6       88.6       12.1       7.3       0       942       0.0862       237         23       15       56       ER       13.6       113.8       12.0       6.8       0       941       0.1834       492         24       16       12       ER       13.6       113.2       11.0       6.5       0       942       0.1027       289         26       12       34       NEE       11.1       93.7       12.1       4.8       330       945       -0.1656       -476       884         27       12       50       NEE       16.8       86.9       9.5       4.4       1208       945       -0.5413 <td< td=""><td>23</td><td>15</td><td>49</td><td>NEE</td><td>13.7</td><td>113.8</td><td>12.0</td><td>6.8</td><td>202</td><td>941</td><td>-0.1874</td><td>-503</td><td></td><td>995</td></td<>	23	15	49	NEE	13.7	113.8	12.0	6.8	202	941	-0.1874	-503		995
25       16       20       NEE       13.6       99.9       11.6       6.1       167       942       -0.0691       -194       483         21       15       25       ER       14.0       90.1       12.4       6.7       0       941       0.1025       281         22       15       41       ER       13.6       88.6       12.1       7.3       0       942       0.0862       237         23       15       56       ER       13.6       113.8       12.0       6.8       0       941       0.1834       492         24       16       12       ER       13.6       113.2       11.0       6.5       0       942       0.1027       289         26       12       34       NEE       11.1       93.7       12.1       4.8       330       945       -0.1656       -476       884         27       12       50       NEE       11.9       95.6       9.4       4.7       1212       946       -0.4595       -1246       1630         28       13       5       NEE       16.8       86.9       9.5       4.4       1208       945       -0.4159 <t< td=""><td>24</td><td>16</td><td>4</td><td>NEE</td><td>13.7</td><td>113.2</td><td>11.0</td><td>6.5</td><td>190</td><td>942</td><td>-0.2062</td><td>-528</td><td></td><td>936</td></t<>	24	16	4	NEE	13.7	113.2	11.0	6.5	190	942	-0.2062	-528		936
21       15       25       ER       14.0       90.1       12.4       6.7       0       941       0.1025       281         22       15       41       ER       13.6       88.6       12.1       7.3       0       942       0.0862       237         23       15       56       ER       13.6       113.8       12.0       6.8       0       941       0.1834       492         24       16       12       ER       13.6       113.2       11.0       6.5       0       942       0.1027       289         26       12       34       NEE       11.1       93.7       12.1       4.8       330       945       -0.1656       -476       884         27       12       50       NEE       11.9       95.6       9.4       4.7       1212       946       -0.4595       -1246       1630         28       13       5       NEE       16.8       86.9       9.5       4.4       1208       945       -0.5413       -1509       2072         29       13       20       NEE       16.0       106.5       11.1       5.1       549       946       -0.4159	25	16	20	NEE	13.6	99.9	11.6	6.1	167	942	-0.0691	-194		483
22       15       41       ER       13.6       88.6       12.1       7.3       0       942       0.0862       237         23       15       56       ER       13.6       113.8       12.0       6.8       0       941       0.1834       492         24       16       12       ER       13.6       113.2       11.0       6.5       0       942       0.1595       408         25       16       28       ER       13.3       99.9       11.6       6.1       0       942       0.1027       289         26       12       34       NEE       11.1       93.7       12.1       4.8       330       945       -0.1656       -476       884         27       12       50       NEE       11.9       95.6       9.4       4.7       1212       946       -0.4595       -1246       1630         28       13       5       NEE       16.8       86.9       9.5       4.4       1208       945       -0.5413       -1509       2072         29       13       20       NEE       16.0       106.5       11.1       5.1       549       946       -0.4159	21	15	25	ER	14.0	90.1	12.4	6.7	0	941	0.1025		281	
23       15       56       ER       13.6       113.8       12.0       6.8       0       941       0.1834       492         24       16       12       ER       13.6       113.2       11.0       6.5       0       942       0.1595       408         25       16       28       ER       13.3       99.9       11.6       6.1       0       942       0.1027       289         26       12       34       NEE       11.1       93.7       12.1       4.8       330       945       -0.1656       -476       884         27       12       50       NEE       11.9       95.6       9.4       4.7       1212       946       -0.4595       -1246       1630         28       13       5       NEE       16.8       86.9       9.5       4.4       1208       945       -0.5413       -1509       2072         29       13       20       NEE       16.0       106.5       11.1       5.1       549       946       -0.4159       -1138       1545         30       13       35       NEE       13.9       88.2       12.4       4.8       355       945	22	15	41	ER	13.6	88.6	12.1	7.3	0	942	0.0862		237	
24         16         12         ER         13.6         113.2         11.0         6.5         0         942         0.1595         408           25         16         28         ER         13.3         99.9         11.6         6.1         0         942         0.1027         289           26         12         34         NEE         11.1         93.7         12.1         4.8         330         945         -0.1656         -476         884           27         12         50         NEE         11.9         95.6         9.4         4.7         1212         946         -0.4595         -1246         1630           28         13         5         NEE         16.8         86.9         9.5         4.4         1208         945         -0.5413         -1509         2072           29         13         20         NEE         16.0         106.5         11.1         5.1         549         946         -0.4159         -1138         1545           30         13         35         NEE         13.9         88.2         12.4         4.8         355         945         -0.2423         -652         1147	23	15	56	ER	13.6	113.8	12.0	6.8	0	941	0.1834		492	
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	24	16	12	ER	13.6	113.2	11.0	6.5	0	942	0.1595		408	
26       12       34       NEE       11.1       93.7       12.1       4.8       330       945       -0.1656       -476       884         27       12       50       NEE       11.9       95.6       9.4       4.7       1212       946       -0.4595       -1246       1630         28       13       5       NEE       16.8       86.9       9.5       4.4       1208       945       -0.5413       -1509       2072         29       13       20       NEE       16.0       106.5       11.1       5.1       549       946       -0.4159       -1138       1545         30       13       35       NEE       13.9       88.2       12.4       4.8       355       945       -0.2423       -652       1147         26       12       43       ER       11.2       93.7       12.1       4.8       0       945       0.1418       408         27       12       58       ER       15.2       95.6       9.4       4.7       0       945       0.1435       384         28       13       13       ER       16.8       86.9       9.5       4.4       0	25	16	28	ER	13.3	99.9	11.6	6.1	0	942	0.1027		289	
2/       12       50       NEE       11.9       95.6       9.4       4.7       1212       946       -0.4595       -1246       1630         28       13       5       NEE       16.8       86.9       9.5       4.4       1208       945       -0.4595       -1246       1630         29       13       20       NEE       16.0       106.5       11.1       5.1       549       946       -0.4159       -1138       1545         30       13       35       NEE       13.9       88.2       12.4       4.8       355       945       -0.2423       -652       1147         26       12       43       ER       11.2       93.7       12.1       4.8       0       945       0.1418       408         27       12       58       ER       15.2       95.6       9.4       4.7       0       945       0.1418       408         28       13       13       ER       16.8       86.9       9.5       4.4       0       945       0.2019       563         29       13       27       ER       16.8       86.9       9.5       4.4       0       945 <td< td=""><td>26</td><td>12</td><td>34</td><td>NEE</td><td>11.1</td><td>93.7</td><td>12.1</td><td>4.8</td><td>330</td><td>945</td><td>-0.1656</td><td>-476</td><td></td><td>884</td></td<>	26	12	34	NEE	11.1	93.7	12.1	4.8	330	945	-0.1656	-476		884
28       13       5       NEE       16.8       86.9       9.5       4.4       1208       945       -0.5413       -1509       2072         29       13       20       NEE       16.0       106.5       11.1       5.1       549       946       -0.4159       -1138       1545         30       13       35       NEE       13.9       88.2       12.4       4.8       355       945       -0.2423       -652       1147         26       12       43       ER       11.2       93.7       12.1       4.8       0       945       0.1418       408         27       12       58       ER       15.2       95.6       9.4       4.7       0       945       0.1435       384         28       13       13       ER       16.8       86.9       9.5       4.4       0       945       0.2019       563         29       13       27       ER       16.8       86.9       9.5       4.4       0       945       0.2019       563         29       13       27       ER       15.0       106.5       11.1       5.1       0       946       0.1485       40	27	12	50	NEE	11.9	95.6	9.4	4.7	1212	946	-0.4595	-1246		1630
29       13       20       NEE       16.0       106.5       11.1       5.1       549       946       -0.4159       -1138       1545         30       13       35       NEE       13.9       88.2       12.4       4.8       355       945       -0.2423       -652       1147         26       12       43       ER       11.2       93.7       12.1       4.8       0       945       0.1418       408         27       12       58       ER       15.2       95.6       9.4       4.7       0       945       0.1435       384         28       13       13       ER       16.8       86.9       9.5       4.4       0       945       0.2019       563         29       13       27       ER       15.0       106.5       11.1       5.1       0       946       0.1485       404         30       13       42       ER       15.0       106.5       11.1       5.1       0       946       0.1485       404	28	13	5	NEE	16.8	86.9	9.5	4.4	1208	945	-0.5413	-1509		2072
30       13       35       NEE       13.9       88.2       12.4       4.8       355       945       -0.2423       -652       1147         26       12       43       ER       11.2       93.7       12.1       4.8       0       945       0.1418       408         27       12       58       ER       15.2       95.6       9.4       4.7       0       945       0.1435       384         28       13       13       ER       16.8       86.9       9.5       4.4       0       945       0.2019       563         29       13       27       ER       15.0       106.5       11.1       5.1       0       946       0.1485       404         30       13       42       ER       12.9       88.2       12.4       4.8       0       946       0.1485       404 <td>29</td> <td>13</td> <td>20</td> <td>NEE</td> <td>16.0</td> <td>106.5</td> <td>11.1</td> <td>5.1</td> <td>549</td> <td>946</td> <td>-0.4159</td> <td>-1138</td> <td></td> <td>1545</td>	29	13	20	NEE	16.0	106.5	11.1	5.1	549	946	-0.4159	-1138		1545
26         12         43         ER         11.2         93.7         12.1         4.8         0         945         0.1418         408           27         12         58         ER         15.2         95.6         9.4         4.7         0         945         0.1418         408           28         13         13         ER         16.8         86.9         9.5         4.4         0         945         0.2019         563           29         13         27         ER         15.0         106.5         11.1         5.1         0         946         0.1485         408           30         13         42         ER         15.9         104.5         11.4         4.8         0         946         0.1485         404	30	13	35	NEE	13.9	88.2	12.4	4.8	355	945	-0.2423	-052		114/
27       12       58       EK       15.2       95.6       9.4       4.7       0       945       0.1435       384         28       13       13       ER       16.8       86.9       9.5       4.4       0       945       0.2019       563         29       13       27       ER       15.0       106.5       11.1       5.1       0       946       0.1485       408         30       13       42       FR       12.9       88.2       12.4       4.8       0       946       0.1830       404	26	12	43	ER	11.2	93./	12.1	4.8	0	945	0.1418		408	
26         13         13         EK         16.8         80.9         9.5         4.4         0         945         0.2019         563           29         13         27         ER         15.0         106.5         11.1         5.1         0         946         0.1485         408           30         13         42         FR         12.9         88.2         12.4         4.8         0         946         0.1830         404	27	12	58	ER	15.2	95.6	9.4	4./	0	945	0.1435		384	
27 13 27 EK 15.0 100.5 11.1 5.1 0 946 0.1485 408 30 13 42 FR 12.9 88.2 12.4 4.8 0 046 0.1830 404	28	13	13	EK	10.8	80.9 10/ F	9.5	4.4 E 1	0	945	0.2019		203	
	30	13	42	FR	12.9	88.2	12.4	4.8	0	946	0.1465		400	

S.Table 12: CO<sub>2</sub>-flux measurements and environmental parameters on 15 and 16 Jul

Norr         Min         NEK / ER         'C         vol %         C         C         Min*         mbar         ppm s <sup>-1</sup> NL         ER         C           1         15         5         NLK         227         71.9         104         11.4         76.9         03.47         73.9         103           4         15         5.9         NLK         23.7         71.9         104         11.4         74.9         03.47         73.9         103           4         15         5.9         NLK         23.5         77.0         13.5         14.7         40.7         04.8         0.0497         93.4         02.44         49.7           2         15         3         16         24.6         71.9         14.4         10         0.99.8         0.2447         93.4         0.244         10.8         10.2         11.4         10.8         0.2414         10.8         10.8         11.7         10.8         10.8         10.7         10.8         10.8         10.7         10.8         10.8         10.7         10.8         10.8         10.8         10.8         10.8         10.8         10.8         10.8         10.8         10.8         1	Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	(	CO <sub>2</sub> flux	
hour         min         NEE / ER         'C         val %         'C         'C         mbar //         ppm s <sup>1</sup> NEE         ER         GD           1         15         5         NRE         23.7         119         114         109         97.7         0.3487         0.9497         0.948         1187           4         15         52         16         55         16.7         0.77         0.77         0.97         0.2484         0.2497         0.244         0.444         0.444												mg	CO2 m <sup>2</sup>	h¹
1         15         5         NRE         2.2.7         7.1.9         19.4         17.4         7.99         9.73         0.3477         7.95         1193           2         15         27         MEE         22.23         0.1         2.0         1.1.4         2.11         4.8         5.71         5.8         0.377         7.93         1.4.6           4         10         5         1.8         1.4         4.01         6.97         0.3287         7.93         1.6.6           2         15         6.8         1.8         2.0         1.4.4         1.0         6.97         0.2384         7.93         1.6.6         7.4         7.0         1.6.6         0.9244         7.93         1.6.6         7.94		hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
2         15         21         NEE         2.7.7         56.4         2.4.3         18.3         46.5         967         0.2.707         7.98         1173           4         15         52         NEE         2.2.5         77.0         15.3         14.7         407         983         0.0274         5.77         73         72           5         16         0         NEE         2.2.5         77.0         15.3         14.7         407         983         0.0247         5.77         73         72           16         15         78         2.2.7         56.6         2.4.3         17.3         0         983         0.0247         955           5         16         2.2         RE         2.0.7         16.5         17.4         17.6         3.2.7         76.4         1.3.1         1.1.7         1.5.3         1.0.7         15.5         3.0.9         983         0.0.12.4         1.3.1         1.1.6         3.1.2         1.1.6         3.1.2         1.1.6         3.1.2         1.1.6         3.1.2         1.1.6         3.1.2         1.1.6         3.1.2         1.1.6         3.1.2         1.1.6         3.1.2         1.1.6         3.1.2         1.	1	15	5	NEE	23.7	71.9	19.4	17.4	769	957	-0.3487	-765		1387
3         4         4         102         53         40         63         57         63         64         67         57         67         77         105         143         0         953         67         67         67         67         67         67         67         67         67         67         68         0.212         78         74         175         140         0         98         0.2154         435         170         170         68         0.2154         335         171         175         340         0.81         0.2154         335         171         175         340         0.81         0.2154         335         171         175         340         0.81         0.2154         335         171         175         340         0.81         0.2154         335         171         176         0         98         0.2164         331         847         184         184	2	15	21	NEE	23.7	56.6	24.3	19.3	456	957	-0.2977	-598		1193
4         15         50         161         143         410         998         0.074         5.74         747           5         16         18         22.5         51.0         113         143         0         998         0.074         574         23           1         15         18         18         22.7         25.6         23.1         113         0         998         0.074         577         23         12.7           3         15         15         18         22.1         17.0         15.0         10.0         998         0.0215         -         44           6         16         23         NEE         17.0         15.0         10.0         998         -0.016         -2.49         1013           8         16         51         NEE         18.8         31.2         17.4         15.5         30.9         988         -0.036         -0.038         0.0316         -0.06         6.0         10.0         10.0         12.7         12.7         42.5         988         -0.030         -0.0         9.0         0.0333         HB3         14.6         14.9         10.0         10.0         10.0         10.0	3	15	37	NEE	22.7	87.1	20.1	14.8	521	958	-0.3707	-793		1608
5         65         63         64         63         63         63         63         63         63         63         63         63         63         63         63         63         63         63         64         63         63         64         63         63         64         63         64         63         64         63         64         63         64         63         64         63         64         63         63         63         63         63         63         63         63         63         63         63         63         63         63         63         63 </td <td>4</td> <td>15</td> <td>52</td> <td>NEE</td> <td>22.5</td> <td>77.0</td> <td>18.5</td> <td>14.7</td> <td>407</td> <td>958</td> <td>-0.0942</td> <td>-244</td> <td></td> <td>987</td>	4	15	52	NEE	22.5	77.0	18.5	14.7	407	958	-0.0942	-244		987
2         15         28         E8         227         56.6         213         193         0         958         0.2479         956           4         15         59         FR         214         77.0         155         147         0         958         0.2479         743           5         16         22         ME         195         555         174         176         321         958         0.2475         444           6         16         22         ME         195         555         174         176         558         0.0         958         0.2476         -463         1103           8         16         51         ME         188         540         122         179         988         0.1736         -240         667           17         29         MFE         122         446         122         177         425         978         0.2316         -3337         665           16         44         ER         190         450         122         177         0         988         0.2316         403         142           17         72         ER         294         66.0	5	16	6 13	FR	20.6	52.3 71.9	17.0	14.0	363	958	-0.2764	-579	623	1022
3         15         45         17         223         17         21         14         0         958         0.2027         743           5         16         32         17         20         55.3         170         140         0         958         0.2027         743         144         144         221         958         0.2155         744         144         221         958         0.2156         743         144         14         221         958         0.1156         343         958         0.1158         344         144         144         145         240         667         1227           7         16         37         NIE         192         468         112         174         155         389         958         0.1070         355         1448         160         585         174         174         155         0         958         0.2103         345         645           7         16         74         178         160         555         174         174         155         0         958         0.2321         643         1442           10         17         27         184         162         <	2	15	28	FR	22.7	56.6	24.3	19.3	0	958	0.2947		595	
4         15         59         ER         214         77.0         155         147         0         953         D2415         444           6         16         22         NIR         195         555         174         176         503         093         0215         444           6         16         27         MIR         195         555         174         176         530         953         02155         443         1101           8         16         51         NIR         188         312         174         155         369         953         01176         -243         647           10         17         20         NIR         188         50         174         170         0         953         0.1130         -333         645           8         16         58         ER         194         50         174         176         0         953         0.2130         645           11         17         12         ER         194         50         163         133         82         64           12         13         0.117         121         141         160         99	3	15	45	ER	23.1	87.1	20.1	14.8	0	958	0.3812		815	
5         16         12         KR         200         52.3         170         140         0.4         98         0.213	4	15	59	ER	21.4	77.0	18.5	14.7	0	958	0.2862		743	
6       16       23       NFE       195       55.5       17.4       17.6       3271       988       0.2154       -4.58       1103         8       16       57       NEE       18.8       31.2       17.4       15.5       389       988       -0.216       -4.288       103         9       17       25       NEE       18.8       31.2       17.4       15.5       389       988       -0.216       -4.48       .417       .55       17.4       17.6       978       -0.216       -3.75       6467         6       17       20       NEE       10.2       17.4       15.5       0       988       0.2385       -665       14.67         7       16       24       BR       18.4       17.4       17.5       0       988       0.3381       -337       -665         10       17       27       BR       19.0       54.0       16.2       11.9       0       988       0.3381       -8327       -66.0       13.2       13.2       13.3       13.2       13.2       13.2       13.2       13.2       15.5       16.6       989       0.3371       -64.0       132.4       13.2       14.2<	5	16	12	ER	20.0	52.3	17.0	14.0	0	958	0.2115		444	
7         16         37         NEE         19.3         4.0.0         16.7         15.5         38.9         988         -0.10%         -240         867           9         17         5         NEE         18.8         54.0         16.2         11.9         381         978         -0.1326         -315         667           10         17         20         NEE         18.4         55.5         17.4         17.6         0.0         958         -0.2169         -885         -647           7         16         29         BR         19.4         55.5         17.4         17.6         0.0         958         0.0384         -881         -           10         12         ER         19.0         16.0         16.2         17.7         0.0         958         0.0333         -82           11         12         46         NEE         22.4         40.6         16.2         10.7         90         -0.333         -6.03         14.2           13         13         NEE         27.4         7.6.9         17.8         16.0         959         -0.3177         -4.60         15.2           14         13         20 <td>6</td> <td>16</td> <td>23</td> <td>NEE</td> <td>19.5</td> <td>55.5</td> <td>17.4</td> <td>17.6</td> <td>321</td> <td>958</td> <td>-0.1554</td> <td>-356</td> <td></td> <td>1237</td>	6	16	23	NEE	19.5	55.5	17.4	17.6	321	958	-0.1554	-356		1237
8         10         51         NEE         18.8         31.2         17.4         15.5         38.9         98.8         0.0176         0.240         66.7           10         17         20         NEE         0.2         40.6         12.2         12.7         425         99.8         0.03265         66.7           6         16         24         ER         19.0         43.0         17.4         15.5         0.0         99.8         0.03265         66.5         14.0           10         17         21         ER         19.0         54.0         10.2         19.9         0.0         99.8         0.0325         66.5         12.2           10         17         27         ER         19.0         19.4         14.2         10.07         96.9         0.3321         48.0         12.2           11         12         25.9         MEE         27.4         77.9         12.1         18.1         86.0         99.9         0.3321         48.0         14.2           13         13         MEE         27.4         76.9         19.8         14.2         10.0         99.9         0.3221         48.0         14.122	7	16	37	NEE	19.3	43.0	16.7	15.5	360	958	-0.2146	-438		1103
9         17         5         NEE         16.8         54.0         11.2         11.9         381         648         0.1336         .515         .647           6         10         29         BR         19.4         55.5         17.4         17.6         0         958         0.2356         .555         1446           7         16         28         BR         19.4         55.5         17.4         17.5         0         958         0.2355         .665.           8         10         58         BR         18.8         31.2         17.4         15.5         0         958         0.2310         .627         17.7           10         17         27         BR         22.6         40.6         16.2         12.7         0         958         0.3333         .633         .442           12         25         NEE         22.4         40.6         16.9         9.0332         .603         1442           13         13         NEE         27.4         5.9         17.8         16.0         9.99         0.3372         .600         1532           14         13         3.0         RE         26.1         <	8	16	51	NEE	18.8	31.2	17.4	15.5	389	958	-0.1076	-240		867
10         17         20         MEE         10.2         11.2         11.7         40         958         0.3.249         -8.85         11.46           6         16         44         BR         10.0         43.0         11.67         15.5         0         958         0.3.255         665           9         17         12         IR         19.0         14.5         15.5         0         958         0.3.255         665           10         17         27         IR         19.0         14.2         11.9         0         958         0.3.33         40.3         1442           12         12         59         MEE         22.1         84.0         16.0         12.7         0         958         0.3.21         40.0         13.2           14         13         29         MEE         27.4         76.9         19.8         14.2         0         959         0.3.21         40.0         13.2           15         13         43         MEE         22.4         58.9         10.7         18.2         0         959         0.3.21         40.0         13.0           12         13         6.1	9	17	5	NEE	18.8	54.0	16.2	11.9	381	958	-0.1336	-315		687
6         10         29         RR         194         55.5         17.4         17.6         0         938         0.3349         881           8         16         58         RR         18.8         31.2         17.4         15.5         0         99.8         0.2315         665           9         17         12         ER         17.0         0.4         15.5         0         99.8         0.3333         882           10         17         27         ER         22.8         40.6         12.2         17.9         96.8         0.3333         882         12.4           11         12         45         MEE         22.1         84.4         17.6         12.9         105.9         99.0         0.3372         440         132.4           13         13         MEE         27.4         76.9         19.8         15.0         27.8         96.0         0.3372         -10.27         26.0           11         12         52         ER         22.0         71.7         17.7         18.1         0.999         0.3322         -10.27         26.0           13         3         0.0         ER         22.0	10	17	20	NEE	20.2	40.6	18.2	12.7	425	958	-0.2190	-585		1466
$  \begin{array}{ccccccccccccccccccccccccccccccccccc$	6	16	29	ER	19.4	55.5	17.4	17.6	0	958	0.3849		881	
B         16         BB         ER         188         312         1.4         15.5         0         988         0.2810         62/1           10         17         22         ER         190         540         16.2         119         0         988         0.3333         40.3         1442           12         12         45         NKE         252         80.7         17.8         14.2         1057         460         1532           13         13         NKE         27.7         71.7         17.1         15.1         8.8         499         -0.3321         -468         1522           14         13         29         NKE         27.4         76.9         198         15.0         878         460         -0.3321         -4680         1470           13         33         NKE         26.4         589         19.7         16.2         808         959         -0.3222         -674           13         30         ER         27.5         884         17.6         12.9         0         499         0.3321         -10.7         23.5           14         13         36         ER         27.0 <td< td=""><td>/</td><td>16</td><td>44</td><td>ER</td><td>19.0</td><td>43.0</td><td>16./</td><td>15.5</td><td>0</td><td>958</td><td>0.3255</td><td></td><td>665</td><td></td></td<>	/	16	44	ER	19.0	43.0	16./	15.5	0	958	0.3255		665	
9         17         12         ER         190         540         162         119         0         988         0.1581         372           10         17         27         ER         228         406         182         127         0         988         0.3333         682           11         12         12         59         NEE         2281         684         174         129         1959         999         0.3217         6409         1522           13         13         13         NEE         27.7         71.7         18.1         866         999         0.3312         640         1522           13         43         NEE         27.4         78.9         188         17.6         280         999         0.3922         674           13         13         20         ER         27.0         77.9         188         14.0         999         0.4770         863           14         13         S6         ER         27.0         77.9         188         17.0         999         0.0772         1333           15         13         51         ER         27.0         76.9         17.8	8	16	58	ER	18.8	31.2	1/.4	15.5	0	958	0.2810		627	
ID         ID <thid< th="">         ID         ID         ID<!--</td--><td>9</td><td>17</td><td>12</td><td>ER</td><td>19.0</td><td>54.0</td><td>16.2</td><td>11.9</td><td>0</td><td>958</td><td>0.1581</td><td></td><td>372</td><td></td></thid<>	9	17	12	ER	19.0	54.0	16.2	11.9	0	958	0.1581		372	
12         12         13         13         NEE         231         88.4         17.6         12.9         1059         999         -0.3177         -0.409         1324           13         13         NEE         27.7         71.7         21.7         18.1         866         999         -0.3121         -0.60         1532           15         13         43         NEE         27.4         7.69         18.9         16.0         0.999         -0.3212         -0.60         17.7         23.60           11         12         5         ER         26.9         80.7         198         16.2         80.8         999         0.3292         -0.027         2360           12         13         6         ER         27.0         7.69         188         15.0         999         0.4318         781           14         13         NEE         25.5         29.2         21.3         16.5         653         959         -0.1218         -275         1055           16         14         27         NEE         23.2         27.3         18.5         10.46         969         -0.2131         44.9         14.93         16.44         4.43 </td <td>10</td> <td>17</td> <td>27 45</td> <td>ER NFF</td> <td>22.8</td> <td>40.6</td> <td>18.2</td> <td>12.7</td> <td>0</td> <td>958</td> <td>-0.2833</td> <td>-603</td> <td>882</td> <td>1442</td>	10	17	27 45	ER NFF	22.8	40.6	18.2	12.7	0	958	-0.2833	-603	882	1442
13         13         13         NEE         22.7         71.7         21.7         18.1         866         999         -0.3221         -660         1532           14         13         29         NEE         21.4         76.9         198         150         876         960         -0.319         -460         1470           15         13         43         NEE         22.4         75.9         844         176         12.9         0         959         0.3792         840           12         13         6         ER         27.5         88.4         176         12.9         0         959         0.4318         781           13         13         20         ER         28.0         71.7         21.7         18.1         0         959         0.4318         781           14         13         36         ER         27.0         76.9         18.8         15.0         0         959         0.4318         781           15         13         14         77         16.2         0         959         0.2128         223         1055           16         14         42         7         15.5	12	12	59	NFF	28.1	88.4	17.6	12.9	1059	959	-0.3177	-649		1324
14         13         29         NEE         27.4         76.9         198         150         878         960         -0.3819         -0.400         1470           15         13         43         NEE         264         56.9         197         162         00         959         0.3922         -0.027         2840           12         13         6         ER         27.5         88.4         176         12.9         0         959         0.3922         67.4           13         320         ER         280         71.7         21.7         18.1         0         959         0.4170         853           16         13         59         NEE         25.5         29.2         21.3         18.5         107.6         959         0.0502         1333           17         14         13         NEE         25.5         29.2         21.3         18.5         107.6         959         0.0272         105.1           18         14         27         NEE         25.4         24.1         21.0         14.4         709         9.90         0.2131         4.39         12.8         16.69         3069         16.9         3	13	13	13	NEE	27.7	71.7	21.7	18.1	866	959	-0.3321	-680		1532
15         13         43         NEE         26.4         58.9         19.7         16.2         888         959         -0.3922         -10.27         2300           11         12         52         ER         26.9         80.7         19.8         142         0         959         0.3922         67.4           13         13         20         ER         22.0         76.9         19.8         15.0         0         959         0.4170         853           14         13         36         ER         22.0         76.9         19.8         15.0         0         959         0.0570         2311         1575           16         13         59         NEE         25.5         22.2         21.3         18.5         107.6         959         0.0576         -231         1575           17         14         13         NEE         25.6         44.4         21.0         14.4         769         -0.076         -231         1575           18         14         27         NEE         23.7         26.1         21.9         14.5         66.4         959         0.2131         43.9         12.38           14 <td>14</td> <td>13</td> <td>29</td> <td>NFF</td> <td>27.4</td> <td>76.9</td> <td>19.8</td> <td>15.0</td> <td>878</td> <td>960</td> <td>-0.3819</td> <td>-690</td> <td></td> <td>1470</td>	14	13	29	NFF	27.4	76.9	19.8	15.0	878	960	-0.3819	-690		1470
	15	13	43	NEE	26.4	58.9	19.7	16.2	808	959	-0.3922	-1027		2360
	11	12	52	ER	26.9	80.7	19.8	14.2	0	959	0.3972		840	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	12	13	6	FR	27.5	88.4	17.6	12.9	0	959	0.3292		674	
	13	13	20	ER	28.0	71.7	21.7	18.1	0	959	0.4170		853	
151351ER25158.919.716.209590.50721333161359NEE25.529.221.318.51076959-0.076-23115.75171413NEE24.032.117.915.5663959-0.1218-2751055181427NEE23.726.121.914.5604960-0.2686-6931689191443NEE25.645.421.014.4769959-0.2131.4391238201458NEE26.327.318.515.810.8959-0.6090-1668306916146ER24.929.221.318.509590.3450780181420ER23.532.117.915.509590.3450780181455ER24.226.121.914.409590.51481401211237NEE30.162.920.515.99590.5148140122156ER28.527.318.515.80959-0.3133.8301919241321NEE28.480.117.312.914.25957-0.3183.8301919241321NEE28.480.1	14	13	36	ER	27.0	76.9	19.8	15.0	0	959	0.4318		781	
16         13         59         NEE         25.5         29.2         21.3         18.5         1076         959         -0.0976         -2.31         1575           17         14         13         NEE         24.0         32.1         17.9         15.5         653         959         -0.1218         -275         1055           18         14         27         NEE         23.7         26.1         21.9         14.5         604         969         -0.2686         -0.2686         1689           19         14         43         NEE         25.6         45.4         21.0         14.4         769         959         -0.2186         -0.99         1668         3069           16         14         6         ER         24.9         29.2         21.3         18.5         0         959         0.4563         1344           17         14         20         ER         25.5         45.4         21.0         14.4         0         959         0.3456         976           18         14         35         ER         25.5         45.4         21.0         14.4         0         959         0.5148         1401         1	15	13	51	ER	25.1	58.9	19.7	16.2	0	959	0.5072		1333	
17       14       13       NEE       24.0       32.1       17.9       15.5       653       959       -0.1218       -275       1055         18       14       27       NEE       23.7       26.1       21.9       14.5       604       960       -0.2666       -693       1689         19       14       43       NEE       25.6       45.4       21.0       14.4       769       959       -0.2131       -439       1238         16       14       6       ER       24.9       29.2       21.3       18.5       0       959       0.5663       1344         17       14       20       ER       23.5       32.1       17.9       15.5       0       959       0.3450       700       16         18       14       35       ER       24.2       26.1       21.9       14.4       0       959       0.3874       798       100       14       101       11       101       11       101       11       101       11       101       11       101       11       101       11       101       11       101       11       11       11       121       145       14	16	13	59	NEE	25.5	29.2	21.3	18.5	1076	959	-0.0976	-231		1575
18         14         27         NEE         23.7         26.1         21.9         14.5         604         960         -0.2686         -693         1689           19         14         43         NEE         25.6         45.4         21.0         14.4         769         959         -0.2131         -439         1238           20         14         58         NEE         24.3         27.3         18.5         1048         959         -0.6000         -1668         3069           16         14         6         ER         24.9         29.2         21.3         18.5         0         959         0.5663         1344           17         14         20         ER         23.5         32.1         17.9         15.5         0         959         0.3866         996           19         14         50         ER         24.2         26.1         21.9         14.4         0         959         0.3874         7780           20         15         6         ER         28.5         27.3         18.5         15.8         0         959         0.3874         7171         454         1210           21	17	14	13	NEE	24.0	32.1	17.9	15.5	653	959	-0.1218	-275		1055
19         14         43         NEE         25.6         45.4         21.0         14.4         769         959         -0.2131         -4.39         1238           20         14         58         NEE         26.3         27.3         18.5         15.8         1048         959         -0.6090         -1668         3069           16         14         6         ER         24.9         29.2         21.3         18.5         0         959         0.3450         780           17         14         20         ER         22.5         45.4         21.0         14.4         0         959         0.3450         780           19         14         50         ER         25.5         45.4         21.0         14.4         0         959         0.3450         780           20         15         6         FR         28.5         27.3         18.5         15.8         0         959         0.5148         1401           21         12         37         NEE         28.8         83.2         20.6         16.0         303         958         -0.0539         -143         888           23         13         <	18	14	27	NEE	23.7	26.1	21.9	14.5	604	960	-0.2686	-693		1689
201458NEE26.327.318.515.81048959 $-0.6090$ $-1668$ 306916146ER24.929.221.318.509590.34501344171420ER23.532.117.914.509590.3864966191450ER25.545.421.014.409590.387479820156ER28.527.318.515.809590.51481401211237NEE30.162.920.515.9944958-0.171-454121022136NEE27.089.222.818.1890957-0.3183-8301919241321NEE28.480.117.312.91425957-0.6657-16472999251336NEE27.489.222.818.1890957-0.3183-8301919241321NEE28.454.121.816.41212957-0.2714-7371496211244ER29.862.920.515.99580.2700756221258ER26.783.220.616.009580.2700756221258ER26.783.220.5 </td <td>19</td> <td>14</td> <td>43</td> <td>NEE</td> <td>25.6</td> <td>45.4</td> <td>21.0</td> <td>14.4</td> <td>769</td> <td>959</td> <td>-0.2131</td> <td>-439</td> <td></td> <td>1238</td>	19	14	43	NEE	25.6	45.4	21.0	14.4	769	959	-0.2131	-439		1238
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	14	58	NEE	26.3	27.3	18.5	15.8	1048	959	-0.6090	-1668		3069
17         14         20         ER         23.5         32.1         17.9         15.5         0         959         0.3450         780           18         14         35         ER         24.2         26.1         21.9         14.5         0         960         0.3866         996           19         14         50         ER         25.5         45.4         21.0         14.4         0         959         0.3874         798           20         15         6         ER         28.5         27.3         18.5         15.8         0         959         0.5148         1401           21         12         37         NEE         28.8         83.2         20.6         16.0         303         958         -0.0539         -14.3         888           23         13         6         NEE         27.0         89.2         22.8         18.1         890         957         -0.0657         -1647         2999           25         13         36         NEE         28.4         85.1         12.18         16.4         1212         957         -0.2714         -737         1496           24         13	16	14	6	ER	24.9	29.2	21.3	18.5	0	959	0.5663		1344	
18         14         35         ER         24.2         26.1         21.9         14.5         0         960         0.3866         996           19         14         50         ER         25.5         45.4         21.0         14.4         0         959         0.3874         798           20         15         6         ER         28.5         27.3         18.5         15.8         0         959         0.5148         1401           21         12         51         NEE         28.8         83.2         20.6         16.0         303         958         -0.0539         -14.3         888           23         13         6         NEE         27.0         89.2         22.8         18.1         890         957         -0.3183         -830         1919           24         13         2.1         NEE         28.4         80.1         17.3         12.9         1425         957         -0.6677         -1647         2999           25         13         36         NEE         28.4         54.1         21.8         16.4         1212         957         -0.2714         -737         1496           21	17	14	20	ER	23.5	32.1	17.9	15.5	0	959	0.3450		780	
19         14         50         ER         25.5         45.4         21.0         14.4         0         959         0.3874         798           20         15         6         ER         28.5         27.3         18.5         15.8         0         959         0.5148         1401           21         12         37         NEE         30.1         62.9         20.5         15.9         944         958         -0.0739         -143         888           23         13         6         NEE         27.0         89.2         22.8         18.1         890         957         -0.3183         -830         1919           24         13         21         NEE         28.4         80.1         17.3         12.9         1425         957         -0.6657         -1647         2999           25         13         36         NEE         28.4         54.1         21.8         16.4         1212         957         -0.2714         -737         1496           21         12         44         ER         29.8         62.9         20.6         16.0         0         958         0.2860         756         22         12	18	14	35	ER	24.2	26.1	21.9	14.5	0	960	0.3866		996	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	19	14	50	ER	25.5	45.4	21.0	14.4	0	959	0.3874		798	
21       12       37       NEE       30.1       62.9       20.5       15.9       944       958       -0.1717       -454       1210         22       12       51       NEE       28.8       83.2       20.6       16.0       303       958       -0.0539       -143       888         23       13       6       NEE       27.0       89.2       22.8       18.1       890       957       -0.3183       -830       1919         24       13       21       NEE       28.4       80.1       17.3       12.9       1425       957       -0.6657       -1647       2999         25       13       36       NEE       28.4       54.1       21.8       16.4       1212       957       -0.2714       -737       1496         21       12       44       ER       29.8       62.9       20.5       15.9       0       958       0.2860       756         23       13       14       ER       27.4       89.2       22.8       18.1       0       957       0.4183       1089         24       13       29       ER       28.0       80.1       17.3       12.9	20	15	6	ER	28.5	27.3	18.5	15.8	0	959	0.5148		1401	
22       12       51       NEE       28.8       83.2       20.6       16.0       303       958       -0.0539       -143       888         23       13       6       NEE       27.0       89.2       22.8       18.1       890       957       -0.3183       -830       1919         24       13       21       NEE       28.4       80.1       17.3       12.9       1425       957       -0.6657       -1.647       2999         25       13       36       NEE       28.4       54.1       21.8       16.4       1212       957       -0.2714       -7.37       1496         21       12       44       ER       29.8       62.9       20.5       15.9       0       958       0.2860       756         23       13       14       ER       27.4       89.2       22.8       18.1       0       957       0.4183       1089         24       13       29       ER       28.0       54.1       21.8       16.4       0       957       0.5463       1353         25       13       43       ER       28.0       54.1       21.8       16.4       0       957 </td <td>21</td> <td>12</td> <td>37</td> <td>NEE</td> <td>30.1</td> <td>62.9</td> <td>20.5</td> <td>15.9</td> <td>944</td> <td>958</td> <td>-0.1717</td> <td>-454</td> <td></td> <td>1210</td>	21	12	37	NEE	30.1	62.9	20.5	15.9	944	958	-0.1717	-454		1210
23       13       6       NEE       27.0       89.2       22.8       18.1       890       957       -0.3183       -830       1919         24       13       21       NEE       28.4       80.1       17.3       12.9       1425       957       -0.6657       -1647       2999         25       13       36       NEE       28.4       54.1       21.8       16.4       1212       957       -0.2714       -737       1496         21       12       44       ER       29.8       62.9       20.5       15.9       0       958       0.2860       756         22       12       58       ER       26.7       83.2       20.6       16.0       0       958       0.2790       745         23       13       14       ER       27.4       89.2       22.8       18.1       0       957       0.4183       1089       1450         24       13       29       ER       28.0       54.1       21.8       16.4       0       957       0.4183       1089       1450         24       13       51       NEE       28.7       48.0       18.0       14.1       1098 <td>22</td> <td>12</td> <td>51</td> <td>NEE</td> <td>28.8</td> <td>83.2</td> <td>20.6</td> <td>16.0</td> <td>303</td> <td>958</td> <td>-0.0539</td> <td>-143</td> <td></td> <td>888</td>	22	12	51	NEE	28.8	83.2	20.6	16.0	303	958	-0.0539	-143		888
24       13       21       NEE       28.4       80.1       17.3       12.9       1425       957       -0.6657       -1647       2999         25       13       36       NEE       28.4       54.1       21.8       16.4       1212       957       -0.2714       -737       1496         21       12       44       ER       29.8       62.9       20.5       15.9       0       958       0.2860       756         22       12       58       ER       26.7       83.2       20.6       16.0       0       957       0.4183       1089         23       13       14       ER       27.4       89.2       22.8       18.1       0       957       0.4183       1089         24       13       29       ER       28.0       80.1       17.3       12.9       0       957       0.5463       1353         25       13       43       ER       28.0       54.1       21.8       16.4       0       957       -0.1815       -498       1450         26       13       51       NEE       28.7       48.0       18.0       14.1       1098       957       -0.0566 </td <td>23</td> <td>13</td> <td>6</td> <td>NEE</td> <td>27.0</td> <td>89.2</td> <td>22.8</td> <td>18.1</td> <td>890</td> <td>957</td> <td>-0.3183</td> <td>-830</td> <td></td> <td>1919</td>	23	13	6	NEE	27.0	89.2	22.8	18.1	890	957	-0.3183	-830		1919
25       13       36       NEE       28.4       54.1       21.8       16.4       1212       957       -0.2714       -737       1496         21       12       44       ER       29.8       62.9       20.5       15.9       0       958       0.2860       756         22       12       58       ER       26.7       83.2       20.6       16.0       0       958       0.2790       745         23       13       14       ER       27.4       89.2       22.8       18.1       0       957       0.4183       1089         24       13       29       ER       28.0       80.1       17.3       12.9       0       957       0.5463       1353         25       13       43       ER       28.0       54.1       21.8       16.4       0       957       0.2791       759         26       13       51       NEE       28.7       48.0       18.0       14.1       1098       957       -0.1815       -498       1450         27       14       6       NEE       30.4       34.2       20.0       15.4       619       957       -0.0566       -146	24	13	21	NEE	28.4	80.1	17.3	12.9	1425	957	-0.6657	-1647		2999
21       12       44       ER       29.8       62.9       20.5       15.9       0       958       0.2860       756         22       12       58       ER       26.7       83.2       20.6       16.0       0       958       0.2790       745         23       13       14       ER       27.4       89.2       22.8       18.1       0       957       0.4183       1089         24       13       29       ER       28.0       80.1       17.3       12.9       0       957       0.5463       1353         25       13       43       ER       28.0       54.1       21.8       16.4       0       957       0.2791       759         26       13       51       NEE       28.7       48.0       18.0       14.1       1098       957       -0.1815       -498       1450         27       14       6       NEE       30.4       34.2       20.0       15.4       619       957       -0.0566       -146       1265         28       14       20       NEE       27.2       32.3       18.8       16.9       436       958       -0.0946       -258	25	13	36	NEE	28.4	54.1	21.8	16.4	1212	957	-0.2714	-737		1496
22         12         58         ER         26.7         83.2         20.6         16.0         0         958         0.2790         745           23         13         14         ER         27.4         89.2         22.8         18.1         0         957         0.4183         1089           24         13         29         ER         28.0         80.1         17.3         12.9         0         957         0.5463         1353           25         13         43         ER         28.0         54.1         21.8         16.4         0         957         0.2791         759           26         13         51         NEE         28.7         48.0         18.0         14.1         1098         957         -0.1815         -498         1450           27         14         6         NEE         30.4         34.2         20.0         15.4         619         957         -0.0566         -146         1265           28         14         20         NEE         27.2         32.3         18.8         16.9         436         958         -0.0946         -258         1316           29         14	21	12	44	ER	29.8	62.9	20.5	15.9	0	958	0.2860		756	
23       13       14       ER       27.4       89.2       22.8       18.1       0       957       0.4183       1089         24       13       29       ER       28.0       80.1       17.3       12.9       0       957       0.5463       1353         25       13       43       ER       28.0       54.1       21.8       16.4       0       957       0.2791       759         26       13       51       NEE       28.7       48.0       18.0       14.1       1098       957       -0.1815       -498       1450         27       14       6       NEE       30.4       34.2       20.0       15.4       619       957       -0.0566       -146       1265         28       14       20       NEE       27.2       32.3       18.8       16.9       436       958       -0.0946       -258       1316         29       14       34       NEE       23.8       36.9       17.7       15.2       442       958       -0.1642       -443       1097         30       14       49       NEE       24.5       24.0       18.5       13.5       687       958 </td <td>22</td> <td>12</td> <td>58</td> <td>ER</td> <td>26.7</td> <td>83.2</td> <td>20.6</td> <td>16.0</td> <td>0</td> <td>958</td> <td>0.2790</td> <td></td> <td>745</td> <td></td>	22	12	58	ER	26.7	83.2	20.6	16.0	0	958	0.2790		745	
24         13         29         ER         28.0         80.1         17.3         12.9         0         957         0.5463         1353           25         13         43         ER         28.0         54.1         21.8         16.4         0         957         0.2791         759           26         13         51         NEE         28.7         48.0         18.0         14.1         1098         957         -0.1815         -498         1450           27         14         6         NEE         30.4         34.2         20.0         15.4         619         957         -0.0566         -146         1265           28         14         20         NEE         27.2         32.3         18.8         16.9         436         958         -0.0946         -258         1316           29         14         34         NEE         23.8         36.9         17.7         15.2         442         958         -0.1642         -443         1097           30         14         49         NEE         24.5         24.0         18.5         13.5         687         958         -0.2098         -552         1395	23	13	14	ER	27.4	89.2	22.8	18.1	0	957	0.4183		1089	
25         13         43         ER         28.0         54.1         21.8         16.4         0         957         0.2791         759           26         13         51         NEE         28.7         48.0         18.0         14.1         1098         957         -0.1815         -498         1450           27         14         6         NEE         30.4         34.2         20.0         15.4         619         957         -0.0566         -146         1265           28         14         20         NEE         27.2         32.3         18.8         16.9         436         958         -0.0946         -258         1316           29         14         34         NEE         23.8         36.9         17.7         15.2         442         958         -0.1642         -443         1097           30         14         49         NEE         24.5         24.0         18.5         13.5         687         958         -0.2098         -552         1395           26         13         58         ER         30.6         48.0         18.0         14.1         0         957         0.3493         952      <	24	13	29	ER	28.0	80.1	17.3	12.9	0	957	0.5463		1353	
20       13       51       NEE       28.7       48.0       18.0       14.1       1098       957       -0.1815       -498       1450         27       14       6       NEE       30.4       34.2       20.0       15.4       619       957       -0.0566       -146       1265         28       14       20       NEE       27.2       32.3       18.8       16.9       436       958       -0.0946       -258       1316         29       14       34       NEE       23.8       36.9       17.7       15.2       442       958       -0.0946       -258       1316         29       14       34       NEE       23.8       36.9       17.7       15.2       442       958       -0.0946       -252       1395         26       13       58       ER       30.6       48.0       18.0       14.1       0       957       0.3493       952         27       14       13       ER       28.9       34.2       20.0       15.4       0       958       0.4320       1120         28       14       27       ER       25.0       32.3       18.8       16.9       0	25	13	43	ER	28.0	54.1	21.8	16.4	0	957	0.2791	100	759	1.150
2/       14       6       NEE       30.4       34.2       20.0       15.4       619       957       -0.0566       -146       1265         28       14       20       NEE       27.2       32.3       18.8       16.9       436       958       -0.0946       -258       1316         29       14       34       NEE       23.8       36.9       17.7       15.2       442       958       -0.1642       -443       1097         30       14       49       NEE       24.5       24.0       18.5       13.5       687       958       -0.2098       -552       1395         26       13       58       ER       30.6       48.0       18.0       14.1       0       957       0.3493       952         27       14       13       ER       28.9       34.2       20.0       15.4       0       958       0.4320       1120         28       14       27       ER       25.0       32.3       18.8       16.9       0       958       0.3848       1058         29       14       41       ER       23.3       36.9       17.7       15.2       0       958	26	13	51	NEE	28.7	48.0	18.0	14.1	1098	957	-0.1815	-498		1450
28       14       20       NEE       27.2       32.3       18.8       16.9       436       958       -0.0946       -258       1316         29       14       34       NEE       23.8       36.9       17.7       15.2       442       958       -0.0946       -258       1316         30       14       49       NEE       24.5       24.0       18.5       13.5       687       958       -0.0946       -258       1395         26       13       58       ER       30.6       48.0       18.0       14.1       0       957       0.3493       952         27       14       13       ER       28.9       34.2       20.0       15.4       0       958       0.4320       1120         28       14       27       ER       25.0       32.3       18.8       16.9       0       958       0.3848       1058         29       14       41       ER       23.3       36.9       17.7       15.2       0       958       0.2419       654         30       14       55       FR       24.2       24.0       18.5       13.5       0       957       0.3205	27	14	6	NEE	30.4	34.2	20.0	15.4	619	957	-0.0566	-146		1265
29       14       34       NEE       23.8       36.9       17.7       15.2       442       958       -0.1642       -443       1097         30       14       49       NEE       24.5       24.0       18.5       13.5       687       958       -0.2098       -552       1395         26       13       58       ER       30.6       48.0       18.0       14.1       0       957       0.3493       952         27       14       13       ER       28.9       34.2       20.0       15.4       0       958       0.4320       1120         28       14       27       ER       25.0       32.3       18.8       16.9       0       958       0.3848       1058         29       14       41       ER       23.3       36.9       17.7       15.2       0       958       0.2419       6554         30       14       55       FR       24.2       24.0       18.5       13.5       0       957       0.3205       843	28	14	20	NEE	27.2	32.3	18.8	16.9	436	958	-0.0946	-258		1316
30         14         49         NEE         24.5         24.0         18.5         13.5         687         958         -0.2098         -552         1395           26         13         58         ER         30.6         48.0         18.0         14.1         0         957         0.3493         952           27         14         13         ER         28.9         34.2         20.0         15.4         0         958         0.4320         1120           28         14         27         ER         25.0         32.3         18.8         16.9         0         958         0.3848         1058           29         14         41         ER         23.3         36.9         17.7         15.2         0         958         0.2419         654           30         14         55         FR         24.2         24.0         18.5         13.5         0         957         0.3205         843	29	14	34	NEE	23.8	36.9	17.7	15.2	442	958	-0.1642	-443		1097
26         13         58         ER         30.6         48.0         18.0         14.1         0         957         0.3493         952           27         14         13         ER         28.9         34.2         20.0         15.4         0         958         0.4320         1120           28         14         27         ER         25.0         32.3         18.8         16.9         0         958         0.3848         1058           29         14         41         ER         23.3         36.9         17.7         15.2         0         958         0.2419         654           30         14         55         FR         24.2         24.0         18.5         13.5         0         957         0.3205         843	30	14	49	NEE	24.5	24.0	18.5	13.5	08/	958	-0.2098	-552	075	1342
27       14       13       EK       28.9       34.2       20.0       15.4       0       958       0.4320       1120         28       14       27       ER       25.0       32.3       18.8       16.9       0       958       0.3848       1058         29       14       41       ER       23.3       36.9       17.7       15.2       0       958       0.2419       654         30       14       55       ER       24.2       24.0       18.5       13.5       0       957       0.3205       843	26	13	58	ER	30.6	48.0	18.0	14.1	0	957	0.3493		952	
26         14         27         EK         25.0         32.3         18.8         16.9         0         958         0.3848         1058           29         14         41         ER         23.3         36.9         17.7         15.2         0         958         0.2419         654           30         14         55         FR         24.2         24.0         18.5         13.5         0         957         0.3205         843	27	14	13	ER	28.9	34.2	20.0	15.4	0	958	0.4320		1120	
27 14 41 EK 23.3 30.7 17.7 15.2 U 958 0.2419 654 30 14 55 FR 24.2 24.0 18.5 13.5 0 957 0.3205 843	28	14	27	EK	20.0	32.3	18.8	10.9	0	958	0.3848		1058	
	30	14	55	FR	23.3	24.0	18.5	13.2	0	957	0.2419		843	

S.Table 13: CO<sub>2</sub>-flux measurements and environmental parameters on 22 and 23 Jul

Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	(	CO <sub>2</sub> flux	
											mg	CO2 m <sup>2</sup>	h⁻¹
	hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
1	13	13	NEE	31.7	48.0	19.9	15.1	838	940	-0.2758	-579		1471
2	13	28	NEE	31.8	25.4	21.6	18.7	1237	940	-0.2969	-570		1610
3	13	43	NEE	31.9	29.3	20.2	16.1	4 4 1	940	-0.1095	-340		1422
4	14	14	NEE	31.0	20.0	19.0	10.7	1207	939	-0.2297	-303		1473 2055
5	14	20	ER	30.9	48.0	19.7	17.7	0	939	-0.4798	-901	892	2055
2	13	35	ER	32.0	25.4	21.6	18.7	0	940	0.5422		1040	
3	13	53	ER	31.9	29.3	20.2	16.1	0	939	0.5292		1077	
4	14	8	ER	31.1	28.8	19.8	16.7	0	939	0.3684		908	
5	14	23	ER	31.0	21.1	19.7	17.7	0	939	0.5567		1104	
6	15	21	NEE	34.5	16.9	24.6	23.4	470	942	-0.0995	-213		1539
7	15	35	NEE	35.8	18.9	21.5	17.5	1123	942	-0.2115	-402		1840
8	15	50	NEE	35.9	14.5	21.8	17.5	1060	942	-0.1407	-292		1117
9	16	4	NEE	33.5	30.4	23.7	15.3	642	942	-0.0918	-202		690
10	16	17	NEE	32.4	18.4	21.7	17.7	454	942	0.0290	73	100/	892
0	15	28	ER	34.7	16.9	24.6	23.4	3 1	942	0.6201		1320	
/	15	42	ER	30.4	18.9	21.0	17.5	1	942	0.7566		1439	
8	15	57	ER	34.4	14.5	21.8	17.5	0	942	0.3962		820	
9	10	25	ER	32.0	10.4	23.7	10.5	0	942	0.2204		407	
10	15	25	NEE	34.9	27.1	23.8	18.9	1033	942	-0.1554	-314	900	1341
12	14	47	NEE	34.9	23.6	22.1	19.3	935	942	-0.2387	-469		1439
13	14	33	NEE	34.7	20.3	26.7	25.1	918	942	-0.0466	-92		1367
14	14	17	NEE	35.9	26.9	24.8	19.2	1211	942	-0.2423	-418		1401
15	14	2	NEE	36.4	13.8	23.1	19.3	1361	942	-0.3328	-828		2207
11	15	8	ER	34.6	27.1	23.8	18.9	0	942	0.5075		1027	
12	14	55	ER	35.3	23.6	22.1	19.3	1	942	0.4950		971	
13	14	40	ER	34.8	20.3	26.7	25.1	0	942	0.6492		1275	
14	14	24	ER	35.6	26.9	24.8	19.2	4	942	0.5694		983	
15	14	10	ER	35.9	13.8	23.1	19.3	2	942	0.5535		1379	
16	17	35	NEE	22.6	11.7	0.4	-0.4	264	942	-0.1869	-439		934
17	17	19	NEE	24.1	18.7	19.4	16.7	282	942	-0.0056	-12		721
18	17	5	NEE	26.0	9.4	21.0	18.9	331	942	-0.0927	-233		1035
19	16	50	NEE	26.9	11.9	22.0	18.0	487	942	-0.1742	-351		1127
20	16	34	NEE	28.9	17.1	20.0	17.7	346	942	-0.2920	-779		1845
16	17	42	ER	22.5	11.7	0.4	-0.4	18	942	0.2105		495	
17	17	28	ER	23.1	18.7	19.4	16.7	18	942	0.3188		709	
18	17	11	ER	24.8	9.4	21.0	18.9	18	942	0.3178		802	
19	16	57	ER	26.6	11.9	22.0	18.0	0	942	0.3846		776	
20	16	43	ER	27.5	17.1	20.0	17.7	0	942	0.3977		1066	
21	12	48	NEE	34.8	18.7	21.5	17.2	629	943	-0.1518	-389		1323
22	13	2	NEE	34.2	21.7	22.7	17.3	1131	942	-0.1358	-348		1446
23	13	16	NEE	34.1	30.4	22.4	20.8	1049	942	-0.2625	-658		2209
24	13	31	NEE	35.5	18.0	23.0	20.0	1201	942	-0.4720	-1123		2661
25	13	46	NEE	35.8	15.7	22.0	18.6	1222	942	-0.0902	-235	005	1256
21	12	55	ER	34.3	18.7	21.5	17.2	0	942	0.3646		935	
22	13	9	ER	33.9	21.7	22.7	17.3	0	942	0.4279		1098	
23	13	24	EK	34.7	30.4	22.4	20.8	0	942	0.6203		1001	
24 25	13	39	ER	30.0	18.0	23.0	20.0	2	942	0.0409		1038	
25	13	32	NEE	31.4	11.9	22.0	18.2	1038	942	-0.0636	-170	1021	1326
27	14	48	NEE	34.0	11.8	21.7	17.3	1200	939	-0.1573	-393		1469
28	15	3	NEE	34.4	10.9	22.9	16.1	1118	939	-0.2191	-572		1651
29	15	18	NEE	33.6	11.7	20.3	17.0	914	939	-0.1811	-464		928
30	15	33	NEE	31.6	14.3	24.9	16.8	995	939	-0.2350	-592		1230
26	14	39	ER	32.3	11.9	23.3	18.2	0	939	0.4350		1157	
27	14	56	ER	34.1	11.8	21.7	17.3	0	939	0.4306		1076	
28	15	11	ER	33.9	10.9	22.9	16.1	0	939	0.4122		1078	
29	15	26	ER	31.2	11.7	20.3	17.0	0	939	0.1798		464	
30	15	40	ER	32.3	14.3	24.9	16.8	0	939	0.2540		638	

S.Table 14: CO<sub>2</sub>-flux measurements and environmental parameters on 28 and 29 Jul

Plot	Measu Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	(	CO <sub>2</sub> flux	
											ma	CO2 m <sup>2</sup>	h⁻¹
	hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
1	14	25	NEE	21.7	75.2	16.2	14.4	716	947	-0.3344	-730		1286
2	14	37	NEE	21.4	37.4	18.7	15.8	1124	947	-0.4784	-958		1567
3 4	14 15	50 3	NEE	21.0	54.0 42.0	17.0	15.0	626	947	-0.4281	-909		2055
5	15	15	NEE	22.4	31.8	17.4	16.9	932	947	-0.5435	-1118		1893
1	14	31	ER	21.2	75.2	16.2	14.4	0	947	0.2538	1110	555	1070
2	14	43	ER	21.1	37.4	18.7	15.8	0	947	0.3038		609	
3	14	57	ER	20.8	54.6	17.0	15.0	0	947	0.3192		680	
4	15	9	ER	21.5	42.0	17.4	15.2	0	947	0.3654		938	
5	15	22 19	NEE	22.8	31.8 29.7	17.7	16.9	720	947 946	-0.2779	-620	//4	1404
7	12	31	NEE	21.5	28.6	15.1	13.5	544	946	-0.2357	-472		1193
8	12	43	NEE	22.4	31.6	17.6	14.5	820	946	-0.2489	-542		1257
9	12	55	NEE	20.3	52.2	15.4	13.0	431	946	-0.1661	-385		872
10	13	7	NEE	20.4	37.3	16.1	11.3	669	946	-0.2815	-742	705	1429
7	12	23	FR	22.5	29.7	17.9	14.1	0	940	0.3508		705	
8	12	49	ER	21.1	31.6	17.6	14.5	0	946	0.3270		715	
9	13	1	ER	20.0	52.2	15.4	13.0	0	946	0.2101		487	
10	13	14	ER	20.9	37.3	16.1	11.3	0	946	0.2615		688	
11	18	35	NEE	15.0	43.0	15.1	14.1	251	948	-0.1146	-249		800
12	18	23	NEE	15.3	39.3	16.6	15.5	228	948	-0.1422	-300		821
13	18	11 E0	NEE	16.0	40.3	1/./	15.3	1//	948	-0.0424	-89		649 700
14	17	59 46	NEE	17.0	25.7	18.3	17.0	306	948	-0.1079	-199		1852
11	18	40	FR	14.7	43.0	15.1	14.1	0	948	0.2532	1220	551	1032
12	18	28	ER	15.0	39.3	16.6	15.5	0	948	0.2465		521	
13	18	17	ER	15.4	40.3	17.7	15.3	0	948	0.2652		559	
14	18	5	ER	16.7	25.7	18.3	17.0	0	948	0.2718		503	
15	17	53	ER	18.7	21.9	16.9	16.2	0	947	0.2356		625	
16	15	29	NEE	23.7	27.0	17.1	14.4	849	947	-0.3661	-861		2010
17	15	41	NEE	23.7	29.5	16.1	14.2	791	947	-0.3263	-728		1499
18	16	1	NEE	24.4	32.1	18.3	14.8	718	947	-0.2861	-727		1685
19	16 16	14	NEE	23.8	44.3	19.4	15.1	618	947	-0.2480	-508		1329
16	10	35	FR	23.1	27.0	17.1	14.4	0	947	0.4881	-2003	1149	3000
17	15	47	FR	23.7	29.5	16.1	14.2	0	947	0.3457		771	
18	16	7	ER	24.1	32.1	18.3	14.8	0	947	0.3769		959	
19	16	20	ER	22.6	44.3	19.4	15.1	0	947	0.3995		821	
20	16	33	ER	23.6	31.0	17.1	13.3	0	947	0.3380		923	
21	14	12	NEE	22.5	32.8	17.5	15.9	326	947	-0.0750	-201		911
22	14	0	NEE	24.5	33.9	18.5	16.2	615	947	-0.2217	-590		1405
23	13	48	NEE	24.0	48.1	19.1	15.7	343	946	-0.3779	-984		2073
24	13	34	NEE	25.0	27.1	19.1	15.9	1133	946	-0.7109	-1/58		2944
25	13	23	ED	22.2	24.9	18.9	14.0	0	940	-0.2894	-793	710	1991
21	14	6	FR	23.7	33.9	17.5	16.2	0	947	0.3056		815	
23	13	54	ER	24.6	48.1	19.1	15.7	0	946	0.4194		1090	
24	13	41	ER	24.5	27.1	19.1	15.9	0	946	0.4789		1186	
25	13	29	ER	23.8	24.9	18.9	14.0	0	946	0.2890		788	
26	17	32	NEE	19.9	26.5	16.9	15.6	394	947	-0.0201	-56		884
27	17	20	NEE	20.4	21.5	19.9	16.1	675	947	-0.2504	-660		1253
28	1/	5	NEE	20.2	24./	18.3	15.4	320	94/	-0.12/4	-352		1143
27 30	10	5∠ 40	NEE	21.0	23.0 21.7	10.9	13.0	528 337	947	-0.2072	-718		1094
26	10	30	FR	10.3	26.5	16.0	15.6	0	947	0.1200	527	828	10/4
27	17	26	ER	20.5	21.5	19.9	16.1	0	947	0.2248		593	
28	17	11	ER	19.2	24.7	18.3	15.4	0	947	0.2855		791	
29	16	58	ER	20.9	23.6	15.9	15.0	0	947	0.2488		670	
30	16	46	ER	22.1	21.7	16.5	13.7	0	947	0.2921		766	

S.Table 15: CO<sub>2</sub>-flux measurements and environmental parameters on 7 Aug.

Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	(	CO <sub>2</sub> flux	
											mg	CO2 m <sup>2</sup>	h⁻¹
	hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
1	16	11	NEE	13.8	45.5	11.7	10.5	429	955	-0.1848	-418		807
2	16	23	NEE	13.4	30.0	11.9	11.7	280	954	-0.1602	-332		748
3	10	35	NEE	12.7	20.8	11.0	10.6	105	955	-0.0527	-110		142
4	16	48	NEE	13.3	19.6	11.8	12.2	470	955	-0.2320	-617		1054
5	1/	17	FR	14.9	21.3 45.5	12.1	12.4	410	954	-0.4338	-923	389	1381
2	16	29	FR	13.3	30.0	11.9	11.7	0	955	0.2001		415	
3	16	42	ER	12.3	20.8	11.6	10.6	0	955	0.2828		625	
4	16	54	ER	13.3	19.6	11.8	12.2	0	955	0.1641		436	
5	17	7	ER	16.3	21.3	12.1	12.4	0	954	0.2167		459	
6	17	14	NEE	17.1	20.7	12.7	13.1	206	954	-0.2124	-488		1039
7	17	26	NEE	19.3	17.2	11.7	11.3	318	954	-0.2724	-554		983
8	17	38	NEE	20.0	16.8	12.7	12.7	306	954	-0.2160	-478		997
9	17	50	NEE	18.3	29.9	11.2	10.6	477	954	-0.1500	-353		571
10	18	9	NEE	18.3	21.1	11.1	11.8	637	955	-0.2230	-597		
6	1/	20	ER	18.1	20.7	12.7	13.1	0	954	0.2402		550	
/	17	32	ER	19.2	17.2	11.7	11.3	0	954	0.2112		429	
8	1/	44	ER	18.4	16.8	12.7	12.7	0	954	0.2333		519	
9	17	50	ER	18.3	29.9	11.2	10.6	0	955	0.0929		218	
10	- 11	- 51	ER NFF	14.0	21.1	9.3	11.8	338	- 954	-0 2475	-544	-	- 774
12	12	3	NFF	13.3	20.9	10.3	11.0	423	954	-0.0495	-106		599
13	12	15	NEE	13.3	17.6	12.7	12.8	407	954	-0.2397	-513		1007
14	12	27	NFF	13.4	25.3	11.1	9.9	381	954	-0.3035	-572		858
15	12	39	NEE	12.7	16.3	9.2	10.4	407	954	-0.5879	-1603		2128
11	11	57	FR	13.6	30.7	9.3	10.3	0	954	0.1049		231	-
12	12	9	FR	13.4	20.9	10.3	11.0	0	954	0.2306		493	
13	12	21	FR	13.5	17.6	12.7	12.8	0	954	0.2315		495	
14	12	33	FR	13.0	25.3	11.1	9.9	0	954	0.1515		286	
15	12	52	ER	12.5	16.3	9.2	10.4	0	954	0.1921		524	
16	12	59	NFF	13.8	17.8	9.7	9.8	989	954	-0.5015	-1229		1662
17	13	11	NFF	14.6	19.2	9.6	10.3	1166	954	-0.4404	-1021		1499
18	13	25	NEE	18.2	17.7	10.5	10.8	1087	954	-0.3675	-960		1608
19	13	37	NEE	19.3	27.4	12.1	9.9	967	954	-0.3796	-795		1219
20	13	50	NEE	16.0	14.7	12.3	11.8	292	954	-0.3294	-930		1728
16	13	5	ER	13.5	17.8	9.7	9.8	0	954	0.1765		433	
17	13	17	ER	15.5	19.2	9.6	10.3	0	954	0.2068		478	
18	13	31	ER	18.5	17.7	10.5	10.8	0	954	0.2480		648	
19	13	43	ER	17.5	27.4	12.1	9.9	0	954	0.2013		424	
20	13	57	ER	15.5	14.7	12.3	11.8	0	954	0.2822		798	
21	15	58	NEE	13.4	28.6	11.3	11.6	273	955	-0.0953	-266		777
22	15	46	NEE	14.2	21.5	13.0	13.0	318	955	-0.0172	-48		588
23	15	32	NEE	13.7	28.1	13.7	14.1	347	955	-0.2271	-618		1326
24	15	19	NEE	13.8	18.4	12.6	13.3	521	955	-0.4444	-1152		1982
25	15	7	NEE	14.2	27.3	13.3	12.7	320	955	-0.1118	-318		817
21	16	4	ER	13.3	28.6	11.3	11.6	0	955	0.1832		511	
22	15	52	ER	13.7	21.5	13.0	13.0	0	955	0.1940		540	
23	15	38	ER	14.1	28.1	13.7	14.1	0	955	0.2605		708	
24	15	25	ER	13.8	18.4	12.6	13.3	0	955	0.3200		830	
25	15	13	ER	13.5	27.3	13.3	12.7	0	955	0.1752		499	
26	14	54	NEE	15.7	18.7	11.9	11.0	222	954	-0.0069	-20		505
27	14	42	NEE	17.2	19.3	13.2	12.5	709	954	-0.2232	-599		1345
28	14	30	NEE	16.6	23.3	10.5	11.4	1241	954	-0.3880	-1093		1780
29	14	18	NEE	13.0	22.9	11.1	10.6	545	954	-0.2472	-690		1190
30	14	6	NEE	13.8	21.6	10.8	11.0	336	954	-0.1846	-502		900
26	15	0	ER	15.0	18.7	11.9	11.0	0	954	0.1695		486	
27	14	48	ER	16.8	19.3	13.2	12.5	0	954	0.2773		/46	
28	14	36	ER	17.7	23.3	10.5	11.4	0	954	0.2449		687	
29	14	24	EK	14.5	22.9	10.9	10.6	0	954	0.1802		200	
30	14	13	EK	13.1	21.0	10.8	11.0	0	904	0.1402		240	

S.Table 16: CO<sub>2</sub>-flux measurements and environmental parameters on 15 Aug

NEW         Min         NEY         CR         'C         'C         'P         P         No         P         NO	Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	C	CO <sub>2</sub> flux	
hour         min         NEE / ER         "C         vol %         *C         r C         r Model probability         mbar         ppm s <sup>-1</sup> NEE         PR         0Ps           1         18         27         NEE         P3         223         0.0         2.8         0.00         0.000												mg (	CO2 m <sup>2</sup>	h⁻¹
1         16         29         NRE         9.7         27.0         8.5         7.8         138         449         4.0127         7.4         4.5           2         16         14         NRE         113         2.27         8.5         8.8         2.11         4.4         4.0177         7.13         4.5           3         16         49         113         2.27         8.5         8.8         2.11         4.4         4.0177         7.13         7.13         7.13         7.13         7.14         7.14         4.0120         7.21         7.13         7.14         7.14         7.14         7.14         7.14         7.15		hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
2         16         16         16         16         90         9.2         164         90         0.177         315         145           4         15         43         MEE         112.3         21.5         8.8         33         570         909         0.0177         312         718           5         15         43         MEE         112.3         21.5         8.8         33         570         909         0.0177         317         73           16         42         48         199         247         8.4         0         949         0.177         377           5         15         51         54         64         173         21.1         15.5         8.4         0         949         0.180         -432         104.4           6         15         74         MEE         173         21.1         12.2         10.9         20.1         0.127.4         3.5         9.1         0.163         0.170         9.1         0.127.4         3.6         10.6         10.1         10.1         10.1         10.1         10.1         10.1         10.1         10.1         10.1         10.1         10.1         10	1	16	29	NEE	9.7	27.0	8.0	7.8	136	949	-0.0182	-42		285
3         15         59         NEE         11.5         2.27         8.5         8.0         2.11         94.9         0.0.712         7.72         185           5         15         2.8         NEE         17.2         3.25         9.5         8.4         205         94.9         0.0.712         7.72         1.65           1         95         6.5         18         199         2.20         9.5         8.4         205         9.49         0.0.329         2.275           5         15         2.5         178         1.4         0         9.49         0.0.329         2.27           6         15         19         NEE         10.1         2.23         1.5         1.4         0         9.49         0.0.196         4.32         1.044           7         15         35         NEE         10.1         2.21         1.15         1.19         0         9.55         9.51         0.0.176         4.470         1.942           10         16         7         NEE         10.3         1.22         10.9         9.51         0.0.176         4.432         1.942           10         16         7         NEE	2	16	14	NEE	10.5	24.0	9.0	8.2	164	949	-0.0839	-175		445
4         15         43         Not         17.3         27.5         8.8         8.3         5.00         949         0.0.47         5.75         9           5         15         23         18         17.2         20         20.5         8.4         20.5         9.4         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         949         0.0         0.0         949         0.0         0.0         949         0.0         0.0         949         0.0         0.0         949         0.0         0.0         949         0.0         0.0         949         0.0         0.0         949         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0	3	15	59	NEE	11.5	22.7	8.5	8.0	2/1	949	-0.1///	-392		/18
5         8         43         10         12         12         16         20         948         20         948         20         948         20         948         20         20         20           3         15         6         6         17         19         22         10         10         20         20           4         15         5         6         16         17         18         0         949         0.1320         20           5         5         5         5         5         6         17         15         19         RE         123         22.1         122         10.9         700         941         0.167         349         868           9         16         7         NEE         18.3         22.0         11.0         8.9         555         951         0.176         470         948         868           9         16         7         NEE         18.4         22.7         10.3         97         77         951         0.1723         463         450           9         16         15         GR         18.6         27.1         15.3         97	4	15	43	NEE	12.3	21.5	8.8	8.3	570	949	-0.4782	-1269		1636
2         16         28         99         240         90         82         0         949         13789         220           4         15         51         58         19         19         27.5         86         8.3         0         949         1319         207           5         15         54         48         119         27.5         86         8.4         0         949         0.1319         207           6         15         59         8.4         0         949         0.1319         402         10           7         15         55         NRE         19.3         20.1         12.4         10.6         617         910         0.731         0.1604         -399         848           9         16         7         NRE         18.5         297         10.3         97         971         0.1729         473         473           6         15         53         E8         18.4         22.9         10.8         9         0         951         0.1343         333           10         6         15         E8         18.4         32.9         10.3         8.9         0.	5	15	28	FR	9.2	32.5	9.5	8.4	295	949	-0.2697	-5/5	243	977
3         16         6         18         19         2.7         8.5         8.0         0         949         0.1130         327           5         15         54         10         113         119         210         25         95         8.4         0         949         0.1130         347           6         15         35         NE         19         NE         19.1         22.1         12.2         10.9         700         951         -0.1270         -5.2         1044           8         15         NIE         19.1         22.1         12.4         16.6         417         0.161         0.169         -3.3         951         0.1010         -3.4         0.444           9         16         7         NIE         118         22.9         110         89         951         0.1010         -2.21         443           6         15         22         RE         18.6         27.1         17.3         19         0         951         0.1133         -3.3         -3.3           7         15         23         RE         18.4         29.0         10         13.2         13.3         13.0	2	16	22	FR	9.9	24.0	9.0	8.2	0	949	0.1290		270	
4         15         51         ER         119         21.5         8.8         8.3         0         949         0.1380         307           6         15         19         NLE         10.2         27.1         15.3         11.9         210         951         0.1380         402         16.4           7         15         55         NLE         19.3         20.1         12.4         16.6         617         951         0.167         349         448           9         6         7         NLE         118.3         27.9         951         0.167         349         449           6         15         27         NE         116.4         27.1         113.3         11.9         0         951         0.176         443           6         15         27         NE         116.4         27.1         113.3         11.9         0         951         0.176         443           10         16         15         58         16.0         20.1         12.4         10.6         0         951         0.138         90.0         461         14.4           11         12         11.0         13.1	3	16	6	ER	10.9	22.7	8.5	8.0	0	949	0.1479		327	
5         15         36         16         17         15         15         17         17         17         17         18         17         17         17         18         17         17         17         18         17         17         17         18         17         17         17         17         18         17         17         17         17         17         17         17         18         17         17         17         18         17         17         18         17         17         18         17         17         18         17         17         18         17         18         17         19         0         95         0         17         18         17         19         0         95         0         17         14	4	15	51	ER	11.9	21.5	8.8	8.3	0	949	0.1380		367	
6       15       19       NEE       182       27.1       15.3       11.9       210       951       0.1895       4.32       1064         8       15       51       NFE       19.3       20.1       17.4       10.0       617       951       0.207       552       1044         8       15       51       NFE       19.3       20.1       17.4       10.0       617       951       0.2167       3.49       484         6       15       23       NEE       18.6       22.7       10.3       9.7       577       951       0.1765       43.3       27         7       15       43       FR       19.0       22.8       10.0       6.0       951       0.74.4       40.0         9       16       15       FR       18.4       22.9       10.0       8.9       0.0       951       0.143.3       33.3       10.1       10.4       4.0       4.0       4.0       4.0       4.0       4.0       4.0       4.0       4.0       4.0       4.0       4.0       4.0       4.0       10.0       10.0       10.0       10.0       10.0       10.0       4.0       10.0       10.0	5	15	36	ER	12.1	32.5	9.5	8.4	0	949	0.1882		402	
7       15       35       NEE       19.1       28.1       12.2       10.9       700       951       0.2770       5.62       1044         9       16       7       NEE       18.8       29.9       11.0       8.9       655       951       0.1201       2.81       0.54         6       15       27       EK       18.6       22.7       13.3       17.9       0       951       0.2775       463         7       15       59       ER       18.6       20.1       12.4       10.6       0       951       0.2775       483         9       16       15       ER       18.4       20.1       12.4       10.6       0       951       0.2144       480         10       16       31       ER       18.4       20.1       11.0       80       0       951       0.1346       504       10.1         11       12       41       NEE       17.5       21.9       10.9       9.4       401       952       0.3376       644       10.1         13       12       NEE       17.1       21.3       11.4       9.4       0       962       0.3269       0.464<	6	15	19	NEE	18.2	27.1	15.3	11.9	210	951	-0.1895	-432		1065
8         15         51         NEE         19.3         20.1         12.4         10.6         477         941         0.1667         3.69         648           10         7         NEE         185         29.7         170         951         0.1765         4.70         971           6         15         27         ER         186         22.1         153         11.9         0         951         0.275         4.83         14.9           6         15         27         ER         186         22.1         15.3         0.0         951         0.1423         3.33         1.3           10         16         15         ER         184         22.9         10.3         67         0         951         0.1423         3.33         1.12           11         12         27         NEE         117.3         21.3         11.4         98         42.6         952         -0.3046         -6.41         1.12           12         13         28         NEE         17.7         21.3         11.4         0.8         0         952         -0.3046         -6.41         1.13           13         28         ER </td <td>7</td> <td>15</td> <td>35</td> <td>NEE</td> <td>19.1</td> <td>28.1</td> <td>12.2</td> <td>10.9</td> <td>700</td> <td>951</td> <td>-0.2770</td> <td>-562</td> <td></td> <td>1044</td>	7	15	35	NEE	19.1	28.1	12.2	10.9	700	951	-0.2770	-562		1044
9         16         7         NEE         18.8         32.9         11.0         8.9         6355         691         0.1201         2.81         615           10         16         23         NRE         18.6         27.1         15.3         11.9         0         951         0.0275         470         974           6         15         ER         18.6         27.1         15.3         11.9         0         951         0.0239         483           7         15         ER         18.4         20.0         11.0         8.9         0         951         0.0239         483           9         16         15         ER         18.4         22.9         10.0         89.0         952         0.3061         601         1064           12         2         0.7         NRE         17.5         21.9         10.9         9.4         601         952         0.306         601         1064         101           13         13         28         NEE         17.1         21.3         11.4         9.8         0         952         0.346         564         101           14         13         3.7	8	15	51	NEE	19.3	20.1	12.4	10.6	617	951	-0.1667	-369		848
10       16       27       ER       18.5       29.7       10.3 $9.7$ $9.57$ $9.91$ $0.277$ $4.70$ $974$ $473$ $874$ $632$ 7       15       43       ER       140       28.1       11.2       10.9       0       991 $0.2279$ $483$ 8       15       59       ER       18.4       22.9       11.0       8.0       991 $0.1423$ 333         10       16       15       ER       18.4       22.9       10.0       8.9       0       951 $0.1423$ 333         11       12       17       NEE       17.5       21.9       10.9 $4.401$ 952 $4.3076$ $4.611$ 11.1         13       13       12       NEE       17.4       21.3       11.2       10.3       707       952 $4.629$ $-1.687$ $4.76$ 12.3         14       13       28       RF       17.3       21.9       10.9       922 $0.2241$ $4.76$ 22.8         11       12       49       RF       17.4       21.3       11.2       10.3	9	16	7	NEE	18.8	32.9	11.0	8.9	535	951	-0.1201	-281		615
B         13         27         15         43         17         103         0         91         0.22/15         80.2           8         15         59         FR         186         20.1         12.4         10.9         0         951         0.2144         480           9         16         15         FR         18.4         22.9         11.0         89         0         951         0.1286         594           10         16         31         FR         18.1         27.1         13.4         98         62.6         952         -0.305.6         -447         1122           11         12         41         NEE         17.2         20.4         13.6         12.2         49.2         -6.279         -4.43         1017           13         13         28         NEE         17.2         20.4         13.6         12.2         40.4275         -16.67         22.8           13         13         20         FR         17.4         21.3         11.4         14         99         20.226.1         477           14         13         37         FR         16.8         20.4         13.5         12.8<	10	16	23	NEE	18.5	29.7	10.3	9.7	577	951	-0.1765	-470	(22	974
I         ID         ID         L20         L20         L20         P         ID         ID         P         ID         ID         ID         ID<	0	15	27	ER	18.0	27.1	10.3	10.0	0	951	0.2775		032	
a         b	0	15	43 50	ED	19.0	20.1	12.2	10.9	0	951	0.2379		403	
10         11         11         11         12         11         12         14         14         93         62         631         0.1886         594           11         12         41         NEE         181         27.3         11.4         98         628         92         -0.3076         -641         1064           12         12         77         NEE         175         219         109         4.4         610         652         -0.3076         -641         1013           13         12         NEE         172         204         136         77         922         -0.269         -0.897         2286           11         12         49         ER         17.4         213         114         98         0         962         0.1860         403         128           12         13         5         ER         17.3         219         100         942         0.962         0.2261         416         146         146         147         133         112         103         0         952         0.2285         569         907           17         12         56         NEE         82         2	9	16	15	FR	18.0	32.9	12.4	8.9	0	951	0.2104		333	
11         12         41         NEE         181         213         114         98         626         952         4.3001         4.61         57         1044           12         12         57         NEE         175         219         109         94         601         952         4.3006         -647         1123           13         13         12         NEE         172         204         136         120         542         952         -0.306         -647         1123           15         13         45         NEE         171         213         112         103         97         952         -0.6295         -1667         2286           11         12         49         ER         174         213         114         98         0         952         0.2249         -476         147           13         33         20         ER         172         213         112         03         0         952         0.2249         -474         476         147           14         13         37         ER         168         204         136         120         0         952         0.2249         -	10	16	31	FR	18.1	29.7	10.3	9.7	0	951	0.1886		504	
12       12       57       NEE       175       219       109       94       601       952       0.0576       6-47       1123         13       12       NEE       169       191       152       128       497       952       0.0579       6-543       10171         15       13       45       NEE       17.1       21.3       11.4       98       0       952       0.2579       6.4265       2286         11       12       49       RE       17.4       21.3       11.4       98       0       952       0.2240       476       2286         13       13       20       FR       16.69       191       152       12.8       0       952       0.2240       474         14       13       37       FR       16.8       20.4       13.6       12.0       952       0.2240       53       760         15       13       22       FR       17.2       21.3       11.2       10.3       0       952       0.2240       53.3       760         16       12       41       NEE       8.8       31.2       6.5       6.4       0       948       0.0228 <td>11</td> <td>12</td> <td>41</td> <td>NEE</td> <td>18.1</td> <td>21.3</td> <td>11.4</td> <td>9.8</td> <td>626</td> <td>952</td> <td>-0.3061</td> <td>-661</td> <td>504</td> <td>1064</td>	11	12	41	NEE	18.1	21.3	11.4	9.8	626	952	-0.3061	-661	504	1064
13       13       12       NEE       169       191       152       128       497       992       0.2579       6.584       1013         14       13       28       NEE       17.2       20.4       13.6       120       542       992       0.3146       584       1013         11       12       449       RE       17.1       21.3       11.4       98       0       992       0.2261       476         13       13       20       ER       17.3       21.9       10.9       9.4       0       992       0.2261       476         14       13       37       ER       16.8       20.4       13.6       12.0       0       992       0.2261       476         15       13       52       ER       17.2       13       11.2       10.3       0       992       0.2281       566       907         16       12       41       NEE       8.2       27.6       6.5       6.4       351       948       0.2282       -533       780         17       13       2.8       NEE       8.8       38.1       6.7       6.4       20       948       0.2288	12	12	57	NEE	17.5	21.9	10.9	9.4	601	952	-0.3076	-647		1123
14       13       28       NEE       17.2       20.4       13.6       12.0       54.2       95.2       -0.0346       -584       1013         15       13       45       NEE       17.1       21.3       11.2       10.3       707       952       -0.6295       -1687       2286         12       13       5       ER       17.4       21.3       11.4       9.8       0       952       0.2261       4476         14       13       37       ER       16.8       20.4       13.6       12.0       0       952       0.2205       599         15       13       52       ER       17.2       21.3       11.2       10.3       0       952       0.2205       590         16       12       41       NEE       8.5       26.2       6.9       6.3       329       948       -0.2262       -533       780         19       13       28       NEE       8.8       31.2       6.5       6.4       290       948       -0.228       -6.9       6.3       950         19       13       28       NEE       8.8       28.2       6.5       6.4       0	13	13	12	NEE	16.9	19.1	15.2	12.8	497	952	-0.2579	-543		1017
15         13         45         NE         17.1         21.3         11.2         10.3         707         952         -0.6295         -1.687         2286           11         12         13         5         ER         17.3         21.9         10.9         94.0         952         0.2241         476           13         13         20         ER         16.9         11.1         15.2         12.8         0.         952         0.2241         474           15         13         52         ER         17.2         21.3         11.2         10.3         0.         952         0.2235         569           16         12         4.1         NEE         8.2         2.6         6.5         6.4         351         948         0.2228         .423         960           17         12         56         NEE         8.8         31.2         6.5         6.4         329         948         0.2228         .494         818           20         13         43         NEE         8.8         31.2         6.5         6.4         0.948         0.1373         341           17         13         44         ER </td <td>14</td> <td>13</td> <td>28</td> <td>NEE</td> <td>17.2</td> <td>20.4</td> <td>13.6</td> <td>12.0</td> <td>542</td> <td>952</td> <td>-0.3146</td> <td>-584</td> <td></td> <td>1013</td>	14	13	28	NEE	17.2	20.4	13.6	12.0	542	952	-0.3146	-584		1013
	15	13	45	NEE	17.1	21.3	11.2	10.3	707	952	-0.6295	-1687		2286
12       13       5       ER       17.3       21.9       10.9       9.4       0       952       0.2261       476         13       13       20       ER       16.9       19.1       15.2       12.8       0       952       0.2249       474         14       13       37       ER       16.8       20.4       15.6       6.4       952       0.2230       429         15       13       52       ER       17.2       21.3       11.2       10.3       0       952       0.2235       599         16       12       44       NEE       8.2       27.6       6.5       6.4       351       948       -0.2278       -566       907         17       12       56       NEE       8.8       31.2       6.5       6.5       329       948       -0.228       -494       818         20       13       43       NEE       8.8       31.2       6.5       6.4       0       948       0.1373       341         17       13       4       ER       8.2       27.6       6.5       6.5       0       948       0.1373       343       341       155	11	12	49	ER	17.4	21.3	11.4	9.8	0	952	0.1860		403	
13         20         ER         16.9         19.1         15.2         12.8         0         952         0.2249         474           14         13         37         ER         16.8         20.4         13.6         12.0         0         952         0.2230         429           16         12         41         ME         8.2         27.6         6.5         6.4         331         948         -0.2230         566         907           17         12         56         NEE         8.5         26.2         6.9         6.3         329         948         -0.2230         623         950           18         13         12         NEE         8.8         38.1         6.7         6.4         290         948         -0.2320         623         950           19         13         28         NEE         8.8         38.1         6.7         6.4         0         948         -0.1025         .1159         1555           16         12         49         ER         8.6         26.2         6.9         6.3         0         949         0.1373         341           17         13         4	12	13	5	ER	17.3	21.9	10.9	9.4	0	952	0.2261		476	
14         13         37         ER         16.8         20.4         13.6         12.0         0         952         0.2210         429           15         13         52         ER         17.2         21.3         11.2         10.3         0         952         0.2235         599           16         12         41         NEE         8.2         27.6         6.5         6.4         31         948         -0.2278         -566         907           17         12         56         NEE         8.5         26.2         6.9         6.3         329         948         -0.2202         -533         780           19         13         28         NEE         8.8         31.2         6.5         6.5         0         948         -0.2288         .444         818           20         13         43         NEE         8.8         27.6         6.5         6.4         0         948         0.1050         247           18         13         20         ER         8.8         31.2         6.5         6.5         0         948         0.1221         328           17         13         36 <t< td=""><td>13</td><td>13</td><td>20</td><td>ER</td><td>16.9</td><td>19.1</td><td>15.2</td><td>12.8</td><td>0</td><td>952</td><td>0.2249</td><td></td><td>474</td><td></td></t<>	13	13	20	ER	16.9	19.1	15.2	12.8	0	952	0.2249		474	
151352ER17.221.311.210.309520.2235599161241NEE8.227.66.56.4351948 $-0.2278$ $-566$ 907171256NEE8.831.26.56.5302948 $-0.2228$ $-533$ 790181312NEE8.831.26.56.5302948 $-0.2280$ $-623$ 950191328NEE8.838.16.76.4290948 $-0.2288$ $-494$ 818201343NEE8.828.86.96.8283949 $-0.4025$ $-1159$ 1555161249ER8.227.66.56.50948 $0.1021$ 328191336ER8.738.16.76.40949 $0.1377$ 3962115ER9.028.86.96.80949 $0.1377$ 3962115ER9.028.86.96.80949 $0.1377$ 3962115ER9.022.811.5749951 $-0.1414$ $-384$ 843221447NEE19.222.013.611.5749951 $-0.3124$ 4491630241416NEE19.221.14.312.559595	14	13	37	ER	16.8	20.4	13.6	12.0	0	952	0.2310		429	
16         12         41         NEE         8.2         27.6         6.5         6.4         351         948         -0.2278         -5.66         907           17         12         56         NEE         8.5         26.2         6.9         6.3         329         948         -0.2262         -533         780           18         13         12         NEE         8.8         38.1         6.7         6.4         290         948         -0.2288         -494         818           20         13         43         NEE         8.8         28.8         6.9         6.4         0         948         0.1033         341           17         13         4         ER         8.6         26.2         6.9         6.3         0         948         0.1050         247           18         13         20         ER         8.8         31.2         6.5         6.5         0         948         0.1050         2325           20         13         51         ER         9.0         28.8         6.9         6.8         0         949         0.1377         396           21         15         2         N	15	13	52	ER	17.2	21.3	11.2	10.3	0	952	0.2235		599	
17       12       56       NEE       8.5       26.2       6.9       6.3       329       948       -0.2262       -5.33       780         18       13       12       NEE       8.8       31.2       6.5       6.5       302       948       -0.2288       .494       818         20       13       43       NEE       8.8       28.8       6.9       6.8       283       949       -0.4025       -1159       1555         16       12       49       ER       8.2       27.6       6.5       6.4       0       948       0.0250       -1159       1555         16       12       49       ER       8.2       27.6       6.5       6.5       0       948       0.1050       247         18       13       20       ER       8.8       31.2       6.5       6.5       0       949       0.1373       328         19       13       36       ER       8.7       38.1       6.7       6.4       0       949       0.1377       328       261         21       15       2       NEE       19.2       20.8       13.6       10.4       766       951	16	12	41	NEE	8.2	27.6	6.5	6.4	351	948	-0.2278	-566		907
18       13       12       NEE       8.8       31.2       6.5       6.5       30.2       94.8       -0.23.0       -6.23       950         19       13       28       NEE       8.8       38.1       6.7       6.4       290       94.8       -0.228.8       -494       818         20       13       43       NEE       8.8       28.8       6.9       6.8       283       949       -0.4025       .1159       1555         16       12       49       ER       8.2       27.6       6.5       6.4       0       94.8       0.1050       247         18       13       20       ER       8.8       31.2       6.5       6.5       0       94.8       0.1050       247         18       13       20       ER       8.7       38.1       6.7       6.4       0       949       0.1377       396         20       13       51       ER       8.7       38.1       6.7       6.4       0       949       0.1377       396       1261         21       15       2       NEE       19.3       20.8       11.6       11.5       749       91       0.13167 <td>17</td> <td>12</td> <td>56</td> <td>NEE</td> <td>8.5</td> <td>26.2</td> <td>6.9</td> <td>6.3</td> <td>329</td> <td>948</td> <td>-0.2262</td> <td>-533</td> <td></td> <td>780</td>	17	12	56	NEE	8.5	26.2	6.9	6.3	329	948	-0.2262	-533		780
19       13       28       NRE       8.8       38.1       6.7       6.4       290       948       -0.2288       .494       818         20       13       43       NEE       8.8       28.8       6.9       6.8       283       949       -0.4025       .1159       1555         16       12       49       ER       8.2       27.6       6.5       6.4       0       948       0.0150       247         18       13       20       ER       8.8       31.2       6.5       6.5       0       948       0.1221       328         19       13       36       ER       8.7       381       6.7       6.4       0       949       0.1377       326         20       13       51       ER       9.0       28.8       6.9       6.8       0       949       0.1377       396         21       15       2       NEE       19.3       20.8       13.6       10.4       706       951       -0.1414       -384       843         22       14       47       NEE       19.2       20.0       13.6       11.5       749       951       -0.5231       -1328	18	13	12	NEE	8.8	31.2	6.5	6.5	302	948	-0.2320	-623		950
20       13       43       NEE       8.8       28.8       6.9       6.8       283       949       -0.4025       -1199       1555         16       12       49       ER       8.2       27.6       6.5       6.4       0       948       0.1373       341         17       13       4       ER       8.6       26.2       6.9       6.3       0       948       0.1221       328         19       13       36       ER       8.7       38.1       6.7       6.4       0       949       0.1377       396         20       13       51       ER       9.0       28.8       6.9       6.4       0       949       0.1377       396         21       15       2       NEE       19.2       20.0       13.6       10.4       706       951       -0.1414       -384       843         22       14       47       NEE       19.2       22.0       13.6       11.5       749       951       -0.2309       -628       1261         23       14       31       NEE       18.2       23.8       11.9       11.3       453       951       -0.531       -1328 <td>19</td> <td>13</td> <td>28</td> <td>NEE</td> <td>8.8</td> <td>38.1</td> <td>6.7</td> <td>6.4</td> <td>290</td> <td>948</td> <td>-0.2288</td> <td>-494</td> <td></td> <td>818</td>	19	13	28	NEE	8.8	38.1	6.7	6.4	290	948	-0.2288	-494		818
16         12         49         ER         8.2         27.6         6.5         6.4         0         948         0.1373         341           17         13         4         ER         8.6         26.2         6.9         6.3         0         948         0.1373         341           17         13         4         ER         8.8         31.2         6.5         6.5         0         948         0.1221         328           19         13         36         ER         8.7         38.1         6.7         6.4         0         949         0.1502         325           20         13         51         ER         9.0         28.8         6.9         6.8         0         949         0.1377         396           21         15         2         NEE         19.2         22.0         13.6         11.5         749         951         -0.2309         -6.28         1261           23         14         31         NEE         18.2         22.3         12.5         595         951         -0.5231         -1328         2052           25         13         59         NEE         18.2	20	13	43	NEE	8.8	28.8	6.9	6.8	283	949	-0.4025	-1159	0.44	1555
17       13       4       ER       8.6       26.2       6.9       6.3       0       948       0.1050       247         18       13       20       ER       8.8       31.2       6.5       6.5       0       948       0.1050       247         20       13       51       ER       8.7       38.1       6.7       6.4       0       949       0.1502       325         20       13       51       ER       9.0       28.8       6.9       6.8       0       949       0.1377       396         21       15       2       NEE       19.2       22.0       13.6       10.4       706       951       -0.1414       -384       843         22       14       47       NEE       19.2       22.0       13.6       11.5       749       951       -0.2309       -628       1261         23       14       31       NEE       18.2       23.3       12.9       11.2       893       952       -0.1916       -535       1024         24       14       54       ER       19.2       22.0       13.6       11.5       0       951       0.2325       633	16	12	49	ER	8.2	27.6	6.5	6.4	0	948	0.1373		341	
181320ER8.831.26.56.509480.1221328191336ER8.738.16.76.409490.1502325201351ER9.028.86.96.809490.137739621152NEE19.320.813.610.4706951-0.1414-384843221447NEE19.222.013.611.5749951-0.2309-6281261231431NEE18.223.811.911.3453951-0.3182-8491630241416NEE19.021.214.312.5595951-0.5231-13282052251359NEE18.222.013.611.509510.1678458221454ER19.222.013.611.509510.2325633231439ER18.923.811.911.309510.2325633241423ER18.923.811.911.309510.2325633241423ER18.923.811.911.309510.2325633251512NEE10.822.59.28.5417949 <td< td=""><td>17</td><td>13</td><td>4</td><td>ER</td><td>8.6</td><td>26.2</td><td>6.9</td><td>6.3</td><td>0</td><td>948</td><td>0.1050</td><td></td><td>247</td><td></td></td<>	17	13	4	ER	8.6	26.2	6.9	6.3	0	948	0.1050		247	
1336ER6.738.16.76.409490.1302323201351ER9.028.86.96.809490.130739621152NEE19.320.813.610.4706951-0.1414-384843221447NEE19.222.013.611.5749951-0.2309-6281261231431NEE18.223.811.911.3453951-0.3182-8491630241416NEE19.021.214.312.5595951-0.5231-13282052251359NEE18.222.312.911.2893952-0.1916-5351024211510ER18.320.813.610.409510.1678458221454ER19.222.013.611.509510.2325633231439ER18.923.811.911.309510.2933781241423ER18.221.214.312.599510.293378124148ER19.022.312.911.2189510.1754489251512NEE10.827.97.26.648994	18	13	20	ER	8.8	31.2	0.0	0.0	0	948	0.1221		328	
21       15       2       NEE       19.3       20.8       13.6       10.4       706       951       -0.1414       -384       843         21       15       2       NEE       19.3       20.8       13.6       10.4       706       951       -0.1414       -384       843         22       14       47       NEE       19.2       20.0       13.6       11.5       749       951       -0.2309       -628       1261         23       14       31       NEE       18.2       23.8       11.9       11.3       453       951       -0.3182       -849       1630         24       14       16       NEE       19.0       21.2       14.3       12.5       595       951       -0.5231       -1328       2052         25       13       59       NEE       18.2       22.0       13.6       11.5       0       951       0.1678       458         21       15       10       ER       18.2       21.2       14.3       12.5       9       951       0.2325       633       781         24       14       23       ER       18.2       21.2       14.3       12.5<	20	13	50	ED	0.7	30.1 20.0	6.0	6.9	0	949	0.1302		206	
115216.117.520.516.516.57499510.141415.6416.5416.54221447NEE19.222.013.611.57499510.2329-6281261231431NEE18.223.811.911.3453951-0.5231-13282052241416NEE19.021.214.312.5595951-0.5231-13282052251359NEE18.222.312.911.2893952-0.1916-5351024211510ER18.320.813.610.409510.1678458221454ER19.222.013.611.509510.2325633231439ER18.923.811.911.309510.2844724241423ER18.221.214.312.599510.284472425148ER19.022.312.911.2189510.1754489261512NEE10.822.59.28.5417949-0.1623-469926271444NEE10.624.98.17.2277949-0.1623-4699262714429NEE	20	15	2	NEE	10.3	20.0	13.6	10.4	706	951	-0.1414	-384	370	8/3
1.1 $1.12$ $1.12$ $1.12$ $1.13$	2 I 22	14	2 47	NFF	19.5	20.0	13.0	11.5	749	951	-0 2309	-628		1261
241416NEE19021214.312.5595951-0.5231-1328100251359NEE18.222.312.911.2893952-0.1916-5351024211510ER18.222.013.610.409510.1678458221454ER19.222.013.611.509510.2325633231439ER18.221.214.312.599510.2844724241423ER18.221.214.312.599510.2844724241423ER18.221.214.312.599510.284472425148ER19.022.312.911.2189510.1754489261512NEE10.822.59.28.5417949-0.1623-469926271444NEE10.624.98.17.2277949-0.0362-8771188291414NEE9.827.87.16.7326949-0.2669-580890301359NEE9.129.77.57.0291949-0.1892-522889261519ER10.727.97.26.6 <td>23</td> <td>14</td> <td>31</td> <td>NFF</td> <td>18.2</td> <td>23.8</td> <td>11.9</td> <td>11.3</td> <td>453</td> <td>951</td> <td>-0.3182</td> <td>-849</td> <td></td> <td>1630</td>	23	14	31	NFF	18.2	23.8	11.9	11.3	453	951	-0.3182	-849		1630
25         13         59         NEE         18.2         22.3         12.9         11.2         893         952         -0.1916         -535         1024           21         15         10         ER         18.3         20.8         13.6         10.4         0         951         0.1678         458           22         14         54         ER         19.2         22.0         13.6         11.5         0         951         0.2325         633           23         14         39         ER         18.9         23.8         11.9         11.3         0         951         0.2325         633           24         14         23         ER         18.2         21.2         14.3         12.5         9         951         0.2844         724           25         14         8         ER         19.0         22.3         12.9         11.2         18         951         0.1754         489           26         15         12         NEE         10.8         22.5         9.2         8.5         417         949         -0.1623         -469         926           27         14         44         NEE	24	14	16	NEE	19.0	21.2	14.3	12.5	595	951	-0.5231	-1328		2052
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	25	13	59	NEE	18.2	22.3	12.9	11.2	893	952	-0.1916	-535		1024
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	15	10	ER	18.3	20.8	13.6	10.4	0	951	0.1678		458	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	22	14	54	ER	19.2	22.0	13.6	11.5	0	951	0.2325		633	
24         14         23         ER         18.2         21.2         14.3         12.5         9         951         0.2844         724           25         14         8         ER         19.0         22.3         12.9         11.2         18         951         0.1754         489           26         15         12         NEE         10.8         22.5         9.2         8.5         417         949         -0.1623         -469         926           27         14         44         NEE         10.6         24.9         8.1         7.2         277         949         -0.1623         -469         926           27         14         44         NEE         10.6         24.9         8.1         7.2         26.6         489         949         -0.1623         -469         926           28         14         29         NEE         10.3         27.9         7.2         6.6         489         949         -0.3062         -877         1188           29         14         14         NEE         9.8         27.8         7.0         291         949         -0.1899         -522         889 <t< td=""><td>23</td><td>14</td><td>39</td><td>ER</td><td>18.9</td><td>23.8</td><td>11.9</td><td>11.3</td><td>0</td><td>951</td><td>0.2933</td><td></td><td>781</td><td></td></t<>	23	14	39	ER	18.9	23.8	11.9	11.3	0	951	0.2933		781	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	24	14	23	ER	18.2	21.2	14.3	12.5	9	951	0.2844		724	
26       15       12       NEE       10.8       22.5       9.2       8.5       417       949       -0.1623       -469       926         27       14       44       NEE       10.6       24.9       8.1       7.2       277       949       -0.1623       -469       926         28       14       29       NEE       10.3       27.9       7.2       6.6       489       949       -0.3062       -877       1188         29       14       14       NEE       9.8       27.8       7.1       6.7       326       949       -0.2069       -580       890         30       13       59       NEE       9.1       29.7       7.5       7.0       291       949       -0.1899       -522       889         26       15       19       ER       12.7       22.5       9.2       8.5       0       949       0.1590       456         27       14       52       ER       10.5       24.9       8.1       7.2       0       949       0.0532       145         28       14       36       ER       10.7       27.9       7.2       6.6       0       949 <td>25</td> <td>14</td> <td>8</td> <td>ER</td> <td>19.0</td> <td>22.3</td> <td>12.9</td> <td>11.2</td> <td>18</td> <td>951</td> <td>0.1754</td> <td></td> <td>489</td> <td></td>	25	14	8	ER	19.0	22.3	12.9	11.2	18	951	0.1754		489	
27       14       44       NEE       10.6       24.9       8.1       7.2       277       949       -0.1543       -422       567         28       14       29       NEE       10.3       27.9       7.2       6.6       489       949       -0.3062       -877       1188         29       14       14       NEE       9.8       27.8       7.1       6.7       326       949       -0.2069       -580       890         30       13       59       NEE       9.1       29.7       7.5       7.0       291       949       -0.1899       -522       889         26       15       19       ER       12.7       22.5       9.2       8.5       0       949       0.1590       456         27       14       52       ER       10.5       24.9       8.1       7.2       0       949       0.0532       145         28       14       36       ER       10.7       27.9       7.2       6.6       0       949       0.1090       312         29       14       21       ER       10.1       27.8       7.1       6.7       0       949       0.1106	26	15	12	NEE	10.8	22.5	9.2	8.5	417	949	-0.1623	-469		926
28       14       29       NEE       10.3       27.9       7.2       6.6       489       949       -0.3062       -877       1188         29       14       14       NEE       9.8       27.8       7.1       6.7       326       949       -0.3062       -877       1188         29       14       14       NEE       9.8       27.8       7.1       6.7       326       949       -0.2069       -580       890         30       13       59       NEE       9.1       29.7       7.5       7.0       291       949       -0.1899       -522       889         26       15       19       ER       12.7       22.5       9.2       8.5       0       949       0.1590       456         27       14       52       ER       10.5       24.9       8.1       7.2       0       949       0.0532       145         28       14       36       ER       10.7       27.9       7.2       6.6       0       949       0.1090       312         29       14       21       ER       10.1       27.8       7.1       6.7       0       949       0.1106	27	14	44	NEE	10.6	24.9	8.1	7.2	277	949	-0.1543	-422		567
29         14         14         NEE         9.8         27.8         7.1         6.7         326         949         -0.2069         -580         890           30         13         59         NEE         9.1         29.7         7.5         7.0         291         949         -0.2069         -580         890           26         15         19         ER         12.7         22.5         9.2         8.5         0         949         0.1590         456           27         14         52         ER         10.5         24.9         8.1         7.2         0         949         0.0532         145           28         14         36         ER         10.7         27.9         7.2         6.6         0         949         0.1090         312           29         14         21         ER         10.1         27.8         7.1         6.7         0         949         0.1106         310           30         14         6         ER         9.7         29.7         7.5         7.0         0         949         0.1340         368	28	14	29	NEE	10.3	27.9	7.2	6.6	489	949	-0.3062	-877		1188
30         13         59         NEE         9.1         29.7         7.5         7.0         291         949         -0.1899         -522         889           26         15         19         ER         12.7         22.5         9.2         8.5         0         949         0.1590         456           27         14         52         ER         10.5         24.9         8.1         7.2         0         949         0.0532         145           28         14         36         ER         10.7         27.9         7.2         6.6         0         949         0.1090         312           29         14         21         ER         10.1         27.8         7.1         6.7         0         949         0.1106         310           30         14         6         ER         9.7         29.7         7.5         7.0         0         949         0.1340         368	29	14	14	NEE	9.8	27.8	7.1	6.7	326	949	-0.2069	-580		890
26       15       19       ER       12.7       22.5       9.2       8.5       0       949       0.1590       456         27       14       52       ER       10.5       24.9       8.1       7.2       0       949       0.0532       145         28       14       36       ER       10.7       27.9       7.2       6.6       0       949       0.1090       312         29       14       21       ER       10.1       27.8       7.1       6.7       0       949       0.106       310         30       14       6       ER       9.7       29.7       7.5       7.0       0       949       0.1340       368	30	13	59	NEL	9.1	29.7	1.5	7.0	291	949	-0.1899	-522		889
27       14       52       ER       10.5       24.9       8.1       7.2       0       949       0.0532       145         28       14       36       ER       10.7       27.9       7.2       6.6       0       949       0.1090       312         29       14       21       ER       10.1       27.8       7.1       6.7       0       949       0.1106       310         30       14       6       ER       9.7       29.7       7.5       7.0       0       949       0.1340       368	26	15	19	ER	12.7	22.5	9.2	8.5	0	949	0.1590		456	
20         14         30         EK         10.7         21.9         7.2         6.6         0         949         0.1090         312           29         14         21         ER         10.1         27.8         7.1         6.7         0         949         0.1090         310           30         14         6         ER         9.7         29.7         7.5         7.0         0         949         0.1340         368	27	14	52	ER	10.5	24.9	8.1	1.2	0	949	0.0532		145	
27 14 21 EK 10.1 27.0 7.1 0.7 0 949 0.1100 310 30 14 6 ER 9.7 29.7 7.5 7.0 0 949 0.1340 368	28	14	30	EK	10.7	27.9	7.2	6.7	0	949	0.1090		210	
	30	14	6	FR	97	27.0	7.5	7.0	0	949	0.1100		368	

S.Table 17: CO<sub>2</sub>-flux measurements and environmental parameters on 26 and 27 Aug.

Plot	Measu Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	(	CO <sub>2</sub> flux	
											mg	CO2 m <sup>2</sup>	h-1
	hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
1	12	3	NEE	23.8	23.4	11.3	8.4	698	962	-0.1695	-373		755
2	12	16	NEE	24.4	21.1	12.1	9.8	774	962	-0.1959	-395		789
3	12	29	NEE	23.7	18.5	11.5	9.2	819	962	-0.18/3	-401		931
4	12	43	NEE	23.2	21.4	11.1	8.3	1/1	962	0.0207	04 041		1383
5	12	50 10	ER	23.8	23.4	13.3	8.4	854 0	962	0.1734	-341	382	884
2	12	23	ER	23.4	21.1	12.1	9.8	0	962	0.1954		395	
3	12	37	ER	22.6	18.5	11.5	9.2	0	962	0.2462		529	
4	12	49	ER	22.9	21.4	11.1	8.3	0	962	0.5539		1437	
5	13	3	ER	23.2	19.8	13.3	10.9	0	962	0.2606		543	
6	13	10	NEE	23.7	17.7	11.8	10.0	790	962	-0.2099	-476		923
7	13	24	NEE	24.8	21.6	10.8	8.1	805	962	-0.1362	-274		821
8	13	36	NEE	25.0	21.6	11.1	8.2	757	962	-0.0821	-180		669
9	13	49	NEE	24.7	36.4	13.7	8.1	738	962	-0.0552	-128		418
10	14	3	NEE	24.5	21.6	10.2	7.5	729	962	0.2479	655	117	730
7	13	30	FP	23.0	21.6	10.8	8.1	0	902	0.1775		547	
, 8	13	43	FR	24.5	21.0	10.0	8.2	0	962	0.2274		489	
9	13	56	FR	24.3	36.4	13.7	8.1	0	962	0.1247		290	
10	14	10	FR	24.3	21.6	10.2	7.5	0	962	0.5238		1385	
11	14	18	NEE	24.8	22.4	14.1	11.1	725	962	-0.1879	-401	1000	862
12	14	31	NEE	25.4	17.6	13.9	11.5	695	961	-0.0626	-129		645
13	14	44	NEE	25.5	16.2	15.0	13.0	723	961	-0.1437	-297		807
14	15	4	NEE	26.9	19.9	16.9	13.2	560	961	-0.0853	-155		662
15	15	17	NEE	26.9	17.5	12.5	10.4	696	961	-0.0237	-62		1480
11	14	25	ER	24.8	22.4	14.1	11.1	0	961	0.2158		461	
12	14	37	ER	24.9	17.6	13.9	11.5	0	961	0.2492		516	
13	14	52	ER	25.6	16.2	15.0	13.0	0	961	0.2469		510	
14	15	11	ER	26.6	19.9	16.9	13.2	0	961	0.2799		508	
15	15	24	ER	26.0	17.5	12.5	10.4	0	961	0.5399		1418	
16	15	30	NEE	26.0	20.5	13.5	11.3	581	961	0.0094	22		572
17	15	43	NEE	25.1	28.6	12.7	9.7	590	961	-0.0945	-213		715
18	15	55	NEE	24.4	21.6	12.5	11.2	561	961	0.0600	155		627
19	16	8	NEE	24.3	24.7	12.6	10.2	541	961	-0.0923	-192		788
20	16	22	NEE	24.3	24.5	13.1	11.3	545	961	-0.3041	-841		1532
16	15	37	ER	25.0	20.5	13.5	11.3	0	961	0.2500		594	
1/	15	49	ER	24.2	28.6	12.7	9.7	0	961	0.2222		502	
18	10	2	ER	23.8	21.6	12.5	11.2	0	961	0.3026		782	
19	10	15	ER	23.5	24.7	12.0	10.2	0	901	0.2808		290	
20	10	2.7 //1	NEE	24.2	24.5	11 0	0.8	651	05.8	-0.0554	-1/0	071	536
∠ I วว	12	54	NEE	24.0	18 /	1/1.9	7.0 11 2	701	750 Q52	-0.0000	- 147		655
23	13	7	NFF	26.0	15.8	14.5	10.9	498	958	-0.1961	-513		1016
24	13	28	NEE	26.9	15.6	15.6	13.8	570	958	-0.2308	-574		1556
25	13	41	NFF	27.7	19.8	15.3	11.0	734	958	-0.0699	-190		601
21	12	47	FR	25.4	20.1	11.9	9.8	0	958	0.1441		387	
22	13	1	ER	26.0	18.4	14.0	11.3	0	958	0.1395		374	
23	13	21	ER	26.5	15.8	14.5	10.9	0	958	0.1924		503	
24	13	35	ER	27.5	15.6	15.6	13.8	0	958	0.3954		982	
25	13	48	ER	28.0	19.8	15.3	11.0	0	958	0.1508		410	
26	13	56	NEE	27.3	17.5	12.7	10.0	363	958	-0.0580	-160		744
27	14	13	NEE	27.2	21.2	14.1	11.1	687	958	-0.0360	-94		614
28	14	32	NEE	26.4	28.9	11.7	8.8	515	957	-0.1361	-372		843
29	15	32	NEE	20.2	19.6	11.6	12.2	338	957	-0.0849	-232		568
30	15	5	NEE	23.8	21.7	13.9	10.9	450	957	0.0904	238		748
26	14	3	ER	27.0	17.5	12.7	10.0	0	957	0.2116		584	
27	14	19	ER	27.3	21.2	14.1	11.1	0	957	0.1997		520	
28	14	44	ER	24.4	28.9	11./	8.8	0	957	0.1713		4/1	
30	15	45	FR	23.7	19.0 21.7	13.0	12.2	0	957	0.1226		337 986	

S.Table 18: CO<sub>2</sub>-flux measurements and environmental parameters on 4 and 5 Sep.

Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	(	CO <sub>2</sub> flux	
											mg	CO2 m <sup>2</sup>	h-1
	hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
1	13	49	NEE	15.4	33.4	9.4	8.6	220	931	0.0647	142		320
2	14	7	NEE	13.2	25.0	11.1	9.9	181	932	0.0442	90		328
3	14	27	NEE	12.1	19.3	10.1	9.5	151	932	0.1408	304		189
4	14	41	NEE	11.6	27.6	10.7	10.1	190	932	0.2252	588		269
5	14	53	FR	11.5	27.6	9.8	9.0	231	932	-0.0021	-4	462	410
2	14	20	FR	12.6	25.0	11.1	9.9	27	932	0.2053		417	
3	14	34	ER	11.7	19.3	10.1	9.5	7	932	0.2279		493	
4	14	47	ER	11.5	27.6	10.7	10.1	2	932	0.3281		858	
5	15	1	ER	11.4	27.6	9.8	9.0	0	932	0.1931		406	
6	15	11	NEE	11.5	28.4	11.6	11.2	164	933	0.0289	66		344
7	15	25	NEE	11.5	31.5	9.6	8.6	206	933	0.0305	62		306
8	15	38	NEE	11.8	26.3	9.6	8.9	210	933	0.0282	63		274
9	15	51	NEE	12.0	35.4	9.9	8.7	186	933	-0.0008	-2		229
10	16	5	NEE	12.4	28.3	10.0	8.8	199	933	0.2120	566	410	268
0	15	18	ER	11.4	28.4	0.6	11.Z 9.6	0	933	0.1788		410	
8	15	32	FP	11.0	26.3	9.0	8.0	0	933	0.1505		336	
9	15	59	FR	12.1	20.3	9.0	8.7	0	933	0.0966		227	
10	16	13	FR	12.1	28.3	10.0	8.8	24	933	0.3119		834	
11	11	9	NEE	9.5	26.6	7.6	7.8	84	934	0.0626	137	001	160
12	11	23	NEE	9.7	18.2	7.8	7.4	89	934	0.0538	114		147
13	11	37	NEE	9.9	17.0	8.5	7.9	95	934	0.1061	225		152
14	11	50	NEE	10.1	21.3	8.1	7.9	93	934	0.0704	131		142
15	12	5	NEE	10.3	22.5	8.1	7.8	116	934	0.1950	525		125
11	11	15	ER	9.7	26.6	7.6	7.8	0	934	0.1362		297	
12	11	30	ER	9.8	18.2	7.8	7.4	0	934	0.1233		261	
13	11	44	ER	10.0	17.0	8.5	7.9	0	934	0.1781		377	
14	11	58	ER	10.2	21.3	8.1	7.9	0	934	0.1468		274	
15	12	12	ER	10.5	22.5	8.1	7.8	0	934	0.2416		650	
16	12	20	NEE	10.7	20.3	8.2	7.7	128	934	0.0473	115		161
17	12	26	NEE	10.9	24.2	7.7	7.3	132	934	0.0461	106		243
18	13	3	NEE	11.8	25.5	8.2	7.4	224	934	0.0738	193		364
19	13	18	NEE	12.4	25.1	8.0	6.9	232	934	-0.0653	-137		423
20	13	33	NEE	12.4	23.8	9.1	7.6	187	934	0.0043	12	075	405
16	12	32	ER	10.9	20.3	8.2	7.7	0	934	0.1136		275	
1/	12	5/	ER	11.4	24.2	1.1	7.3	0	934	0.1522		349	
10	10	24	ER	12.3	25.5	0.2	7.4	0	934	0.2133		207	
20	13	20 41	FR	12.5	23.1	9.1	7.6	0	934	0.1303		200 417	
20	13	36	NEE	17.5	23.0	10.0	9.6	270	931	0.0323	86	417	200
21	13	23	NEE	19.6	27.5	11.2	9.6	674	931	-0.0412	-110		452
23	13	8	NEE	16.7	23.1	13.8	11.8	363	931	-0.2293	-602		1008
24	12	55	NFF	15.8	21.5	11.7	10.1	399	931	-0.0598	-150		775
25	12	42	NEE	16.4	26.3	11.4	10.0	588	931	-0.0206	-57		373
21	13	42	ER	16.5	23.4	10.0	9.6	18	931	0.1065		286	
22	13	29	ER	18.9	27.5	11.2	9.6	19	931	0.1282		342	
23	13	14	ER	17.8	23.1	13.8	11.8	18	931	0.1552		406	
24	13	1	ER	15.6	21.5	11.7	10.1	0	931	0.2487		625	
25	12	48	ER	16.1	26.3	11.4	10.0	0	931	0.1149		316	
26	12	28	NEE	16.4	26.5	11.6	9.9	303	931	0.0197	55		394
27	12	9	NEE	20.3	25.2	10.1	8.3	654	931	0.0038	10		321
28	11	54	NEE	20.1	26.8	10.0	8.4	752	930	-0.1002	-272		632
29	11	42	NEE	20.0	31.6	9.8	8.7	804	931	-0.1292	-343		854
30	11	24	NEE	19.9	22.4	10.9	8.4	407	930	0.1315	341		657
26	12	35	ER	16.1	26.5	11.6	9.9	0	931	0.1612		449	
27	12	15	ER	18.9	25.2	10.1	8.3	0	931	0.1272		331	
28	12	2	ER	20.5	26.8	10.0	8.4	0	930	0.1328		360	
30	11	36	ER	19.3	22.4	7.0 10.9	8.4	0	931	0.1921		999	

S.Table 19: CO<sub>2</sub>-flux measurements and environmental parameters on 11 and 12 Sep.

Nor         Nin         NEE         C         'v         Vi         V         V         C         'V         Hind         Max         ppms <sup>4</sup> NE         Na         Ppms <sup>4</sup> Na         Ppms <sup>4</sup> Na         Na         Ppms <sup>4</sup> Na         Na         Ppms <sup>4</sup> Na         Na         Ppms <sup>4</sup> Na	Plot	Measur Tir	rement ne	Measurem. type	Chamber temp.	Soil moisture	Soil temp 2cm	Soil temp 5cm	PAR	Chamber pressure	Flux slope	(	CO <sub>2</sub> flux	
hour         min         NEE / ER         *C         vol %         *C         rC         rL %         mbar         ppm s1         ML         EA         EA           1         16         19         NEE         101         220         80         7.1         274         963         0.0005         30         7.2         274         963         0.0005         30         7.2         274         963         0.0005         30         7.3         274         963         0.0005         30         7.3         274         963         0.0005         30         7.3         274         963         0.0005         201         7.3         1         6         943         0.0100         4.3         323         7.3         6         943         0.0100         4.3         7.3         6         943         0.0100         4.3         7.3         6         943         0.0100         4.3         7.3         7         7         6         943         0.0100         4.33         7.3         7         7         6         943         0.0103         7.33         7         7         7         7         7         7         7         7         7         7												mg	CO2 m <sup>2</sup>	h-1
1         16         19         MEE         101         220         0.0         7.1         274         963         0.0057         4.65         232           1         15         4.4         MEE         9.5         18.3         4.67         7.7         334         463         0.0057         4.65         222           4         15         17         MEE         9.5         18.0         4.64         462         0.0047         4.65         223           2         16         0.4         MEE         10.1         22.0         4.6         4.7         0.0         463         0.0047         4.65         22.0         1.5         1.5         1.6         1.6         4.7         1.0         9.63         0.00495         2.00         1.5           5         15         9         MEE         1.52         2.24         8.4         3.6         6.57         9.7         0.0079         0.0179         -0.6         2.00           11         12         2.4         1.5         2.29         2.3         1.6         6.57         9.7         0.0079         -0.6         2.00         2.0         2.0         1.5         1.0         0.0079		hour	min	NEE / ER	°C	vol %	°C	°C	μ mol m² s <sup>-1</sup>	mbar	ppm s <sup>-1</sup>	NEE	ER	GEP
2         18         2         NEE         9.5         10.3         6.9         7.7         207         96.3         0.00.51         7.7         272           4         13         17         NEE         9.6         19.2         5.9         6.0         424         962         0.00.51         7.7         27           5         13         0         NEE         10.1         22.2         6.9         7.7         0         963         0.05.9         -9.7         7.7           5         15         5         5         6.8         19.2         2.9         7.7         0         963         0.05.9         9.7         2.9         0.05.9         1.07         0         963         0.07.9         9.7         9.0         0.05.9         1.07         0.05.9         1.07         0.05.9         1.07         0.05.9         1.08         0.05.9         1.08         0.05.9         1.08         1.03         2.00         1.05         0.05.9         1.08         1.03         2.00         1.05         0.05.9         1.08         1.03         2.00         1.05         0.05.9         1.01         2.00         1.05         0.05.9         1.01         1.00         1.0	1	16	19	NEE	10.1	22.0	8.0	7.1	274	963	0.0085	20		232
3       15       44       NEE       9.2       16.6       6.7       7.9       334       96.3       0.0034       2.71       7.72         5       10       NEE       101       2.22       8.4       7.8       4.43       96.2       0.0004       2.71       2.77         1       16       11       17       NEE       101       2.22       8.4       7.8       4.43       96.2       0.0007       4.9       2.77         1       16       11       17       NEE       11.0       2.20       1.0       8.43       0.0       0.0007       4.00       0.0007       4.00       0.0007       4.00       0.0007       4.00       0.0007       4.00       0.0007       4.00       0.0007       <	2	16	2	NEE	9.5	18.3	6.9	7.7	307	963	-0.0307	-65		223
4         15         17         NRE         90         122         59         90         424         902         0.0000         4.18           1         1         21         14         11         122         84         7.8         483         902         0.0000         4.65         237           1         15         53         16         4.5         10.0         90.	3	15	44	NEE	9.2	16.6	6.7	7.9	334	963	0.0253	57		272
5         6         6         6         7         6         6         7         6         7         6         7         6         7	4	15	1/	NEE	9.6	19.2	5.9	6.0	424	962	-0.0804	-218		478
1         1	5	15	24	FR	10.1	23.2	8.4	7.8	458	962	-0.0300	-65	251	329
15         15         15         15         16         16         17         19         0         903         10199         129           6         12         42         MR         135         222         84         78         0         963         0.0953         200         433           6         12         25         MRE         113         224.4         38         36         693         977         0.0959         42         433           7         12         25         MRE         113.4         24.4         48         36         697         0.0195         -66         229           9         11         42         MRE         112         22.9         14         156         0.023         -0149         -06         114           6         12         13         RR         126         22.4         48         39         0         977         0.0103         221           6         12         18         18         129         29         14         38         36         0         967         0.1033         291         395           11         11         33         RR	2	16	11	FR	9.2	18.3	6.9	7.7	0	963	0.0741		157	
4         15         35         IR         86         120         59         40         0         963         1000         203           6         12         42         MLE         135         224         44         39         66         97         0.0090         42         433           7         12         25         MLE         134         224         44         39         66         637         97         0.0090         42         433           8         12         2         MLE         134         225         44         38         57         97         0.0199         36         220           10         11         23         MLE         134         244         38         36         0         977         0.0135         231           6         12         24         RR         134         244         38         36         0         967         0.0133         212           11         13         38         RR         120         37         20         35         0         96         0.0133         212           11         13         38         15         15 <td>3</td> <td>15</td> <td>53</td> <td>FR</td> <td>8.9</td> <td>16.6</td> <td>6.7</td> <td>7.9</td> <td>0</td> <td>963</td> <td>0.1459</td> <td></td> <td>329</td> <td></td>	3	15	53	FR	8.9	16.6	6.7	7.9	0	963	0.1459		329	
5         9         9         9         22         84         78         0         902         0.109         22         433           7         12         25         MIT         13.2         24.4         3.8         3.6         6.97         0.099         -1.68         3.8           7         12         25         MIT         13.2         24.4         3.8         3.6         6.97         0.0190         -1.68         3.8           9         11         42         MIT         13.2         29.9         3.9         4.1         5.06         0.0240         -1.61         206           10         11         42         MIT         12.6         22.4         4.8         3.9         0         9.7         0.1033         215           10         11         3.3         ER         12.0         20.9         3.5         0         9.67         0.0033         216           11         11         3.3         ER         12.0         30.7         2.0         35.0         9.66         0.0037         1.2         3.9         1.13         3.9         1.4         1.40         9.42         0.0105         -248         5.7	4	15	35	FR	8.5	19.2	5.9	6.0	0	963	0.0952		260	
6       12       42       NRE       13.5       2.24       4.8       3.4       5.88       977       0.0395       4.72       4.33         8       12       2.5       NRE       13.4       2.65       4.44       3.8       5.95       977       0.0395       -1.68       330         9       11       2.2       NRE       13.4       2.65       4.4       3.8       9.57       0.0495       -0.0495	5	15	9	ER	9.6	23.2	8.4	7.8	0	962	0.1206		263	
7       12       25       NEE       13.2       2.4.4       3.8       3.6       6.87       6.97       0.0180      36       2.99         9       11       4.2       NEE       12.5       2.99       3.9       4.1       5.636       6.97       0.0180      36       2.99         7       12       51       ER       12.4       2.4       4.8       3.0       6.97       0.0133      233      233         8       12       3.4       ER       12.5       2.65       4.4       3.8       6.0       6.97       0.0133      233      233         9       11       3.3       ER       12.5       2.65       4.4       3.8       6.0       6.97       0.0133      233      233         10       11       13       3.5       ER       12.5       2.66       0.5       6.4       6.92       0.0038      99      99      99      99      99       0.0038      99      99      99      99      99      99      99      99      99      99      99      99      99      99      99	6	12	42	NEE	13.5	22.4	4.8	3.9	588	957	-0.0395	-92		433
8         12         2         NEE         13.4         2.05         4.4         3.8         6.75         6.977         0.0199         3.60         230           10         11         23         NEE         13.1         30.7         2.0         15         248         6.957         0.0185         .0240         .06         141           6         12         34         ER         13.4         32.4         4.88         3.6         0.7         6.013         .231         .231           6         13         16         ER         12.5         2.04         4.8         3.6         0.7         6.013         .231         .231           9         11         13         ER         12.9         2.02         3.5         0.0         6.97         0.0030         .231         .231           10         11         43         NEE         13.3         22.6         6.0         6.7         6.92         0.0050         .141         99           11         13         14         14         14.7         11.0         9.9         7.1         6.0         6.97         0.0030         .141         23.0         133         132         <	7	12	25	NEE	13.2	24.4	3.8	3.6	639	957	-0.0806	-168		383
9         11         42         MEE         125         299         3.9         4.1         506         956         4.0430         -108         230           6         12         51         BR         126         224         4.8         39         0         977         0.1455         341           7         12         34         ER         13.4         24.4         3.8         30         0         977         0.1023         235           9         11         53         ER         12.5         24.6         4.4         3.8         0         977         0.1023         23.5           10         11         43         RR         12.0         30.7         2.0         3.5         2.4         90.7         0.1023         2.3         33           11         11         48         RR         12.6         2.4         6.0         5.5         0         96.4         0.006.6         14.4         197           12         12         41         RE         13.5         16.1         90.7         7.1         6.6         0.0         962         0.0135         14.3         14.2         13.3         15.7 <th< td=""><td>8</td><td>12</td><td>2</td><td>NEE</td><td>13.4</td><td>26.5</td><td>4.4</td><td>3.8</td><td>575</td><td>957</td><td>-0.0159</td><td>-36</td><td></td><td>269</td></th<>	8	12	2	NEE	13.4	26.5	4.4	3.8	575	957	-0.0159	-36		269
10       11       23       NEE       12       34       BR       12.6       2.4       4.8       39       0       997       0.1133       215         7       12       34       BR       13.4       24.4       3.8       3.0       0       997       0.1133       215         9       11       53       BR       12.0       20.9       3.9       4.1       0       957       0.00507       122         10       11       33       BR       12.0       20.7       20.0       35       0       956       0.00507       122         11       11       48       NEE       13.3       12.4       6.0       5.6       6.0       962       0.0050       14       199         12       12       6       NEE       14.7       16.1       90       7.9       470       962       -0.0105       -193       426       521         13       12       24       NEE       14.7       16.1       90       7.9       420       0.0070       193       126       123       126       123       126       123       127       231       121       121       124       124 </td <td>9</td> <td>11</td> <td>42</td> <td>NEE</td> <td>12.5</td> <td>29.9</td> <td>3.9</td> <td>4.1</td> <td>506</td> <td>957</td> <td>-0.0450</td> <td>-108</td> <td></td> <td>230</td>	9	11	42	NEE	12.5	29.9	3.9	4.1	506	957	-0.0450	-108		230
6         12         51         ER         13.4         24.4         3.8         3.9         0         9.97         0.13.3         215           8         12         16         ER         12.5         26.5         4.4         3.8         0.         957         0.1023         233           9         11         53         ER         12.0         20.         3.5         0.         956         0.0056         122           10         11         48         MKE         13.3         22.4         6.0         56         2.4         962         0.0056         .14         198           13         12         2.4         MEE         14.1         199         8.9         7.1         616         962         0.0105         .138         571           14         12         41         MEE         16.1         13.3         7.9         7.2         632         962         0.0052         183           13         12         15         R         13.6         18.5         7.5         6.6         0         962         0.0105         .238           14         12         50         FR         13.6         18	10	11	23	NEE	13.1	30.7	2.0	3.5	248	956	-0.0240	-66		164
I       IZ       IA       IA <thia< th="">       IA       IA       I</thia<>	6	12	51	ER	12.6	22.4	4.8	3.9	0	957	0.1455		341	
B         12         16         LR         12.9         29.0         3.4         3.8         0         977         0.0057         123           10         11         33         ER         12.0         30.7         20         35.5         0         666         0.0589         -0.9         87           11         11         48         NEE         13.3         22.4         6.0         5.6         22.4         96.2         -0.0066         -1.4         198           13         12         24         NEE         16.1         19.9         89         7.1         616         962         -0.0105         -2.94         52.1           14         12         24         NEE         16.1         23.8         7.9         7.2         632         -0.0070         193         -2.44         52.1           13         12         15         ER         13.6         18.5         7.5         6.6         0         962         0.0172         2.33         193         3.6         13.3         13.4         13.5         1.1         16.1         9.0         7.7         0         9.62         0.1727         2.33         13.3         3.65	/	12	34	ER	13.4	24.4	3.8	3.6	0	957	0.1033		215	
9         11         53         ER         120         307         20         35         6         965         00358         98           111         11         48         NEE         133         224         60         5.6         264         962         00066         -201         375           12         12         6         NEE         133         126         6.6         667         962         00066         -214         375           13         12         24         NEE         161         90         79         72         652         962         -0103         -975         476           11         18         ER         128         79         72         652         962         -0106         -29         515           11         11         68         ER         128         77         72         6         0         662         00282         183           12         12         15         ER         136         176         161         9         79         72         0         962         0.1792         486           13         12         S0         ER         133	8	12	16	ER	12.5	26.5	4.4	3.8	0	957	0.1023		233	
ID         II         IA         IA <thia< th="">         IA         IA         IA<!--</td--><td>9</td><td>11</td><td>53</td><td>ER</td><td>12.9</td><td>29.9</td><td>3.9</td><td>4.1</td><td>0</td><td>957</td><td>0.0507</td><td></td><td>122</td><td></td></thia<>	9	11	53	ER	12.9	29.9	3.9	4.1	0	957	0.0507		122	
12         12         12         6         NEE         135         125         7.5         6.6         607         962         4.0066         1.4         188           13         12         2.4         NEE         14.1         16.1         9.0         7.7         470         962         4.0135         -248         521           14         12         2.4         NEE         16.1         23.8         7.9         7.2         632         40.0135         -7.9         55           11         15         FR         12.8         22.6         6.0         962         0.0125         195           12         15         FR         13.6         15.7         16.1         9.0         7.7         0         962         0.1227         23.1           15         13         11         FR         16.9         23.8         7.9         7.2         0         962         0.1227         23.1           15         13         11         FR         16.9         23.8         7.9         7.2         0         962         0.1727         23.13         365           17         13         32         NEE         13.3	10	11	33 48	ER NFF	12.0	30.7	2.0	3.5 5.6	254	956	-0.0358	-201	98	395
13         12         24         NEE         14.7         16.1         90         79         470         962         -0.1153         -248         521           14         12         41         NEE         16.1         199         8.9         7.1         616         962         -0.0135         -195         426           11         11         58         ER         12.8         7.7         66.0         962         0.0135         -195         426           12         12         15         ER         12.6         17.7         16.1         0.7         0         962         0.1279         273           14         12         50         ER         15.7         16.1         0.7         0         962         0.1279         273           15         13         11         ER         16.9         2.38         7.7         0         962         0.1279         2.01792         466           13         14         6.4         NEE         11.3         2.12         5.2         4.3         602         957         0.0538         -1.33         365           14         12         14         6.4         NEE	12	12	6	NFF	13.5	18.5	7.5	6.6	607	962	-0.0066	-14		198
14         12         41         NEE         16.1         19.9         8.9         7.1         616         962         -0.103         -195         426           15         12         59         NEE         16.1         2.3         7.9         7.2         632         962         -0.016         .29         515           12         12         15         ER         13.6         185         7.5         6.6         0         962         0.0852         183           13         12         33         ER         15.7         10.9         962         0.1279         231           15         13         11         ER         16.9         23.8         7.9         7.2         0         962         0.1792         486           16         13         15         NEE         13.3         19.9         5.2         4.3         602         957         0.0245         6.6         368           17         13         32         NEE         11.4         25.4         5.8         5.3         544         957         0.0245         6.6         368           17         13         24         ER         12.2         <	13	12	24	NFF	14.7	16.1	9.0	7.9	470	962	-0.1153	-248		521
15         12         59         NEE         16.1         23.8         79         7.2         63.2         96.2         -0.0168         -2.9         515           11         11         58         ER         12.8         22.6         6.0         5.6         0         96.2         0.0870         193           13         12         33         ER         15.7         16.1         9.0         7.9         0         96.2         0.127         233           14         12         50         ER         15.8         19.9         8.9         7.1         0         96.2         0.1727         233           15         13         11         ER         16.9         2.2.8         7.9         7.2         0         96.2         0.1727         2.33         365           16         13         49         NEE         11.4         2.4         5.8         5.3         5.44         957         -0.0245         -6.6         368           18         13         49         NEE         11.8         2.9.7         7.6         6.3         0         957         0.1168         2.27           14         43         ER	14	12	41	NFF	16.1	19.9	8.9	7.1	616	962	-0.1035	-195		426
	15	12	59	NEE	16.1	23.8	7.9	7.2	632	962	-0.0106	-29		515
12         12         15         ER         136         185         7.5         6.6         0         962         0.0852         183           13         12         33         ER         157         16.1         90         7.9         0         962         0.1279         23           15         13         11         ER         158         199         89         7.1         0         962         0.1792         486           16         13         15         NEE         133         199         5.2         4.3         602         957         -0.0538         -133         365           17         13         22         NEE         11.4         25.4         5.8         5.3         544         957         -0.0245         -6.6         368           19         14         6         NEE         11.8         22.9         5.0         4.5         709         957         -0.0245         -6.6         368           10         13         24         ER         12.2         19.9         5.2         4.3         0         957         0.0148         232           16         13         24         ER <td>11</td> <td>11</td> <td>58</td> <td>FR</td> <td>12.8</td> <td>22.6</td> <td>6.0</td> <td>5.6</td> <td>0</td> <td>962</td> <td>0.0870</td> <td></td> <td>193</td> <td></td>	11	11	58	FR	12.8	22.6	6.0	5.6	0	962	0.0870		193	
13         12         33         ER         15.7         16.1         9.0         7.9         0         962         0.1279         273           14         12         50         ER         15.8         19.9         8.9         7.1         0         962         0.1279         231           16         13         15         NEE         13.3         19.9         5.2         4.3         602         957         -0.0538         -1.33         365           17         13         3.2         NEE         12.1         21.2         5.4         5.4         6.957         0.0245         6.6         368           19         14         6         NEE         11.8         28.9         5.0         4.5         709         957         -0.1546         -333         558           20         14         23         NEE         12.8         22.7         7.6         6.3         0         957         0.0164         225           16         13         24         ER         11.3         21.2         5.4         5.4         0         957         0.1164         225           17         13         41         ER	12	12	15	FR	13.6	18.5	7.5	6.6	0	962	0.0852		183	
14         12         50         ER         15.8         19.9         8.9         7.1         0         962         0.1227         231           15         13         11         ER         16.9         23.8         7.9         7.2         0         962         0.1727         231           16         13         15         NEE         13.3         19.9         5.2         4.3         602         957         -0.0538         -13.3         365           17         13         32         NEE         11.4         25.4         5.8         5.3         544         957         -0.0245         -66         368           19         14         6         NEE         11.8         28.9         5.0         4.5         709         957         -0.0545         -66         368           10         14         23         NEE         12.2         19.9         5.2         4.3         0         957         -0.057         -16         362           16         13         24         ER         11.1         25.4         5.4         0         957         -0.164         222         17         13         41         8.9	13	12	33	FR	15.7	16.1	9.0	7.9	0	962	0.1279		273	
15         13         11         ER         16.9         23.8         7.9         7.2         0         962         0.1792         486           16         13         15         NEE         13.3         19.9         5.2         4.3         602         957         -0.0538         -133         365           17         13         32         NEE         12.1         21.2         5.4         5.4         5.6         957         -0.0538         -133         365           18         13         49         NEE         11.4         25.4         5.4         5.6         957         -0.0245         -66         368           19         14         6         NEE         11.8         28.9         5.0         4.5         709         957         -0.1546         -333         558           20         14         23         NEE         12.2         19.9         5.2         4.3         0         957         -0.1168         2275           18         13         58         ER         11.1         25.4         5.8         5.3         0         957         -0.1208         345           20         14         33	14	12	50	FR	15.8	19.9	8.9	7.1	0	962	0.1227		231	
16         13         15         NEE         13.3         19.9         5.2         4.3         602         957         -0.0538         -133         365           17         13         32         NEE         12.1         21.2         5.4         5.4         556         957         0.0224         61         213           18         13         49         NEE         11.4         25.4         5.8         5.3         544         957         -0.0245         -66         368           20         14         23         NEE         12.8         22.7         7.6         6.3         588         957         -0.0057         -16         332           16         13         24         ER         12.2         19.9         5.2         4.3         0         957         0.0057         -16         322           16         13         24         ER         12.2         28.9         5.0         4.5         0         957         0.1144         302         275           18         13         58         ER         11.1         25.4         5.8         5.3         0         957         0.1024         -76         280	15	13	11	ER	16.9	23.8	7.9	7.2	0	962	0.1792		486	
17       13       32       NEE       12.1       21.2       5.4       5.6       997       0.0262       6.1       213         18       13       49       NEE       11.4       25.4       5.8       5.3       544       957       -0.0245       -6.6       368         19       14       6       NEE       11.8       22.7       7.6       6.3       588       957       -0.0245       -6.6       352         16       13       24       ER       12.2       19.9       5.2       4.3       0       957       0.0938       232         17       13       41       ER       11.3       21.2       5.4       5.4       0       957       0.1168       275         18       13       5.8       ER       11.1       25.4       5.8       0       957       0.1044       225         20       14       33       ER       13.3       22.7       7.6       6.3       0       957       0.1208       345         21       14       42       NEE       13.0       22.3       5.6       5.9       5.37       958       -0.0274       -76       280	16	13	15	NEE	13.3	19.9	5.2	4.3	602	957	-0.0538	-133		365
18         13         49         NEE         11.4         25.4         5.8         5.3         544         997         -0.0245         -66         368           19         14         6         NEE         11.8         289         5.0         4.5         709         957         -0.1546         -333         558           20         14         23         NEE         12.8         22.7         7.6         6.3         588         957         -0.0057         -16         362           16         13         24         ER         12.2         5.4         5.4         0         957         0.0168         232           17         13         41         ER         11.3         21.2         5.4         5.4         0         957         0.1124         302           19         14         15         ER         12.2         28.9         5.0         4.5         0         957         0.1044         22.5           20         14         42         NEE         13.0         22.3         5.6         5.9         5.37         958         -0.0254         -7.6         280           21         14         42	17	13	32	NEE	12.1	21.2	5.4	5.4	556	957	0.0262	61		213
19         14         6         NEE         11.8         28.9         5.0         4.5         709         957         -0.1546         -3.33         558           20         14         23         NEE         12.8         22.7         7.6         6.3         588         957         -0.057         -1.6         362           16         13         24         ER         11.2         19.9         5.2         4.3         0         957         0.0938         222           17         13         41         ER         11.3         21.2         5.4         5.4         0         957         0.1124         302           19         14         15         ER         12.2         28.9         5.0         4.5         0         957         0.1044         225           20         14         33         ER         13.3         22.7         7.6         6.3         0         957         0.1044         2.25           21         14         42         NE         13.0         22.3         5.6         5.9         5.37         958         -0.0274         -7.6         5.37           22         14         59	18	13	49	NEE	11.4	25.4	5.8	5.3	544	957	-0.0245	-66		368
20         14         23         NEE         12.8         22.7         7.6         6.3         588         957         -0.057         -1.6         362           16         13         24         ER         12.2         19.9         5.2         4.3         0         957         0.0938         232           17         13         41         ER         11.3         21.2         5.4         5.4         0         957         0.1168         275           19         14         15         ER         12.2         28.9         5.0         4.5         0         957         0.1044         225           20         14         33         ER         13.3         22.7         7.6         6.3         0         957         0.1248         345           21         14         42         NEE         13.0         22.3         5.6         5.9         537         958         -0.0274         -7.6         280           22         14         59         NEE         13.0         22.3         5.5         5.6         958         -0.078         -216         543           24         15         38         NEE         <	19	14	6	NEE	11.8	28.9	5.0	4.5	709	957	-0.1546	-333		558
16         13         24         ER         122         19.9         5.2         4.3         0         957         0.0938         232           17         13         41         ER         11.3         21.2         5.4         5.4         0         957         0.1168         275           18         13         58         ER         11.1         25.4         5.8         5.3         0         957         0.1164         225           20         14         33         ER         13.3         22.7         7.6         6.3         0         957         0.1208         345           21         14         42         NEE         13.9         24.5         6.1         5.3         558         957         0.0274         -7.6         280           22         14         59         NEE         13.0         22.3         5.6         5.9         5.75         8.00205         -5.7         279           23         15         18         NEE         13.4         21.3         7.1         6.4         509         958         0.0791         -253         572           25         15         57         NEE         <	20	14	23	NEE	12.8	22.7	7.6	6.3	588	957	-0.0057	-16		362
17         13         41         ER         11.3         21.2         5.4         5.4         0         957         0.1168         275           18         13         58         ER         11.1         25.4         5.8         5.3         0         957         0.1124         302           19         14         15         ER         12.2         28.9         5.0         4.5         0         957         0.1044         225           20         14         33         ER         13.3         22.7         7.6         6.3         0         957         0.0274         -7.6         280           21         14         42         NEE         13.0         22.3         5.6         5.9         537         958         -0.025         -5.7         279           23         15         18         NEE         13.4         21.3         7.1         6.4         509         958         -0.0788         -216         543           24         15         38         NEE         13.1         22.5         5.5         6.0         408         958         0.0172         203           22         15         5 <t< td=""><td>16</td><td>13</td><td>24</td><td>ER</td><td>12.2</td><td>19.9</td><td>5.2</td><td>4.3</td><td>0</td><td>957</td><td>0.0938</td><td></td><td>232</td><td></td></t<>	16	13	24	ER	12.2	19.9	5.2	4.3	0	957	0.0938		232	
18         13         58         ER         11.1         25.4         5.8         5.3         0         957         0.1124         302           19         14         15         ER         12.2         28.9         5.0         4.5         0         957         0.1044         225           20         14         33         ER         13.3         22.7         7.6         6.3         0         957         0.128         345           21         14         42         NEE         13.9         24.5         6.1         5.3         558         957         -0.0274         -76         280           22         14         59         NEE         13.0         22.3         5.6         5.9         537         958         -0.0274         -76         543           24         15         38         NEE         13.4         21.3         7.1         6.4         509         958         -0.071         -253         572           25         15         57         NEE         13.1         23.5         5.5         6.0         408         958         0.0390         112         189           21         14	17	13	41	ER	11.3	21.2	5.4	5.4	0	957	0.1168		275	
19         14         15         ER         122         28.9         5.0         4.5         0         957         0.1044         225           20         14         33         ER         13.3         22.7         7.6         6.3         0         957         0.1208         345           21         14         42         NEE         13.9         24.5         6.1         5.3         558         957         -0.0274         -7.6         280           22         14         59         NEE         13.0         22.3         5.6         5.9         537         958         -0.0274         -7.6         280           23         15         18         NEE         12.4         16.8         6.5         5.8         626         958         -0.0788         -216         543           24         15         38         NEE         13.4         21.3         7.1         6.4         509         958         0.0791         -253         572           25         15         57         NEE         13.1         23.5         5.5         6.0         408         958         0.0790         222         22         23         15	18	13	58	ER	11.1	25.4	5.8	5.3	0	957	0.1124		302	
20         14         33         ER         13.3         22.7         7.6         6.3         0         957         0.1208         345           21         14         42         NEE         13.9         24.5         6.1         5.3         558         957         -0.0274         -76         280           22         14         59         NEE         13.0         22.3         5.6         5.9         537         958         -0.0276         -76         280           23         15         18         NEE         12.4         16.8         6.5         5.8         626         958         -0.0788         -216         543           24         15         38         NEE         13.1         23.5         5.6         6.0         408         958         0.0390         112         189           21         14         51         ER         13.0         24.5         6.1         5.3         0         958         0.0790         222           23         15         27         ER         13.3         16.8         6.5         5.8         0         958         0.1221         319         20           24	19	14	15	ER	12.2	28.9	5.0	4.5	0	957	0.1044		225	
21       14       42       NEE       13.9       24.5       6.1       5.3       558       957       -0.0274       -76       280         22       14       59       NEE       13.0       22.3       5.6       5.9       537       958       -0.0205       -57       279         23       15       18       NEE       12.4       16.8       6.5       5.8       626       958       -0.0788       -216       543         24       15       38       NEE       13.4       21.3       7.1       6.4       509       958       -0.0711       -253       572         25       15       57       NEE       13.1       23.5       5.5       6.0       408       958       0.0390       112       189         21       14       51       ER       13.0       24.5       6.1       5.3       0       957       0.0727       203         22       15       8       ER       12.4       22.3       5.6       5.9       0       958       0.1790       222       23         23       15       27       ER       13.3       16.8       6.5       5.8       0	20	14	33	ER	13.3	22.7	7.6	6.3	0	957	0.1208		345	
22       14       59       NEE       13.0       22.3       5.6       5.9       537       958       -0.0205       -57       279         23       15       18       NEE       12.4       16.8       6.5       5.8       626       958       -0.0788       -216       543         24       15       38       NEE       13.4       21.3       7.1       6.4       509       958       -0.071       -253       572         25       15       57       NEE       13.1       23.5       5.5       6.0       408       958       0.0901       12       189         21       14       51       ER       13.0       24.5       6.1       5.3       0       957       0.0727       203         22       15       8       ER       12.4       22.3       5.6       5.9       0       958       0.0790       222         23       15       27       ER       13.3       16.8       6.5       5.8       0       958       0.1047       301         24       15       48       ER       12.2       23.5       5.5       6.0       0       958       0.1047	21	14	42	NEE	13.9	24.5	6.1	5.3	558	957	-0.0274	-76		280
23       15       18       NEE       12.4       16.8       6.5       5.8       626       958       -0.0788       -216       543         24       15       38       NEE       13.4       21.3       7.1       6.4       509       958       -0.0781       -253       572         25       15       57       NEE       13.1       23.5       5.5       6.0       408       958       0.0390       112       189         21       14       51       ER       13.0       24.5       6.1       5.3       0       957       0.0727       203         22       15       8       ER       12.4       22.3       5.6       5.9       0       958       0.0790       222         23       15       2.7       ER       13.3       16.8       6.5       5.8       0       958       0.1047       327         24       15       48       ER       12.2       23.5       5.5       6.0       0       958       0.1047       301         25       16       5       ER       12.2       23.5       5.5       6.0       0       958       0.1047       314       <	22	14	59	NEE	13.0	22.3	5.6	5.9	537	958	-0.0205	-57		279
24         15         38         NEE         13.4         21.3         7.1         6.4         509         958         -0.0971         -253         572           25         15         57         NEE         13.1         23.5         5.5         6.0         408         958         0.0390         112         189           21         14         51         ER         13.0         24.5         6.1         5.3         0         957         0.0727         203           22         15         8         ER         12.4         22.3         5.6         5.9         0         958         0.0790         222           23         15         27         ER         13.3         16.8         6.5         5.8         0         958         0.1196         327           24         15         48         ER         12.2         23.5         5.5         6.0         0         958         0.1047         301           25         16         5         ER         12.2         23.5         5.5         6.0         0         958         0.1047         301           26         13         20         NEE         16.5	23	15	18	NEE	12.4	16.8	6.5	5.8	626	958	-0.0788	-216		543
251557NEE13.123.55.56.04089580.0390112189211451ER13.024.56.15.309570.072720322158ER12.422.35.65.909580.0790222231527ER13.316.86.55.809580.1196327241548ER12.521.37.16.409580.122131925165ER12.223.55.56.009580.1047301261320NEE16.519.07.06.8490962-0.0218-6.3421281355NEE14.129.06.76.1568962-0.0350-100373291423NEE12.424.26.46.05279620.009125160261328ER15.719.07.06.809620.0269-76338301440NEE11.224.26.46.05279620.009125160261328ER15.719.07.06.809620.0245359209271347ER14.124.36.45.40962	24	15	38	NEE	13.4	21.3	7.1	6.4	509	958	-0.0971	-253		572
21         14         51         ER         13.0         24.5         6.1         5.3         0         957         0.0727         203           22         15         8         ER         12.4         22.3         5.6         5.9         0         958         0.0790         222           23         15         27         ER         13.3         16.8         6.5         5.8         0         958         0.1196         327           24         15         48         ER         12.5         21.3         7.1         6.4         0         958         0.1047         301           25         16         5         ER         12.2         23.5         5.5         6.0         0         958         0.1047         301           26         13         20         NEE         16.5         19.0         7.0         6.8         490         962         -0.0218         -6.3         421           28         13         55         NEE         14.1         29.0         6.7         6.1         568         962         -0.0269         -76         338           30         14         40         NEE         12.	25	15	57	NEE	13.1	23.5	5.5	6.0	408	958	0.0390	112		189
22       15       8       ER       12.4       22.3       5.6       5.9       0       958       0.0790       222         23       15       27       ER       13.3       16.8       6.5       5.8       0       958       0.1196       327         24       15       48       ER       12.5       21.3       7.1       6.4       0       958       0.1221       319         25       16       5       ER       12.2       23.5       5.5       6.0       0       958       0.1047       301         26       13       20       NEE       16.5       19.0       7.0       6.8       490       962       -0.0218       -6.3       421         27       13       37       NEE       15.4       24.3       6.4       5.4       613       962       -0.0218       -6.3       421         28       13       55       NEE       14.1       20.9       6.7       6.1       568       962       -0.0269       -7.6       338         30       14       40       NEE       11.2       24.2       6.4       6.0       527       962       0.0091       25	21	14	51	ER	13.0	24.5	6.1	5.3	0	957	0.0727		203	
23       15       27       ER       13.3       16.8       6.5       5.8       0       958       0.1196       327         24       15       48       ER       12.5       21.3       7.1       6.4       0       958       0.1221       319         25       16       5       ER       12.2       23.5       5.5       6.0       0       958       0.1047       301         26       13       20       NEE       16.5       19.0       7.0       6.8       490       962       -0.0218       -6.3       421         27       13       37       NEE       15.4       24.3       6.4       5.4       613       962       -0.0218       -6.3       421         28       13       55       NEE       14.1       20.9       6.7       6.1       568       962       -0.0350       -100       338         30       14       40       NEE       11.2       24.2       6.4       6.0       527       962       0.0091       25       160         26       13       28       ER       15.7       19.0       7.0       6.8       0       962       0.091	22	15	8	ER	12.4	22.3	5.6	5.9	0	958	0.0790		222	
24         15         48         ER         12.5         21.3         7.1         6.4         0         958         0.1221         319           25         16         5         ER         12.2         23.5         5.5         6.0         0         958         0.1047         301           26         13         20         NEE         16.5         19.0         7.0         6.8         490         962         -0.0218         -6.3         421           27         13         37         NEE         15.4         24.3         6.4         5.4         613         962         -0.0218         -6.3         421           28         13         55         NEE         14.1         29.0         6.7         6.1         568         962         -0.0350         -100         373           29         14         23         NEE         12.4         20.9         6.7         6.3         537         962         -0.0269         -76         338           30         14         40         NEE         11.2         24.2         6.4         6.0         527         962         0.0091         25         160           26	23	15	27	ER	13.3	16.8	6.5	5.8	0	958	0.1196		327	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	24	15	48	ER	12.5	21.3	7.1	6.4	0	958	0.1221		319	
26       13       20       NEE       16.5       19.0       7.0       6.8       490       962       -0.0218       -63       421         27       13       37       NEE       15.4       24.3       6.4       5.4       613       962       -0.0218       -63       421         28       13       55       NEE       14.1       29.0       6.7       6.1       568       962       -0.0350       -100       373         29       14       23       NEE       12.4       20.9       6.7       6.3       537       962       -0.0269       -76       338         30       14       40       NEE       11.2       24.2       6.4       6.0       527       962       0.0091       25       160         26       13       28       ER       15.7       19.0       7.0       6.8       0       962       0.1245       359         27       13       47       ER       14.1       24.3       6.4       5.4       0       962       0.0765       209         28       14       14       ER       12.2       29.0       6.7       6.1       0       962	25	16	5	ER	12.2	23.5	5.5	6.0	0	958	0.1047		301	
2/       13       3/       NEE       15.4       24.3       6.4       5.4       613       962       0.0543       148       61         28       13       55       NEE       14.1       29.0       6.7       6.1       568       962       -0.0350       -100       373         29       14       23       NEE       12.4       20.9       6.7       6.3       537       962       -0.0269       -76       338         30       14       40       NEE       11.2       24.2       6.4       6.0       527       962       0.0091       25       160         26       13       28       ER       15.7       19.0       7.0       6.8       0       962       0.1245       359         27       13       47       ER       14.1       24.3       6.4       5.4       0       962       0.0765       209         28       14       14       ER       12.2       29.0       6.7       6.1       0       962       0.0944       272         29       14       31       ER       11.3       20.9       6.7       6.3       0       962       0.0928	26	13	20	NEE	16.5	19.0	/.0	6.8	490	962	-0.0218	-63		421
28       13       55       NEE       14.1       29.0       6.7       6.1       568       962       -0.0350       -100       373         29       14       23       NEE       12.4       20.9       6.7       6.3       537       962       -0.0269       -76       338         30       14       40       NEE       11.2       24.2       6.4       6.0       527       962       0.0091       25       160         26       13       28       ER       15.7       19.0       7.0       6.8       0       962       0.1245       359         27       13       47       ER       14.1       24.3       6.4       5.4       0       962       0.0765       209         28       14       14       ER       12.2       29.0       6.7       6.1       0       962       0.0944       272         29       14       31       ER       11.3       20.9       6.7       6.3       0       962       0.0944       272	27	13	37	NEE	15.4	24.3	6.4	5.4	613	962	0.0543	148		61
29       14       23       NEE       12.4       20.9       6.7       6.3       537       962       -0.0269       -76       338         30       14       40       NEE       11.2       24.2       6.4       6.0       527       962       0.0091       25       160         26       13       28       ER       15.7       19.0       7.0       6.8       0       962       0.1245       359         27       13       47       ER       14.1       24.3       6.4       5.4       0       962       0.0765       209         28       14       14       ER       12.2       29.0       6.7       6.1       0       962       0.0944       272         29       14       31       ER       11.3       20.9       6.7       6.3       0       962       0.0928       263	28	13	55	NEE	14.1	29.0	6.7	6.1	568	962	-0.0350	-100		3/3
30     14     40     NEE     11.2     24.2     6.4     6.0     527     962     0.0091     25     160       26     13     28     ER     15.7     19.0     7.0     6.8     0     962     0.1245     359       27     13     47     ER     14.1     24.3     6.4     5.4     0     962     0.0765     209       28     14     14     ER     12.2     29.0     6.7     6.1     0     962     0.0944     272       29     14     31     ER     11.3     20.9     6.7     6.3     0     962     0.0928     263	29	14	23	NEE	12.4	20.9	6./	6.3	537	962	-0.0269	-/6		338
26       13       28       ER       15.7       19.0       7.0       6.8       0       962       0.1245       359         27       13       47       ER       14.1       24.3       6.4       5.4       0       962       0.0765       209         28       14       14       ER       12.2       29.0       6.7       6.1       0       962       0.0944       272         29       14       31       ER       11.3       20.9       6.7       6.3       0       962       0.0928       263	30	14	40	NEE	11.2	24.2	0.4	0.U	527	962	0.0091	25	055	160
27       13       47       ER       14.1       24.3       6.4       5.4       0       962       0.0765       209         28       14       14       ER       12.2       29.0       6.7       6.1       0       962       0.0944       272         29       14       31       ER       11.3       20.9       6.7       6.3       0       962       0.0928       263	26	13	28	ER	15.7	19.0	7.0	6.8	0	962	0.1245		359	
26         14         14         ER         12.2         29.0         6.7         6.1         0         962         0.0944         272           29         14         31         ER         11.3         20.9         6.7         6.3         0         962         0.0928         263	27	13	4/	ER	14.1	24.3	6.4	5.4	0	962	0.0765		209	
27 14 31 EK 11.3 20.4 0.7 6.3 0 962 0.0928 263	28	14	14	EK	12.2	29.0	0./	0.1	0	962	0.0944		2/2	
30 14 49 FR 10.3 24.2 6.4 6.0 0 962 0.0666 185	30	14	49	FR	10.3	20.7	6.4	6.0	0	962	0.0666		185	

S.Table 20: CO<sub>2</sub>-flux measurements and environmental parameters on 19 and 20 Sep.

10.5	Data	of	enzyme	activities

Plot	Soil depth	Soil mass*	water content	dry weight	Enzyme	Activity
Nr.	cm	(g)	(g water g <sup>-1</sup> soil)	(g)		(nmol g <sup>-1</sup> soil h <sup>-1</sup> )
1	0-5	0.994	385	0.204764	BX	121.25
2	0-5	0.985	558	0.14972	BX	41.75
3	0-5	0.978	594	0.140832	BX	93.16
4	0-5	0.999	488	0.16983	BX	102.99
5	0-5	0.964	294	0.244856	BX	130.63
6	0-5	0.975	355	0.2145	BX	/6./8
/	0-5	0.962	339	0.219330	BX	123.32
8	0-5	0.991	488	0.10847	BA DV	101.0
10	0-5	0.965	533	0.272970	BX	179.27
11	0-5	0.963	694	0 121338	BX	48.56
12	0-5	0.963	576	0.142524	BX	81.3
13	0-5	1.011	456	0.18198	BX	101.59
14	0-5	0.978	475	0.170172	BX	75.42
15	0-5	0.951	339	0.216828	BX	124.12
16	0-5	0.995	297	0.25074	BX	203.73
17	0-5	0.995	313	0.24079	BX	27.06
18	0-5	0.946	276	0.251636	BX	34.06
19	0-5	0.94	238	0.27824	BX	165.12
20	0-5	0.975	242	0.2847	BX	143.86
21	0-5	0.959	381	0.199472	BX	69.35
22	0-5	0.943	438	0.1/5398	BX	57.49
23	U-5	0.994	510	0.103010	BX	80.77
24	0-5	0.947	443	0.174248	BX	41.08
25	0-5	0.951	300	0.236072	BX	133.32
20	0-5	0.963	279	0 254232	BX	43.18
28	0-5	1.036	252	0.294224	BX	245.28
29	0-5	0.936	223	0.29016	BX	121.23
30	0-5	0.945	297	0.23814	BX	74.42
1	0-5	0.994	385	0.204764	CB	169.85
2	0-5	0.985	558	0.14972	CB	24.56
3	0-5	0.978	594	0.140832	CB	81.47
4	0-5	0.999	488	0.16983	CB	36.4
5	0-5	0.964	294	0.244856	CB	69.74
6	0-5	0.975	355	0.2145	CB	75.91
/	0-5	0.962	339	0.219330	CB	50.81
ð 0	0-5	0.991	488	0.1084/	CB	02.73 42.42
10	0-5	0.900	533	0.272970	CB	222 87
10	0-5	0.963	694	0 121338	CB	30.08
12	0-5	0.963	576	0.142524	CB	82.26
13	0-5	1.011	456	0.18198	CB	66.76
14	0-5	0.978	475	0.170172	CB	248.43
15	0-5	0.951	339	0.216828	CB	94.41
16	0-5	0.995	297	0.25074	CB	177.33
17	0-5	0.995	313	0.24079	CB	9.35
18	0-5	0.946	276	0.251636	CB	52.83
19	0-5	0.94	238	0.27824	CB	105.81
20	0-5	0.975	242	0.2847	CB	103.66
21	U-5 0 E	0.959	301 120	0.1794/2	CB	98.43 50.24
22	0-0 0_5	0.943	438 510	0.1/0390 0.162016	CB CR	00.24 107 1 <i>4</i>
23	0-5 0_5	0.774	210	0.103010	CB	30.26
25	0-5	0.951	268	0.258672	C.B	140 23
26	0-5	0.94	300	0.235	CB	29.86
27	0-5	0.963	279	0.254232	CB	7.95
28	0-5	1.036	252	0.294224	CB	210.68
29	0-5	0.936	223	0.29016	CB	42.49
30	0-5	0.945	297	0.23814	CB	78.98

S.Table 21: Data used for enzyme activity calculation: 0-5cm, BX and CB. \* mass of soil suspended in 100ml Buffer for Enzyme Assay.

Plot	Soil depth	Soil mass*	water content	dry weight	Enzyme	Activity
Nr.	cm	(g)	(g water g⁻¹ soil)	(g)		(nmol g <sup>-1</sup> soil h <sup>-1</sup> )
1	0-5	0.994	385	0.204764	BG	2259.6
2	0-5	0.985	558	0.14972	BG	1103.74
3	0-5	0.978	594	0.140832	BG	1202.57
4	0-5	0.999	488	0.16983	BG	1230.26
5	0-5	0.964	294	0.244856	BG	1344.16
6	0-5	0.975	355	0.2145	BG	1304.93
7	0-5	0.962	339	0.219336	BG	1347.14
8	0-5	0.991	488	0.16847	BG	2329.22
9	0-5	0.968	255	0.272976	BG	1330.74
10	0-5	0.965	533	0.15247	BG	2616.4
11	0-5	0.963	694	0.121338	BG	1337.93
12	0-5	0.963	5/6	0.142524	BG	1556.67
13	0-5	1.011	456	0.18198	BG	15/2.49
14	U-5	0.978	475	0.1/01/2	BG	1041.35
10	0-5	0.951	339	0.210828	BG	1011.38
10	0-5	0.995	297	0.23074	DG PC	572.22
17	0-5	0.995	212	0.24079	DG PC	012.61
10	0-5	0.940	270	0.231030	BG	1115
20	0-5	0.94	230	0.27024	BG	860.06
20	0-5	0.959	381	0.2047	BG	1372 44
21	0-5	0.943	438	0.175398	BG	589 45
22	0-5	0.994	510	0.163016	BG	1331.86
24	0-5	0.947	443	0.174248	BG	593.21
25	0-5	0.951	268	0.258672	BG	891.29
26	0-5	0.94	300	0.235	BG	808.19
27	0-5	0.963	279	0.254232	BG	482.88
28	0-5	1.036	252	0.294224	BG	1073.9
29	0-5	0.936	223	0.29016	BG	778.8
30	0-5	0.945	297	0.23814	BG	1081.09
1	0-5	0.994	385	0.204764	NAG	712.05
2	0-5	0.985	558	0.14972	NAG	414.83
3	0-5	0.978	594	0.140832	NAG	439.74
4	0-5	0.999	488	0.16983	NAG	512.93
5	0-5	0.964	294	0.244856	NAG	715.33
6	0-5	0.975	355	0.2145	NAG	517.99
/	0-5	0.962	339	0.219336	NAG	811.46
8	0-5	0.991	488	0.16847	NAG	11/3.8/
9	0-5	0.968	255	0.2/29/6	NAG	435.8
10	0-5	0.965	533	0.15247	NAG	1122.1
11	0-5	0.903	094 E74	0.121330	NAG	407.34
12	0-5	0.903	570 456	0.142524	NAG	444.70
13 1 <i>1</i>	0-5	0.078	450	0.10170	NAG	301.65
15	0-5	0.951	220	0.216828	NAG	658 57
16	0-5	0.995	297	0.25074	NAG	1175 75
10	0.5	0.995	217	0.24079	NAG	299.61
18	0-5	0.946	276	0.251636	NAG	552.01
19	0-5	0.94	238	0.27824	NAG	697.72
20	0-5	0.975	242	0.2847	NAG	775.19
21	0-5	0.959	381	0.199472	NAG	816.81
22	0-5	0.943	438	0.175398	NAG	539.02
23	0-5	0.994	510	0.163016	NAG	288.77
24	0-5	0.947	443	0.174248	NAG	437.9
25	0-5	0.951	268	0.258672	NAG	588.02
26	0-5	0.94	300	0.235	NAG	289.15
27	0-5	0.963	279	0.254232	NAG	474.1
28	0-5	1.036	252	0.294224	NAG	482.05
29	0-5	0.936	223	0.29016	NAG	540.65
30	0-5	0.945	297	0.23814	NAG	612.98

S.Table 22: Data used for enzyme activity calculation: 0-5cm, BG and NAG. \* mass of soil suspended in 100ml Buffer for Enzyme Assay.

Plot	Soil depth	Soil mass *	water content	dry weight	Enzyme	Activity
Nr.	cm	(g)	(g Water g <sup>-1</sup> Soil)	(g)		(nmol g <sup>-1</sup> soil h <sup>-1</sup> )
1	0-5	0.994	385	0.204764	AP	3582.08
2	0-5	0.985	558	0.14972	AP	2576.78
3	0-5	0.978	594	0.140832	AP	1200.27
4	0-5	0.999	488	0.16983	AP	1779.87
5	0-5	0.964	294	0.244856	AP	3411
6	0-5	0.975	355	0.2145	AP	1998.76
7	0-5	0.962	339	0.219336	AP	3373.74
8	0-5	0.991	488	0.16847	AP	4002.58
9	0-5	0.968	255	0.272976	AP	3628.45
10	0-5	0.965	533	0.15247	AP	3822.86
11	0-5	0.963	694	0.121338	AP	1927.69
12	0-5	0.963	576	0.142524	AP	2238.65
13	0-5	1.011	456	0.18198	AP	1989.38
14	0-5	0.978	475	0.170172	AP	1407.16
15	0-5	0.951	339	0.216828	AP	2430.82
16	0-5	0.995	297	0.25074	AP	5645.23
17	0-5	0.995	313	0.24079	AP	2826.43
18	0-5	0.946	276	0.251636	AP	2286.53
19	0-5	0.94	238	0.27824	AP	7462.58
20	0-5	0.975	242	0.2847	AP	4406.48
21	0-5	0.959	381	0.199472	AP	4597.87
22	0-5	0.943	438	0.175398	AP	4229.06
23	0-5	0.994	510	0.163016	AP	4834.46
24	0-5	0.947	443	0.174248	AP	1897.29
25	0-5	0.951	268	0.258672	AP	3704.43
26	0-5	0.94	300	0.235	AP	2708.19
27	0-5	0.963	279	0.254232	AP	2425.09
28	0-5	1.036	252	0.294224	AP	2337.88
29	0-5	0.936	223	0.29016	AP	2209.85
30	0-5	0.945	297	0.23814	AP	3077.88
1	0-5	0.994	385	0.204764	LAP	2066.22
2	0-5	0.985	558	0.149/2	LAP	844.05
3	0-5	0.978	594	0.140832	LAP	1/15.56
4	0-5	0.999	488	0.16983	LAP	1605.19
5	0-5	0.964	294	0.244856	LAP	1200.7
6	0-5	0.975	355	0.2145	LAP	1988.32
1	0-5	0.962	339	0.219336	LAP	1808.06
8	0-5	0.991	488	0.10847	LAP	2087.93
9	0-5	0.968	255	0.2/29/0		1133.17
10	0-5	0.905	604	0.13247		1464 54
10	0-5	0.703	576	0.121330		1016 20
12	0-5	1 011	456	0.142324		1561 04
13	0-5	0.978	430	0.170172	LAP	1670 51
15	0.5	0.951	220	0.216828		1914 05
16	0-5	0.995	297	0.25074	LAP	1872.01
17	0-5	0.995	313	0 24079	LAP	1548 91
18	0-5	0.946	276	0.251636	I AP	1187.99
19	0-5	0.94	238	0.27824	LAP	1485.77
20	0-5	0.975	242	0.2847	LAP	1426.02
21	0-5	0.959	381	0.199472	LAP	1912.04
22	0-5	0.943	438	0.175398	LAP	1395.24
23	0-5	0.994	510	0.163016	LAP	2954.14
24	0-5	0.947	443	0.174248	LAP	1732.81
25	0-5	0.951	268	0.258672	LAP	1347.9
26	0-5	0.94	300	0.235	LAP	1418.24
27	0-5	0.963	279	0.254232	LAP	1312.31
28	0-5	1.036	252	0.294224	LAP	2228.45
29	0-5	0.936	223	0.29016	LAP	1636.37
30	0-5	0.945	297	0.23814	LAP	2035.38

S.Table 23: Data used for enzyme activity calculation: 0-5cm, AP and LAP. \*Mass of soil suspended in 100ml Buffer for Enzyme Assay.

Plot	Soil depth	Soil mass *	water content	dry weight	Enzyme	Activity
Nr.	cm	(g)	(g Water g <sup>-1</sup> Soil)	(g)		(nmol g <sup>-1</sup> soil h <sup>-1</sup> )
1	5-10	0.975	380.7692308	0.2028	BX	197.4120545
2	5-10	0.979	584.9315068	0.142934	BX	156.1856371
3	5-10	0.966	541.025641	0.150696	BX	215.3466822
4	5-10	0.963	495.2380952	0.161784	BX	142.5204891
5	5-10	0.975	323.7288136	0.2301	BX	180.86574
6	5-10	0.96	323.7288136	0.22656	BX	154.5477979
7	5-10	0.992	624.6376812	0.136896	BX	302.671098
8	5-10	0.951	247.2222222	0.273888	BX	189.161659
9	5-10	0.967	145.0980392	0.394536	BX	57.10068579
10	5-10	0.961	262.3188406	0.265236	BX	171.2372561
11	5-10	1.003	861.5384615	0.104312	BX	278.2590428
12	5-10	0.96	549.3506494	0.14/84	BX	235.5443528
13	5-10	0.995	443.4/82609	0.18308	BX	190.4283146
14	5-10	1.049	455.5555556	0.18882	BX	177.9510408
15	5-10	0.995	281.6793893	0.26069	BX	273.6204403
10	5-10 5-10	0.98	254.6099291	0.27030	BX	160.2009120
1/	5-10 5-10	0.98	287.5968992	0.25284	BX	101.9342837
10	5-10 E 10	0.90	287.3908992	0.24708	DX DV	180./00/393
19	5-10	0.99	207.0470300	0.20920		140.400091
20	5-10	0.90	270.3703704	0.2392	BX	24.1274732
21	5 10	0.07	110 20/0816	0.21012	BX	120 0110221
22	5-10	1.08	410.2040810	0.19012	BY	137.7117321
23	5-10	1.00	437.0344000	0.20000	BX	182 2162701
24	5-10	0.96	303 2258065	0.23808	BX	198 8322544
25	5-10	0.70	247 22220003	0.23000	BX	110 3559021
27	5-10	0.96	267.6470588	0.26112	BX	173.6113526
28	5-10	0.94	273.1343284	0.25192	BX	161.7470411
29	5-10	1.05	247.2222222	0.3024	BX	126.9233372
30	5-10	0.95	237.8378378	0.2812	BX	164.9095593
1	5-10	0.975	380.7692308	0.2028	CB	102.3334057
2	5-10	0.979	584.9315068	0.142934	CB	188.2476513
3	5-10	0.966	541.025641	0.150696	CB	243.770545
4	5-10	0.963	495.2380952	0.161784	CB	211.2180001
5	5-10	0.975	323.7288136	0.2301	CB	210.6047915
6	5-10	0.96	323.7288136	0.22656	CB	181.255075
7	5-10	0.992	624.6376812	0.136896	CB	399.2860925
8	5-10	0.951	247.2222222	0.273888	CB	317.2657752
9	5-10	0.967	145.0980392	0.394536	CB	43.52491727
10	5-10	0.961	262.3188406	0.265236	CB	180.0244213
11	5-10	1.003	861.5384615	0.104312	CB	255.4/4646/
12	5-10	0.96	549.3506494	0.14/84	CB	201.4290009
13	5-10 5-10	0.995	443.4782609	0.18308	CB	105.0407050
14	5-10 E 10	1.049	400.000000	0.18882	CB	101.3133808
15	5-10	0.995	281.0/93893	0.26069	CB	328.5565478
10	0-10 E 10	0.90	204.0099291	0.27030	CD	102.0324102
17	5-10	0.96	207.3900992	0.20204	CB	172.3794134
10	5-10	0.90	267.5706772	0.24700	CB	1/2 7/52/00
20	5 10	0.99	207.0470300	0.20920	CB	12/ 0260215
20	5-10	1.02	385 / 368932	0.2372	CB	250 0662317
2 I 22	5-10	0.97	410 2040816	0.21012	CR	54 37497249
22	5-10	1.08	437.6344086	0.20088	CB	184.0035574
23	5-10	1.01	420.8333333	0.19392	CB	174,4051246
25	5-10	0.96	303.2258065	0.23808	CB	216.0818015
26	5-10	0.95	247.2222222	0.2736	CB	150.0628437
27	5-10	0.96	267.6470588	0.26112	CB	199.540386
28	5-10	0.94	273.1343284	0.25192	CB	157.1712379
29	5-10	1.05	247.2222222	0.3024	СВ	162.0405257
30	5-10	0.95	237.8378378	0.2812	СВ	185.8073246

S.Table 24: Data used for enzyme activity calculation: 5-10cm, BX and CB. \*Mass of soil suspended in 100ml Buffer for Enzyme Assay.

Plot	Soil depth	Soil mass *	water content	dry weight	Enzyme	Activity
Nr.	cm	(g)	(g Water g <sup>-1</sup> Soil)	(g)		(nmol g <sup>-1</sup> soil h <sup>-1</sup> )
1	5-10	0.975	380.7692308	0.2028	BG	1442.542187
2	5-10	0.979	584.9315068	0.142934	BG	1360.022226
3	5-10	0.966	541.025641	0.150696	BG	1688.938716
4	5-10	0.963	495.2380952	0.161784	BG	1249.354714
5	5-10	0.975	323.7288136	0.2301	BG	1638.642168
6	5-10	0.96	323.7288136	0.22656	BG	1512.138729
7	5-10	0.992	624.6376812	0.136896	BG	2620.358504
8	5-10	0.951	247.2222222	0.273888	BG	1946.328021
9	5-10	0.967	145.0980392	0.394536	BG	413.2808702
10	5-10	0.961	262.3188406	0.265236	BG	1463.823347
11	5-10	1.003	861.5384615	0.104312	BG	2121.224486
12	5-10	0.96	549.3506494	0.14784	BG	2001.877938
13	5-10	0.995	443.4782609	0.18308	BG	1535.750824
14	5-10	1.049	455.5555556	0.18882	BG	1300.55251
15	5-10	0.995	281.6793893	0.26069	BG	2212.010083
16	5-10	0.98	254.6099291	0.27636	BG	1752.243471
17	5-10	0.98	287.5968992	0.25284	BG	1659.719631
18	5-10	0.96	287.5968992	0.24768	BG	1574.780215
19	5-10	0.99	267.6470588	0.26928	BG	921.9271149
20	5-10	0.96	270.3703704	0.2592	BG	813.8543612
21	5-10	1.02	385.4368932	0.21012	BG	2484.571126
22	5-10	0.97	410.2040816	0.19012	BG	899.6210154
23	5-10	1.08	437.6344086	0.20088	BG	1673.401544
24	5-10	1.01	420.8333333	0.19392	BG	2280.339247
25	5-10	0.96	303.2258065	0.23808	BG	1780.161335
26	5-10	0.95	247.2222222	0.2736	BG	1305.6813
27	5-10	0.96	267.6470588	0.26112	BG	1745.110733
28	5-10	0.94	273.1343284	0.25192	BG	1474.210311
29	5-10	1.05	247.2222222	0.3024	BG	1383.73412
30	5-10	0.95	237.8378378	0.2812	BG	1700.085972
1	5-10	0.975	380.7692308	0.2028	NAG	1317.343314
2	5-10	0.979	584.9315068	0.142934	NAG	755.7166553
3	5-10	0.966	541.025641	0.150696	NAG	612.8784322
4	5-10	0.963	495.2380952	0.161784	NAG	670.9534748
5	5-10	0.975	323.7288136	0.2301	NAG	1103.849294
6	5-10	0.96	323.7288136	0.22656	NAG	706.9176845
7	5-10	0.992	624.6376812	0.136896	NAG	1487.511073
8	5-10	0.951	247.2222222	0.273888	NAG	905.6575964
9	5-10	0.967	145.0980392	0.394536	NAG	385.7334188
10	5-10	0.961	262.3188406	0.265236	NAG	607.0574715
11	5-10	1.003	861.5384615	0.104312	NAG	1997.00363
12	5-10	0.96	549.3506494	0.14/84	NAG	/32.1054466
13	5-10	0.995	443.4782609	0.18308	NAG	292.0802825
14	5-10	1.049	455.5555556	0.18882	NAG	409.7775511
15	5-10	0.995	281.6793893	0.26069	NAG	968.870052
10	5-10	0.98	254.6099291	0.27636	NAG	1249.150114
1/	5-10	0.98	287.5968992	0.25284	NAG	1/33.002938
10	5-10 E 10	0.90	287.3908992	0.24708	NAG	1007.7927
19	5-10 E 10	0.99	207.0470300	0.20920	NAG	775 0001014
20	5-10	0.90	270.3703704	0.2392	NAG	1140 202702
∠ I 22	5-10	0.02	JUJ.4JU07JZ 110 2010014	0.21012	NAG	571 502/02
22	5-10	1.00	410.2040010	0.17012	NAG	571.3027010 656 2220000
23 24	5-10	1.00	437.0344000	0.20000	NAG	1000.0027707
24 25	5-10	0.04	420.00000000 202 2250065	0.17372	NAG	1227.012700 002 2602605
25	5-10	0.90	247 22220003	0.23000	NAG	523 0030753
20	5-10	0.95	267.6470588	0.2730	NAG	858 37057/9
27	5-10	0.94	273 1343284	0.25192	NAG	756 1321428
20	5-10	1.05	247 22207	0.3024	NAG	1030.040754
30	5-10	0.95	237.8378378	0.2812	NAG	820.4980561

S.Table 25: Data used for enzyme activity calculation: 5-10cm, BG and NAG. \*Mass of soil suspended in 100ml Buffer for Enzyme Assay.

Plot	Soil depth	Soil mass *	water content	dry weight	Enzyme	Activity
Nr.	cm	(g)	(g Water g <sup>-1</sup> Soil)	(g)		(nmol g <sup>-1</sup> soil h <sup>-1</sup> )
1	5-10	0.975	380.7692308	0.2028	AP	2413.292658
2	5-10	0.979	584.9315068	0.142934	AP	1837.637156
3	5-10	0.966	541.025641	0.150696	AP	1925.097583
4	5-10	0.963	495.2380952	0.161784	AP	1568.942661
5	5-10	0.975	323.7288136	0.2301	AP	1621.082292
6	5-10	0.96	323.7288136	0.22656	AP	2106.425892
7	5-10	0.992	624.6376812	0.136896	AP	4278.280093
8	5-10	0.951	247.2222222	0.273888	AP	3250.859077
9	5-10	0.967	145.0980392	0.394536	AP	1425.468116
10	5-10	0.961	262.3188406	0.265236	AP	1986.811305
11	5-10	1.003	861.5384615	0.104312	AP	2474.98153
12	5-10	0.96	549.3506494	0.14784	AP	2102.821593
13	5-10	0.995	443.4782609	0.18308	AP	1961.035659
14	5-10	1.049	455.5555556	0.18882	AP	2306.248953
15	5-10	0.995	281.6793893	0.26069	AP	2044.327222
16	5-10	0.98	254.6099291	0.27636	AP	3704.605891
17	5-10	0.98	287.5968992	0.25284	AP	1903.161253
18	5-10	0.96	287.5968992	0.24768	AP	1686.530106
19	5-10	0.99	267.6470588	0.26928	AP	1930.633021
20	5-10	0.96	270.3703704	0.2592	AP	1969.082876
21	5-10	1.02	385.4368932	0.21012	AP	2472.441099
22	5-10	0.97	410.2040816	0.19012	AP	1523.655139
23	5-10	1.08	437.6344086	0.20088	AP	1979.410779
24	5-10	1.01	420.8333333	0.19392	AP	2540.118975
25	5-10	0.96	303.2258065	0.23808	AP	1532.281268
26	5-10	0.95	247.2222222	0.2736	AP	1077.533944
27	5-10	0.96	207.0470588	0.26112	AP	2302.257524
28	5-10 5-10	0.94	2/3.1343284	0.25192	AP	1589.394077
29	5-10 E 10	1.05 0.0E	247.2222222	0.3024	AP AD	1030.309032
	5-10	0.95	237.0370370	0.2012		2327.203320
ן ז	5-10	0.975	584 0315068	0.2020		2701 11262
2	5-10	0.966	541 025641	0.150696	ΙΔΡ	4969 854509
4	5-10	0.963	495 2380952	0.161784	LAP	4616 337777
5	5-10	0.975	323 7288136	0 2301	LAP	3440 309682
6	5-10	0.96	323,7288136	0.22656	LAP	3784.077594
7	5-10	0.992	624.6376812	0.136896	LAP	6111.334655
8	5-10	0.951	247.2222222	0.273888	LAP	3796.291142
9	5-10	0.967	145 0980392	0.394536	LAP	1294 497227
10	5-10	0.961	262.3188406	0.265236	LAP	3838.602484
11	5-10	1.003	861.5384615	0.104312	LAP	8111.695615
12	5-10	0.96	549.3506494	0.14784	LAP	5741.329904
13	5-10	0.995	443.4782609	0.18308	LAP	3772.590796
14	5-10	1.049	455.5555556	0.18882	LAP	3538.771329
15	5-10	0.995	281.6793893	0.26069	LAP	3830.377917
16	5-10	0.98	254.6099291	0.27636	LAP	3383.60864
17	5-10	0.98	287.5968992	0.25284	LAP	3644.790226
18	5-10	0.96	287.5968992	0.24768	LAP	3298.471
19	5-10	0.99	267.6470588	0.26928	LAP	3030.388456
20	5-10	0.96	270.3703704	0.2592	LAP	2274.099269
21	5-10	1.02	385.4368932	0.21012	LAP	3775.750261
22	5-10	0.97	410.2040816	0.19012	LAP	4047.341571
23	5-10	1.08	437.6344086	0.20088	LAP	3089.048096
24	5-10	1.01	420.8333333	0.19392	LAP	3945.697572
25	5-10	0.96	303.2258065	0.23808	LAP	3187.139248
26	5-10	0.95	247.2222222	0.2736	LAP	2973.927539
27	5-10	0.96	267.6470588	0.26112	LAP	3633.390355
28	5-10	0.94	2/3.1343284	0.25192	LAP	3556.66619
29	5-10	1.05	247.2222222	0.3024	LAP	3207.877706
30	5-10	0.95	231.8318318	0.2812	LAP	2959.450275

S.Table 26: Data used for enzyme activity calculation: 5-10cm, AP and LAP. \*Mass of soil suspended in 100ml Buffer for Enzyme Assay.